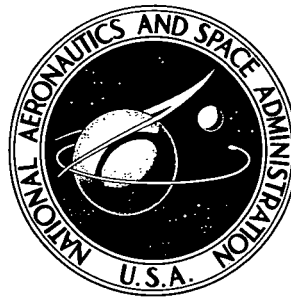


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**PERFORM - A PERFORMANCE OPTIMIZING
COMPUTER PROGRAM FOR DYNAMIC SYSTEMS
SUBJECT TO TRANSIENT LOADINGS**

by W. D. Pilkey, B. P. Wang, Y. Yoo, and B. Clark

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16. Abstract This report contains a description and applications of a computer capability for determining the ultimate optimal behavior of a dynamically loaded structural-mechanical system. This capability provides characteristics of the "theoretically best," or limiting, design concept according to response criteria dictated by design requirements. Equations of motion of the system in first or second order form include incompletely specified elements whose characteristics are determined in the optimization of one or more performance indices subject to the response criteria in the form of constraints. The system is subject to deterministic transient inputs, and the computer capability is designed to operate with a large linear programming on-the-shelf software package which performs the desired optimization. The report contains user-oriented program documentation in engineering, problem-oriented form. Applications cover a wide variety of dynamics problems including those associated with such diverse configurations as a missile-silo system, impacting freight cars, and an aircraft ride control system.					
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FOREWORD

The research described in this report (University of Virginia Project No. 4085-0320) was performed at the University of Virginia Research Laboratories for the Engineering Sciences. W. D. Pilkey was principal investigator. The project was performed under NASA Grant No. NGR 47-005-145 and administered at NASA Langley Research Center.

Special thanks are due to Murray Manufacturing, Division Arrow Hart, Inc. of Earlysville, Virginia, who permitted the use of their computer terminal for communication with a computer center possessing software essential to this project. In addition Murray Manufacturing provided the special accessories necessary to adapt their terminal for our use.

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SECTION I

INTRODUCTION

The current state of the design of physical systems is in some respects as much an art as a science. Of the many considerations involved in systems design, perhaps those related to an evaluation of the physical performance best lend themselves to formal automation. This report describes the results of an effort to place this aspect of real-world systems design on an analytical basis. In particular, a computational capability, PERFORM, has been developed for the evaluation of the limiting physical performance of systems subject to transient disturbances.

PERFORM provides the characteristics of the theoretically best, that is, the limiting, design concept according to response criteria. As a consequence, for certain mechanical, structural, and control systems PERFORM makes it possible to approach a design directly from the design criteria with no a priori commitment to a particular design concept. With this limiting performance capability, the designer can determine the feasibility of his proposed design on the basis of the specifications alone; moreover, he can monitor and measure his success during the design process itself. Heretofore, without the characteristics of the limiting design, the evaluation of proposed designs could be made only by performing a multitude of analyses for each candidate design.

This capability applies to systems with transient loading in which response criteria are of concern. These criteria are usually expressed in terms of constraints formed from displacements, stresses, forces, velocities, or accelerations that cannot exceed certain prescribed values. In addition, objective functions of peak values of other responses are to be minimized. PERFORM provides the time-optimal characteristics of portions of a system such that these constraints are satisfied and objective functions are minimized or maximized.

An outline of the capabilities of PERFORM is given in Section II.

Section III of this report describes the components and design of PERFORM. Also, the procedure for using PERFORM is outlined.

Section IV contains applications of PERFORM, including some numerical results. Among the problems discussed are rail vehicle suspension systems, train impact, aircraft ride control, launch vehicle control, missile/silo isolation, and a

nuclear reactor control system.

The Users Guide for PERFORM is given in Appendix I. The details of the technical formulation underlying PERFORM are in Appendix II. Appendix III contains the programming aspects of the system, including programming documentation. The final Appendix contains listings of programs.

SECTION II

CAPABILITIES OF PERFORM

PERFORM is a computer system that can be used to determine the limiting performance characteristics of a dynamic system subject to transient loading. Ref. 1 considers in detail the concept of limiting performance and its application to shock isolation systems. The example problems of Section IV provide an indication of the range of applications of PERFORM.

The dynamic system can be described and input to PERFORM using the first or second order equations

$$\dot{\bar{s}} = \underline{A}\bar{s} + \underline{B}\bar{u} + \underline{D}\bar{f}_k$$

$$\underline{M}\ddot{\bar{q}} + \underline{C}\dot{\bar{q}} + \underline{K}\bar{q} + \underline{U}\bar{u} = \underline{F}\bar{f}_k$$

in which \bar{u} is a vector of time varying functions, called control or isolator forces, that have replaced portions of the dynamic system. \underline{A} , \underline{B} , \underline{D} , \underline{M} , \underline{C} , \underline{K} , \underline{U} , \underline{F} are coefficient matrices. \bar{s} and \bar{q} are vectors of response variables, e.g., displacements, stresses, accelerations. \bar{f}_k is a forcing function vector where the subscript k designates the k^{th} set of forcing or loading functions. This allows the system to encounter alternative sets of disturbances which might occur with equal probability.

The acceptable equations of motion appear to be linear. In fact, however, they are "quasilinear" since those portions of the system replaced by \bar{u} can be linear, nonlinear, active, or passive. The remainder of the system must be linear as must the overall kinematics.

The user must place his equations in one of the forms of the above equations. The non-zero elements of the matrices \underline{A} , \underline{B} , \underline{D} or \underline{M} , \underline{C} , \underline{K} , \underline{U} , \underline{F} are then entered as inputs. This is accomplished by identifying the matrix, e.g., \underline{M} MATRIX, and then specifying an element and its value, e.g., i , j , and M_{ij} . Elements not entered are assumed to be zero.

PERFORM finds the characteristics, including \bar{u} and trade-offs between optimal response variables, of the dynamic system such that bounds on some of the response variables \bar{s} or \bar{q} or control forces \bar{u} are not violated while the maximum (or minimum) in time of other elements of \bar{s} or \bar{q} are minimized (or maximized).

Regardless of the form (first or second order) used to describe the equations of motion, the formats for the objective function and constraints are the same. In the case of the second order equations, a state variable vector \bar{s} is established as

$$\bar{s} = \begin{bmatrix} \ddot{\bar{q}} \\ \dot{\bar{q}} \\ \bar{q} \end{bmatrix}$$

Any linear combination of state variables, derivatives of state variables, or control forces can be used as an objective function. In the case of the system described by second order equations, these become linear combinations of accelerations, velocities, displacements, and control forces. The objective function is input to PERFORM in the form of

$$\underline{PX1}\bar{s} + \underline{PX2}\bar{u} + \underline{PX3}\bar{f}_k$$

where $\underline{PX1}$, $\underline{PX2}$ and $\underline{PX3}$ are coefficient matrices. If more than one row of the matrices of this equation contains non-zero elements, then the peak values in time of the vectors resulting from the meaningful rows are to be compared. PERFORM minimizes (maximizes) the maximum (minimum) of the peak values.

Constraints may be placed on state variables, derivatives of state variables, and control forces. The general form, which is again linear, is

$$\bar{Y}\bar{L} \leq \bar{Y1}\bar{s} + \bar{Y2}\bar{u} + \bar{Y3}\bar{f}_k \leq \bar{Y}\bar{U}$$

where $\bar{Y1}$, $\bar{Y2}$, $\bar{Y3}$ are coefficient matrices and $\bar{Y}\bar{L}$, $\bar{Y}\bar{U}$ are lower and upper bound vectors. Constraints can be imposed at every time of the response or at specific times.

In summary, PERFORM accepts system equations of the form given above. For prescribed initial conditions, PERFORM then computes the \bar{u} vector such that the max $|\underline{PX1}\bar{s} + \underline{PX2}\bar{u} + \underline{PX3}\bar{f}_k|$

is minimized (or min $|\quad|$ is maximized) while the above constraints are satisfied. Any linear combination of \bar{s} , \bar{u} , and \bar{f}_k can be tabulated or plotted versus time. A tradeoff curve between the maximum objective function and any particular constraint can be generated by varying the bounds on that constraint.

SECTION III

PERFORM SYSTEM DESCRIPTION

To do the limiting performance problem calculations a computer system named PERFORM has been developed. Because several separate programs are used, it is referred to as a system rather than a program.

In this section the system is described with increasing detail. First, the system is presented from the "systems analyst" point of view; the programs, data sets, and inter-relations thereof are described and graphically presented with a system flowchart. Next the functions, subroutine calls, logic, etc. of each of the system programs are described. Program listings and discussions are in Appendix III.

A. System Design

PERFORM is a system of several programs, the functions, inputs, and outputs of which are outlined here. Influencing considerations of the development and operation environment are also discussed.

1. System Flow Description

Figure 1 is the PERFORM system flowchart. The three separate system programs are represented by rectangular boxes; these programs are:

- . PREPROC (Pre-processor)
- . LP Solver (linear programming computer program)
- . PSTPROC (Post-processor)

a. PREPROC

Using the mathematical model of the dynamic system, the pre-processor program computes and punches the linear programming problem from the PERFORM problem specifications described in Appendix I. There are three outputs of this program:

- . PSTPROC Report Specification. This card file contains information necessary for PSTPROC (to which this is an input file) to determine and print the problem solution.
- . Linear Programming Problem Input. This card output is the linear pro-

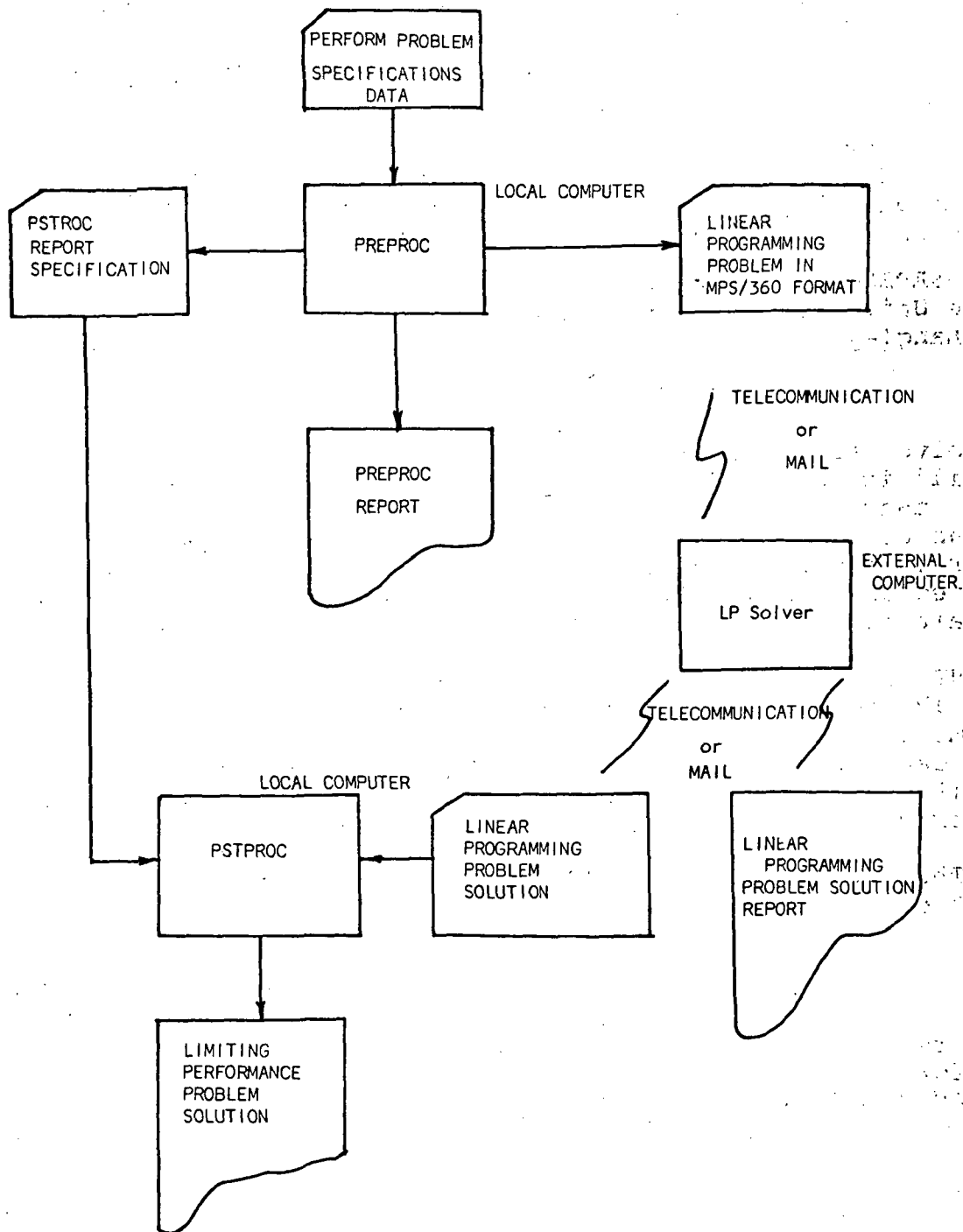


Fig. 1 PERFORM System Flowchart

gramming problem input in MPS/360 format, which is accepted by most major LP solvers.

PREPROC Report. This report is a printed record of the above files.

User options can control the contents of this report. The curved-bottom box is the standard flowcharting symbol for printed reports

The data transmission links are restricted somewhat in both the University of Virginia development environment and the NASA/Langley operating environment. These constraints are discussed in the section entitled "Environment Considerations."

PREPROC is written entirely in FORTRAN and has been tested on the University of Virginia Burroughs B5500, CDC6400, and the NASA/Langley CDC 6600.

b. LP Solver

This refers to any software package that can solve large linear programming problems. Examples of such capabilities are IBM MPS/360, CDC OPTIMA, and CDC OPHELIE. All of these programs accept MPS/360 input format. Since MPS/360 was used in the developmental stages of PERFORM, the LP Solver in the subsequent discussions of this report will be referred to as MPS/360. Anywhere MPS/360 is mentioned, other software packages, such as OPTIMA, could also be used.

MPS/360, Mathematical Programming System/360, is an open ended IBM software package capable of efficiently solving extremely large linear programming problems. The latest versions can handle problems of up to 16,000 rows and essentially unlimited columns. Several workfiles used by MPS/360 are omitted for clarity on the system flowchart of Fig. 1.

The input to MPS/360 is the output of "linear programming input" of PREPROC.

c. PSTPROC

The post-processor program produces the final report of the problem solution. Two inputs are necessary for PSTPROC: the linear programming problem solution from LP Solver and the PSTPROC report specifications from PREPROC. This program is written entirely in FORTRAN.

2. Environment Considerations

In Fig. 1 the programs are labeled "local" and "external" computer and a communications link is shown to and from the LP Solver step. This clearly awkward arrangement is used because

of the limitations of available computing facilities. The Langley Research Center CDC 6600 computing facility has no appropriate linear programming software. At Langley the PERFORM system cannot be run entirely locally, thus the need for an external computer. The system developed is a synthesis of these above constraints and the desire for maximum utilization of local facilities.

Punched cards are indicated as the storage medium for program data interchange. Cards were convenient for transmission to the external computer during development. Replacement with tape would be desirable and easily accomplished for large problems with unmanagable card files.

The decision to use MPS/360 was based on economy and availability. For development, the Virginia Polytechnic Institute and State University IBM/360 50-65 multiprocessor system, with an IBM 2780 telecommunications terminal was used. Recently, OPTIMA on the University of Virginia CDC 6400 has been used.

Use of the system is much simpler if a linear programming package is available locally. The data can be passed between programs on a disk, and the user does not have to be concerned with this data. One can simply put his problem specification data with some prepared control cards and receive the problem solution with one run.*

B. Program Descriptions

Each of the three programs of the system is further described in this section. The purpose of the description is to relate the program coding to the limiting performance problem model but without involving computational details. A detailed listing with more discussion is given in Appendix III.

1. PREPROC

Figure 2 is a flowchart of the main section of PREPROC. This section contains all input, calls to computational subroutines, and varying bound calculations.

Some notes about the flowchart are in order. Predefined blocks, the blocks with outward pointed sides and parallel top and bottom, represent subroutine calls; the name in the block is that of the subroutine. The trapezoidal-shaped box enclosing most of the third page and beneath the label "For each varying bound" is unconventional. It signifies that the sequence of instructions in the block is to be executed for the

* This is currently possible on an automated version of PERFORM at the University of Virginia Computer Science Center, both for on-campus users and for users accessing the computer from a remote, compatible computer terminal.

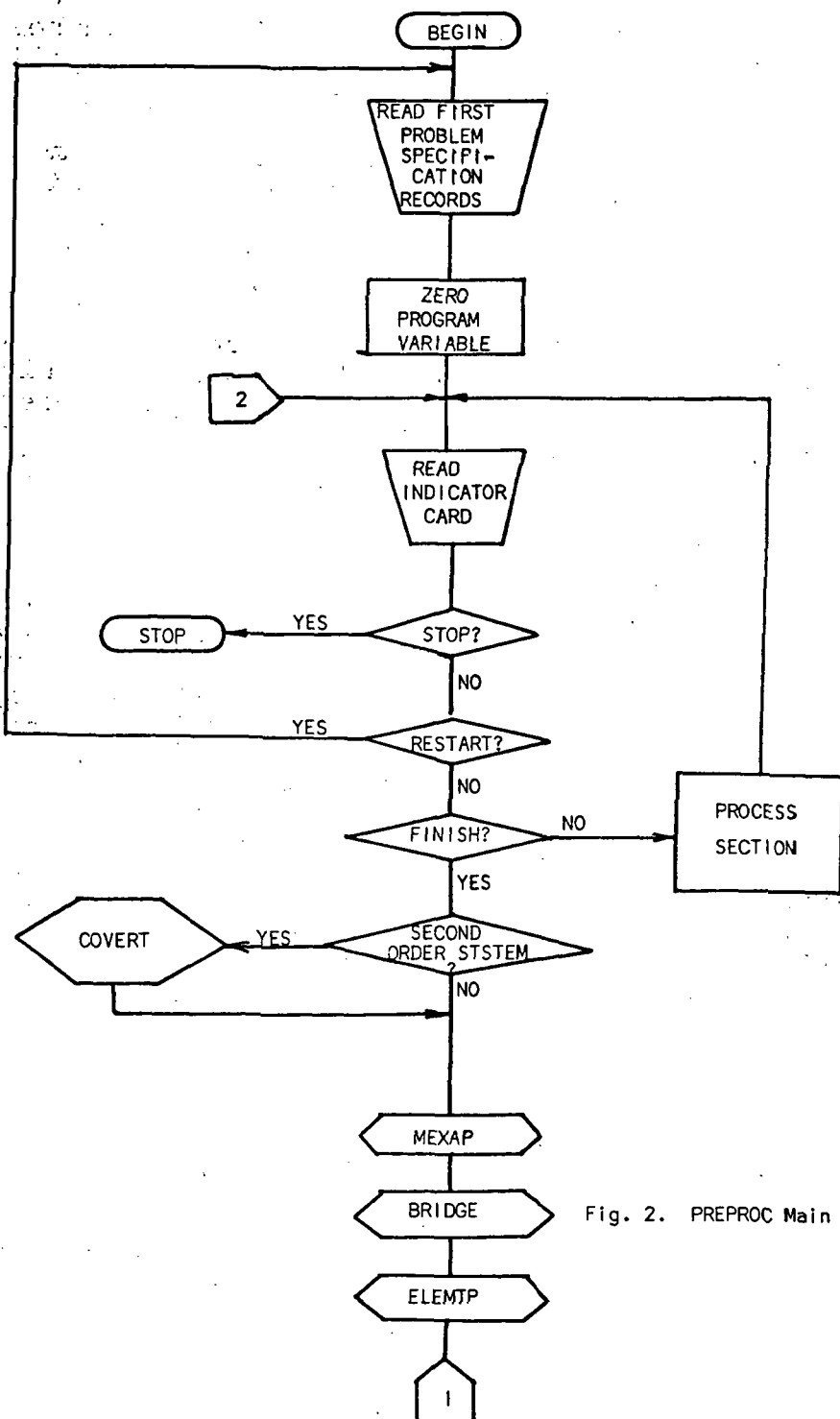


Fig. 2. PREPROC Main Section

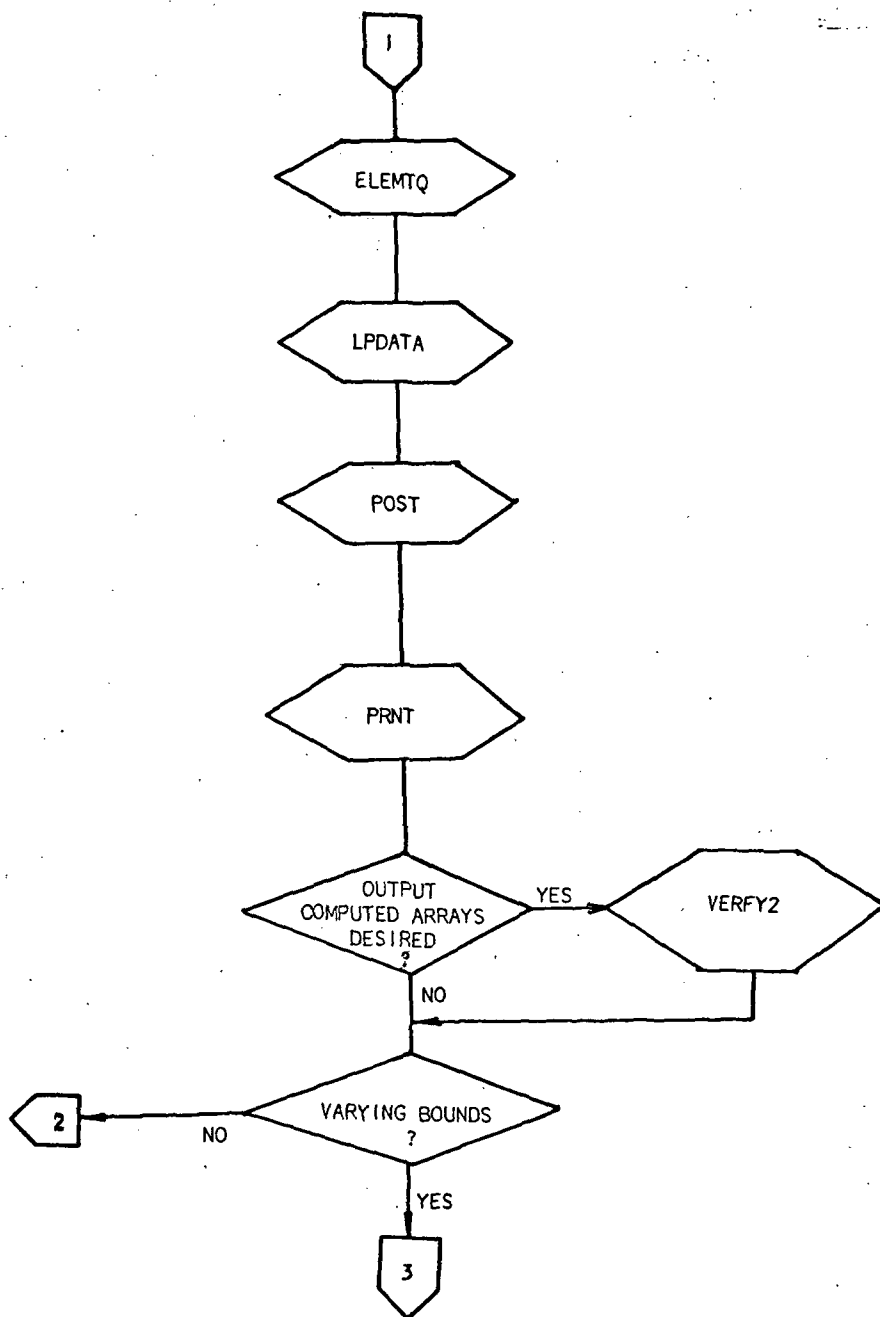


Fig. 2 PREPROC Main Section (continued)

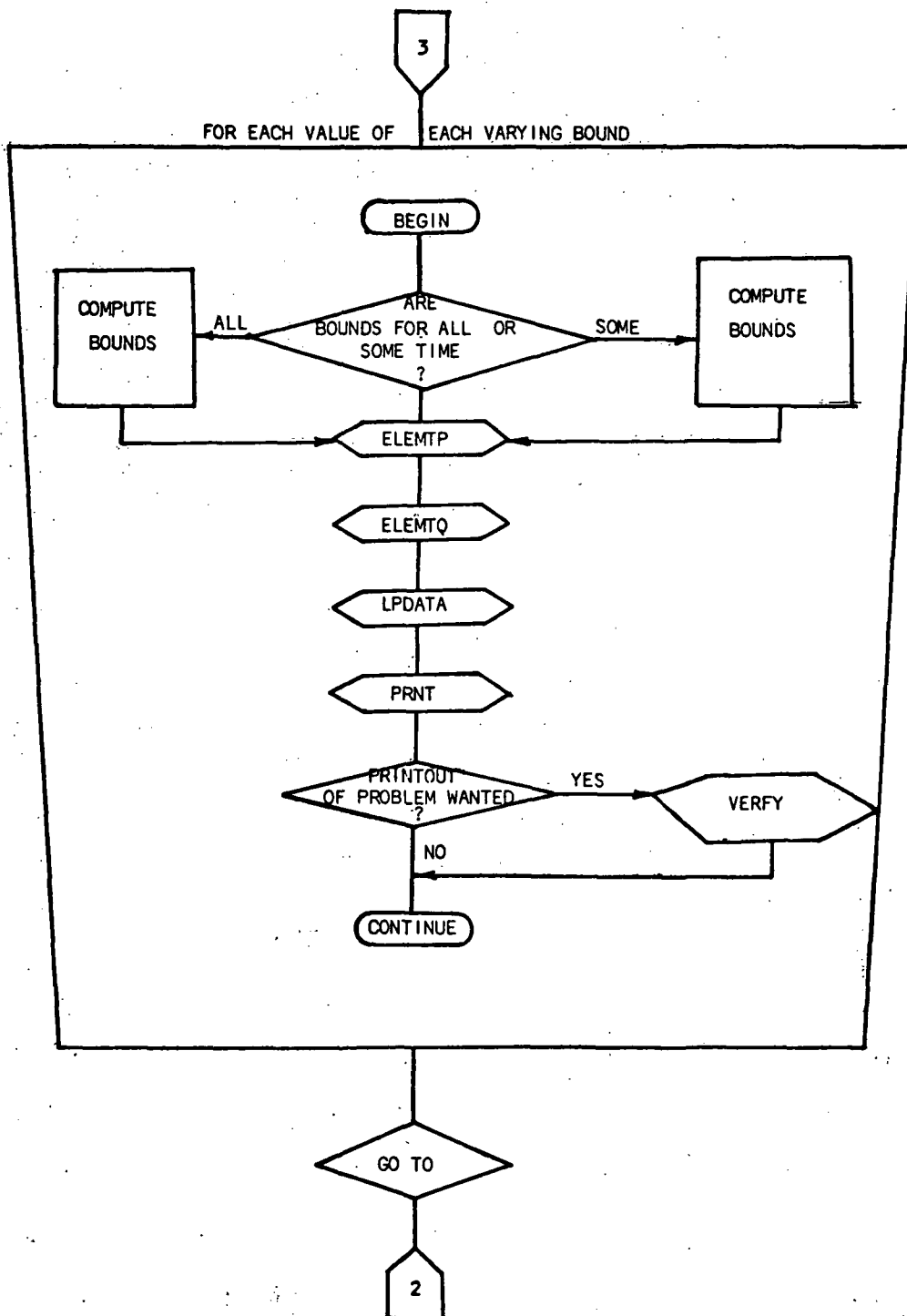


Fig. 2 PREPROC Main Section (concluded)

value of each varying bound, i.e., varying row of the $\overline{Y_L}$ and $\overline{Y_U}$ vectors. This flowchart is not an exact representation of the actual program; from it one can tell what the program does but not necessarily how it is done.

Because all files except those for printed output in the PERFORM system are either cards or in card format, the word "record" used to describe file elements can be interpreted as "card" in this discussion. The records of the problem specifications file are of two types: data and indicator. Data records contain values of program variables. By preceding data records, indicator records associate values with variables; indicator cards also contain problem processing specifications.

Before each section of data records of values for program variables there is an indicator card specifying the program variable array. The last card of a section contains a 1 in the key field; previous cards of the section have a zero in this field. Following the last card of a section the program presumes an indicator card. The program contains no error detection facilities so it behooves the user to double check his input. Details of these records are found in Appendix I. The first thing done by the program is to read three problem specifications records; in Appendix I these three records are numbered cards 1, 2, and 3. Next, most program variables are initialized to zero.

The fourth block reads an indicator card. If the card is a STOP indicator card the program stops. If a RESTART indicator, control returns to the program beginning and a new problem may be processed. A FINISH INPUT DATA record starts the problem processing. Appropriate processing for other indicators is performed - this includes such things as array entry, array printing, problem modification, etc.

If the dynamic system equations are second order, subroutine COVERT is called to reduce the second order equations to first order. The order reduction method is described in Appendix II.

Subroutine MEXAP computes exponential functions of matrices. These are array \underline{P} and array \underline{AEI} , both defined in Appendix II.

The next routine, BRIDGE, computes arrays for matrices \underline{R} , \underline{T} , and vectors $\underline{C1}$, $\underline{C2}$, and \underline{C} as described in Appendix II.

Routine ELEMTP is called to compute those portions of the \underline{H} and \underline{G} arrays that are determined by the objective function. These portions are shown in Table 1 of Appendix II.

The other portions of these arrays, determined by the problem constraints, as shown in Tables 2A and 2B of Appendix II, are calculated in subroutine ELEMTO. Subroutines ELEMTR, ELEMST, and ELEMSTT are called by ELEMTO for calculations but are not shown in Fig. 2. With H and G arrays computed, the next step is to output the results.

Subroutine LPDATA is called to produce the MPS/360 linear programming problem. Other subroutines, not shown, are called to punch different sections of the MPS input: CODATA for columns, RODATA for rows, RHDATA for the right hand sides, and BODATA on the bounds.

The POST routine punches the PSTPROC report specifications. Although this file is shown separately from the MPS/360 linear programming file the user must separate the two from the single card punch output.

To provide a printed problem record subroutine PRNT prints the H and G arrays. If a printout of the calculated arrays is desired, as indicated by a nonzero value of variable INT in the VERIFY section, it is produced by subroutine VERIFY. The problem specification is produced when the VERIFY section is processed and variable INP is nonzero.

Any number of the lower or upper bounds of the rows of the matrix expression $\overline{YU} \leq \dots \leq \overline{YL}$ may be varied. Appendix I contains details of how this is specified.

For each value of each varying bound the linear programming problem is computed, punched, and printed by the subroutine sequence ELEMTP, ELEMTO, LPDATA, and PRNT. If a printout of the problem arrays is desired as indicated by a nonzero value of variable INT, it is produced by subroutine VERIFY. When the loop has been performed for each value of each varying bound, control returns to the indicator point for modifications or other instructions.

There are several additional array manipulation subroutines in PREPROC not mentioned here. These are described in Appendix III A.

2. MPS/360

Mathematical Programming System/360 is an open ended IBM software package for solving optimization problems. MPS is not a program, but a set of procedures with linking facilities. The procedures can do such things as read data, set up files, write solutions, and, of course, solve linear programming problems. The procedure linking facility is known as the control program. It consists of procedure call statements

in addition to ordinary programming facilities such as GOTO, IF, MOVE statements, etc. This control program is compiled and executed in separate OS job steps.

There are two outputs from MPS: the printed linear programming problem report and the punched problem solution.

If the punched linear programming problem output of PREPROC is interpreted, a similarity to the PREPROC input can be observed. Nonzero program variables are entered on cards with array row and column numbers and follow section identifying cards. Unlike PREPROC the alpha characters ROW, COL precede the left justified numbers. The characters are necessary because MPS identifies rows and columns of arrays with FORTRAN-like variables which must begin with an alphabetical character. ROW and COL serve to identify columns of the linear programming tableau; RHS identifies the right hand side vector and BDS identifies the variable bounds specifications.

The control program of MPS/360 for PERFORM is rather simple; the data is read in, the problem solved, and the solution written and punched. A listing and discussion of the control program is in Appendix IIIB.

Each linear programming problem produced for each value of each varying bound requires a separate MPS/360 run.

3. PSTPROC

Program PSTPROC writes the solution to the limiting performance problem using the MPS/360 linear programming problem solution and the PSTPROC report data from PREPROC.

Figure 3 is a functional flowchart of PSTPROC. First the PSTPROC report data, punched by subroutine POST in program PREPROC, is read. Next the first linear programming problem solution is read. Again it should be pointed out that no error detection facilities are in the program. If a card is dropped from the PSTPROC report specifications a linear programming solution card will take its place.

For each row of the tabulation expression, i.e., the Q1, Q2, and Q3 expression, the block inside the box is executed. For all time intervals the value of the expression is calculated and printed. If a graphical presentation of these calculations is desired, as specified by a nonzero value ITR(I) where I is the row number in Q1, Q2, Q3 matrix expression, subroutine TRAJ is called.

After all the tabulation expressions have been procured

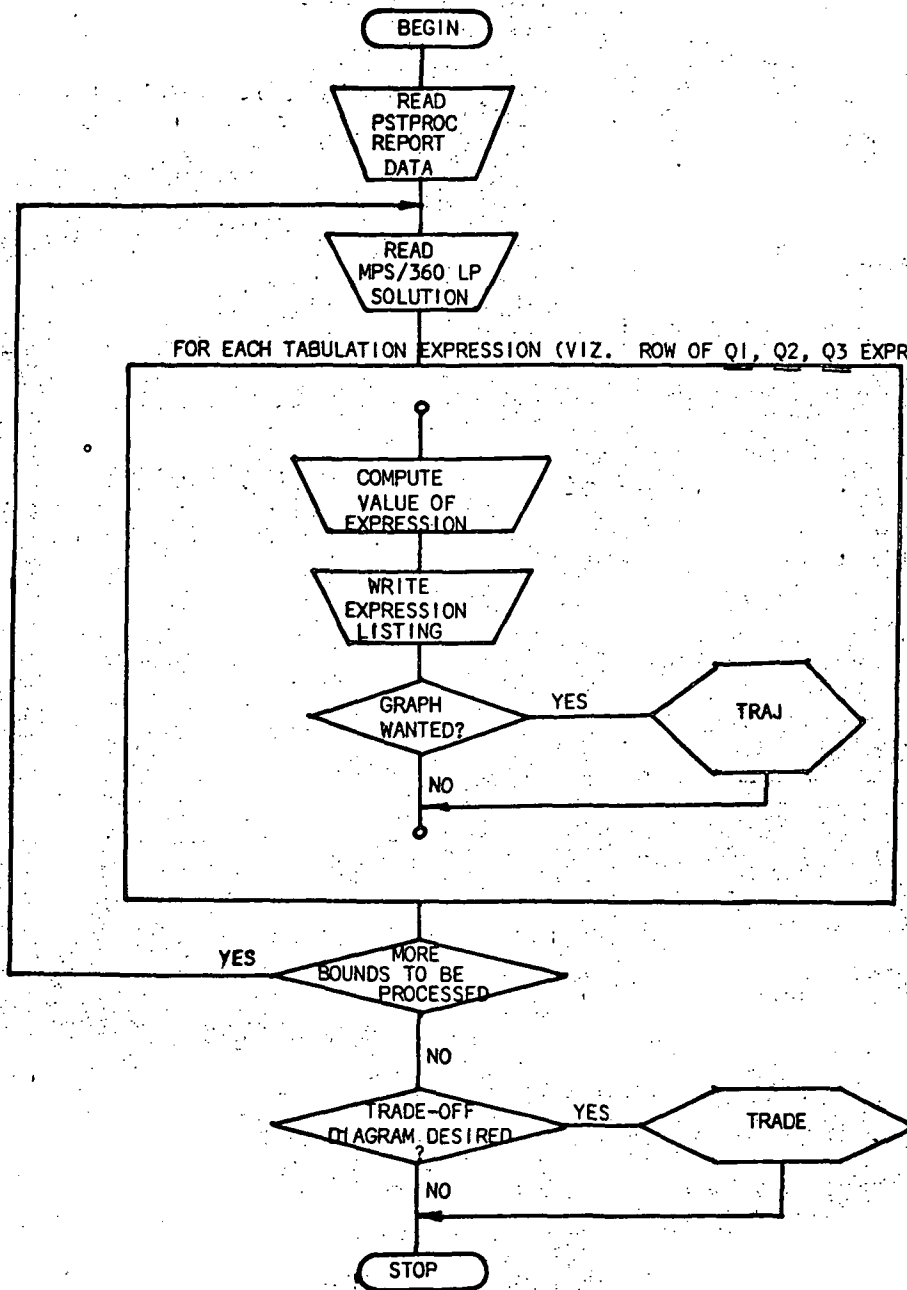


Fig. 3. PSTPROC Main Section, Functional Flow Chart

the next linear programming solution is read and the calculation loop is repeated. If all solutions have been processed variable ITD is checked.

If ITD is nonzero, a trade-off diagram is printed by subroutine TRADE.

After the trade-off diagram is produced processing stops. Note that PSTPROC handles only one problem a run; different problems, with different PSTPROC report decks, require separate runs.

SECTION IV

APPLICATIONS

A. Single-Degree-of-Freedom Shock Isolation System

We begin the applications of PERFORM by considering a single-degree-of-freedom (SDF) dynamic system subject to transient loading. Since this system has been thoroughly explored elsewhere (e.g., Ref. 1), it is included here only to demonstrate the use of PERFORM in the study of the limiting performance of a familiar system.

Consider the SDF system together with the acceleration shock shown in Fig. 4. The equation of motion is given by

$$m\ddot{z} + u = 0 \quad (1)$$

or, for a unit mass,

$$\ddot{z} + u = 0 \quad (2)$$

with initial conditions $\dot{z}(0) = z(0) = 0$

The kinematic relations are

$$z = x + y \quad (3a)$$

$$\dot{z} = \dot{x} + \dot{y} \quad (3b)$$

$$\ddot{z} = \ddot{x} + \ddot{y} = \ddot{x} + f \quad (3c)$$

Substituting Eq(3c) into Eq(2) gives

$$\ddot{x} + u = -\ddot{y} = -f$$

$$x(0) = y(0) = 0$$

$$\dot{x}(0) = \dot{y}(0) = 0$$

Suppose we wish to find the lowest possible peak acceleration of the mass (\ddot{z}) if the relative displacement between the mass and the base is constrained. The function $u(t)$ is the system controller or the isolator function. Thus, we wish to find $u(t)$ such that the maximum acceleration of the mass

$$\phi = \max |\ddot{z}| = \max |u|$$

is minimized while the relative displacement satisfies the constraint

$$|x| \leq A$$

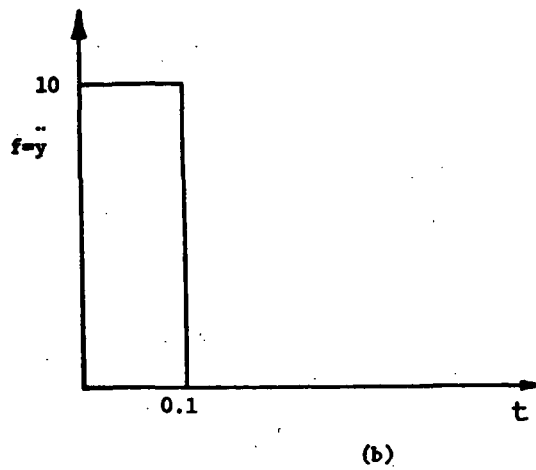
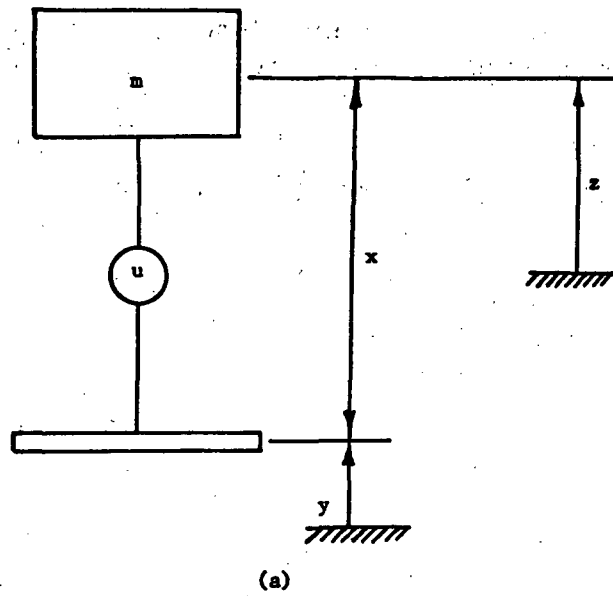


Fig. 4 A SDF System with Acceleration Shock Input

We seek the trade-off between minimum ϕ and a range of values of A. The design value of this information is discussed in Ref. 1.

Specifically, we choose to compute $\min \phi$ for $A = 0.01$, 0.02 , and 0.03 .

The formulation of the problem in the PERFORM format follows. The notation is defined in Appendix I.

1. Equations of Motion ($\ddot{x} + u = -f$)

$$\underline{M}\ddot{\underline{q}} + \underline{C}\dot{\underline{q}} + \underline{K}\underline{q} + \underline{U}\underline{u} = \underline{F}\bar{f}_k$$

where

$$\underline{M} = [1]$$

$$\underline{C} = [0]$$

$$\underline{K} = [0]$$

$$\underline{U} = [1]$$

$$\underline{F} = [-1]$$

$$\underline{q} = [x]$$

$$\dot{\underline{q}} = [\dot{x}]$$

$$\ddot{\underline{q}} = [\ddot{x}]$$

$$\underline{u} = [u]$$

$$\bar{f}_k = [\ddot{y}] = [f]$$

2. Forcing Function (Fig. 4b)

$$f(1,j,1) = 10.0 \text{ for } j = 1 \text{ to } 5$$

$$f(1,j,1) = 0 \text{ for } j = 6 \text{ to } 9$$

where the first index 1 designates that this is the first (and the only) set of forcing functions, j = discrete time, the last index 1 indicates the first component in forcing function set No. 1.

3. Objective Function (ϕ)

$$\underline{PX1} \bar{s} + \underline{PX2} \underline{u} + \underline{PX3} \bar{f}_k$$

where

$$\underline{PX1} = [0 \ 0]$$

$$\underline{\bar{s}} = \begin{bmatrix} \dot{x} \\ x \end{bmatrix}$$

$$\underline{PX2} = [1]$$

$$\underline{PX3} = [0]$$

4. Constraints ($|x| < A$)

$$\underline{\bar{Y}L} < \underline{Y1}\underline{\bar{s}} + \underline{Y2}\underline{\bar{u}} + \underline{Y3}\underline{\bar{f}}_k < \underline{\bar{Y}U}$$

where

$$\underline{Y1} = [0 \ 1]$$

$$\underline{Y2} = [0]$$

$$\underline{Y3} = [0]$$

Since the constraint is for all time and of (\leq) type we set

$$MSP(1,1) = 0$$

$$MSP(1,2) = 0$$

To obtain a trade-off diagram the value of A is varied.
Thus

$$\underline{\bar{Y}U} = A_{01} + n\Delta A_1$$

$$\underline{\bar{Y}L} = A_{02} + n\Delta A_2$$

where

$$A_{01} = SVA1 = 0.1$$

$$A_{02} = SVA2 = -0.1$$

$$\Delta A_1 = 0.1$$

$$\Delta A_2 = -0.1$$

$$n = 1 \text{ to NIC}$$

5. Output

The time trajectory of u is obtained using the output matrix

$$\underline{Q1}\bar{s} + \underline{Q2}\bar{u} + \underline{Q3}\bar{f}_k$$

$$\underline{Q1} = [0 \ 0]$$

$$\underline{Q2} = [1]$$

$$\underline{Q3} = [0]$$

6. Other Data Pertinent to This Problem

We set

$$\text{NOE} = 2$$

$$\text{MODE} = 1$$

$$\text{NDF} = 1$$

$$\text{NU} = 1$$

$$\text{NF} = 1$$

$$\text{NSETS} = 1$$

$$\text{II} = 10$$

$$\text{TM} = 0.02$$

$$\text{NOB} = 1$$

$$\text{NOC} = 1$$

$$\text{ISP} = 0$$

$$\text{NOT} = 1 \text{ (here we assume only one output is required)}$$

and

$$\text{ISET}(1) = 1$$

The whole input deck is shown in Fig. 5.

1 SINGLE-DEGREE-OF-FREEDOM SYSTEM
2 0 1 1 1 10 0.02 1 1 0 3

M MATRIX

1 1 1 1.0

F MATRIX

1 1 1 -1.0

U MATRIX

1 1 1 1.0

FORCING FUNCTION

1 1 1 0

0 1 1 10.0

0 2 10.0

0 3 10.0

0 4 10.0

1 5 10.0

PX2 MATRIX

1 1 1 1.0

Y1 MATRIX

1 1 2 1.0

BOUNDS OF CONSTRAINT

1 1 0 0

0 0.01 2 0.01

-0.01 2 -0.01

Q2 MATRIX

1 1 1 1.0

TRAJECTORY

0 1 1

0 2 1

1 3 1

TRADE OFF DIAGRAM

1 1

VERIFY

1 1

FINISH INPUT DATA

STOP

Fig. 5. Input Deck of SDF System

7. Results

Figures 6a through 6g show the output of PERFORM resulting from the input deck of Fig. 5. These are the time trajectories of the control forces \mathbf{u} (Figs. 6a to 6f) and a diagram (Fig. 6g) indicating the performance trade-off between minimum ϕ the objective function, and A , the bound of the constraint.

$$TB = Q1 \cdot S + Q2 \cdot U + Q3 \cdot F$$

WHERE

$$Q1 = 0.00 \quad 0.00$$

$$Q2 = 1.00$$

$$Q3 = 0.00$$

TIME INTERVAL		TB
0.000 TO	.020	-8.333333
.020 TO	.040	-8.333333
.040 TO	.060	-8.333333
.060 TO	.080	-8.333333
.080 TO	.100	-8.333333
.100 TO	.120	-8.333333
.120 TO	.140	-8.333333
.140 TO	.160	0.000000
.160 TO	.180	0.000000

Fig. 6a. Trajectory of $u(t)$ for $|x| \leq 0.01$.

$$TB = Q1 \cdot S + Q2 \cdot U + Q3 \cdot F$$

WHERE

$$Q1 = 0.00 \quad 0.00$$

$$Q2 = 1.00$$

$$Q3 = 0.00$$

TIME INTERVAL		TB
0.000 TO	.020	-7.142857
.020 TO	.040	-7.142857
.040 TO	.060	-7.142857
.060 TO	.080	-7.142857
.080 TO	.100	-7.142857
.100 TO	.120	-7.142857
.120 TO	.140	-7.142857
.140 TO	.160	0.000000
.160 TO	.180	0.000000

Fig. 6b. Trajectory of $u(t)$ for $|x| \leq 0.02$.

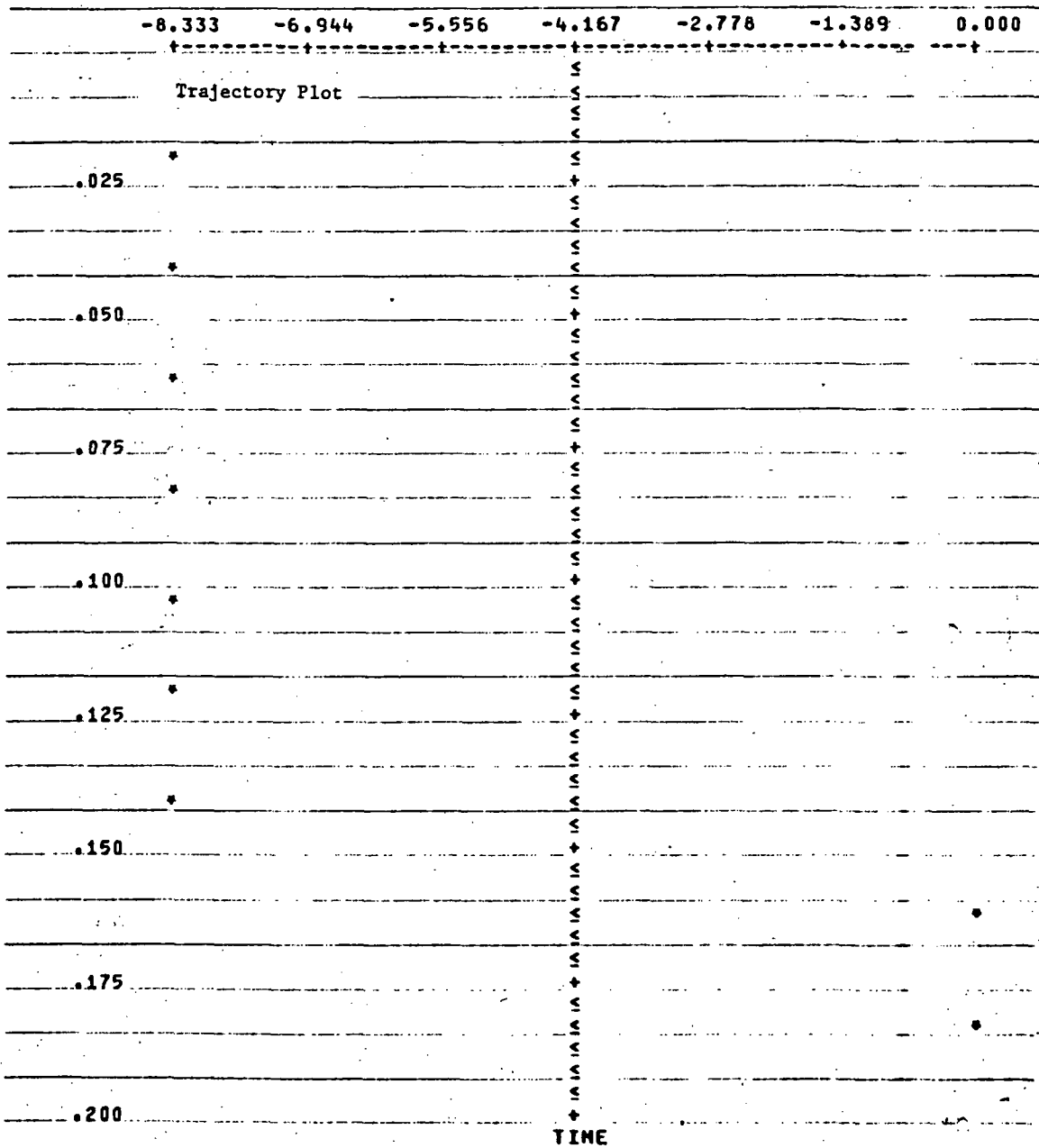


Fig. 6c. Plot of $u(t)$ for $|x| \leq 0.01$.

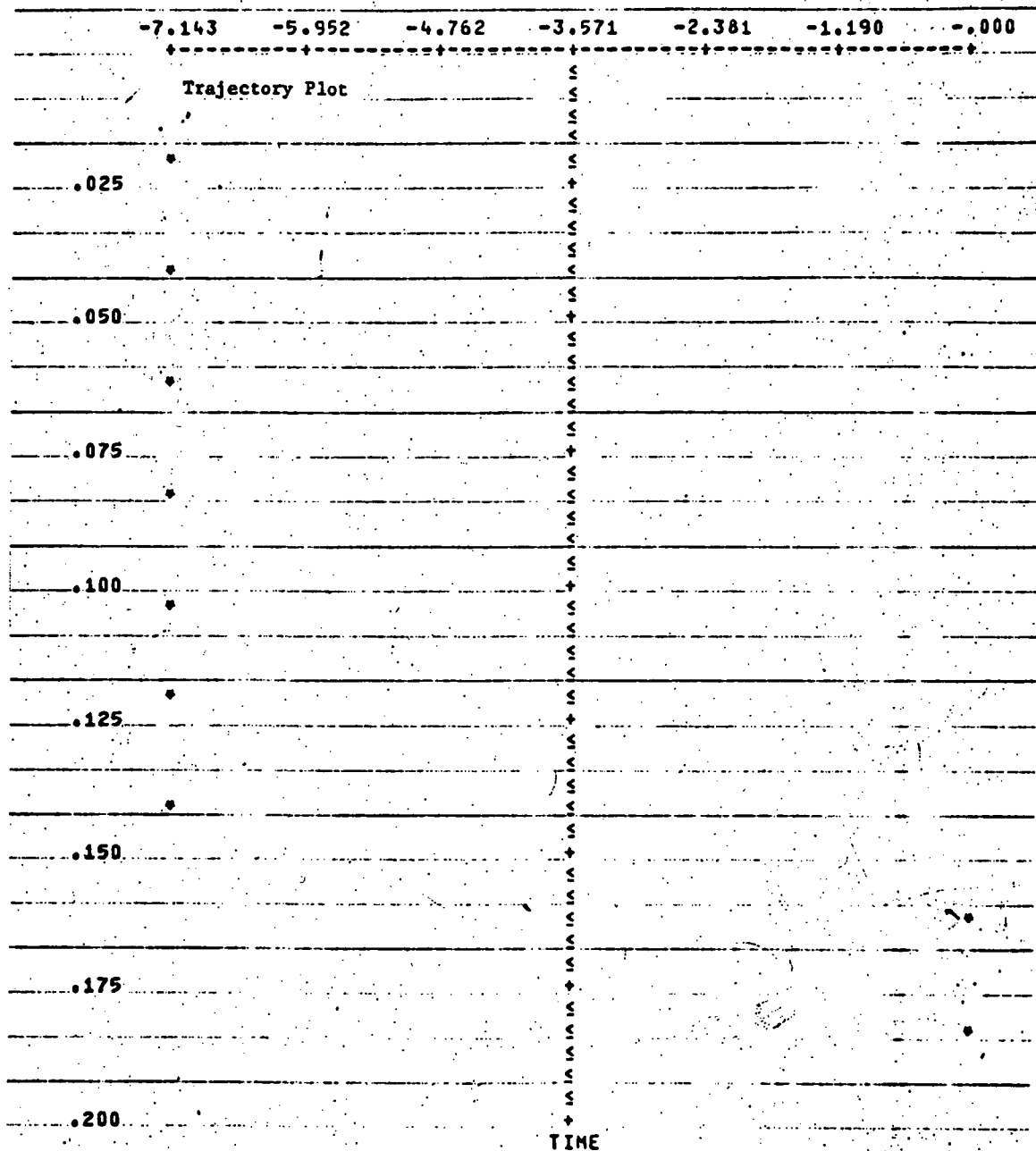


Fig. 6d. Plot of $u(t)$ for $|x| \leq 0.02$.

$$TB = Q1 \cdot S + Q2 \cdot U + Q3 \cdot F$$

WHERE

$$Q1 = 0.00 \quad 0.00$$

$$Q2 = 1.00$$

$$Q3 = 0.00$$

TIME INTERVAL

TB

0.000 TO	.020	-6.250000
.020 TO	.040	-6.250000
.040 TO	.060	-6.250000
.060 TO	.080	-6.250000
.080 TO	.100	-6.250000
.100 TO	.120	-6.250000
.120 TO	.140	-6.250000
.140 TO	.160	-6.250000
.160 TO	.180	0.000000

Fig. 6e. Trajectory of $u(t)$ for $|x| \leq 0.03$.

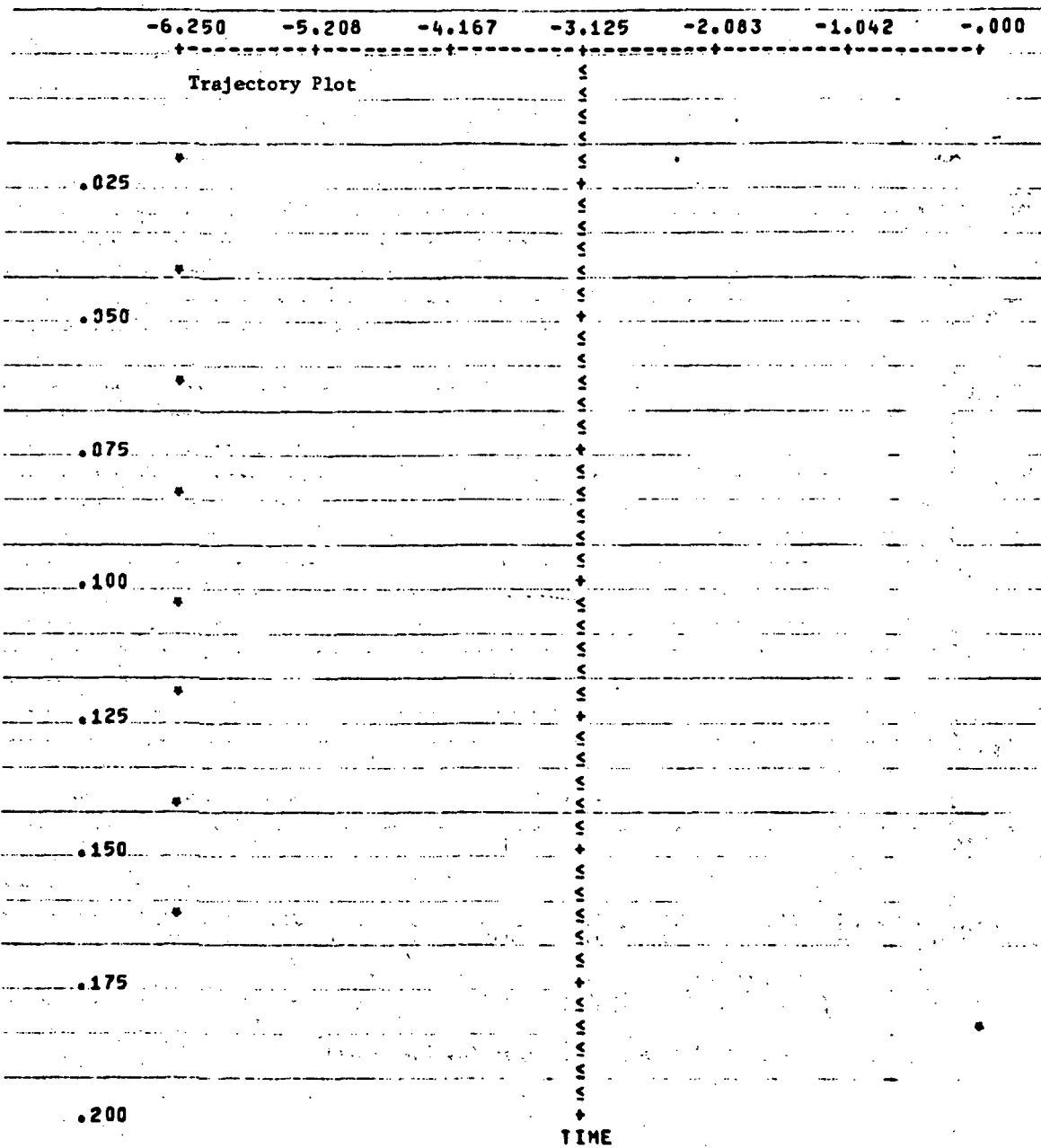


Fig. 6f. Plot of $u(t)$ for $|x| \leq 0.03$.

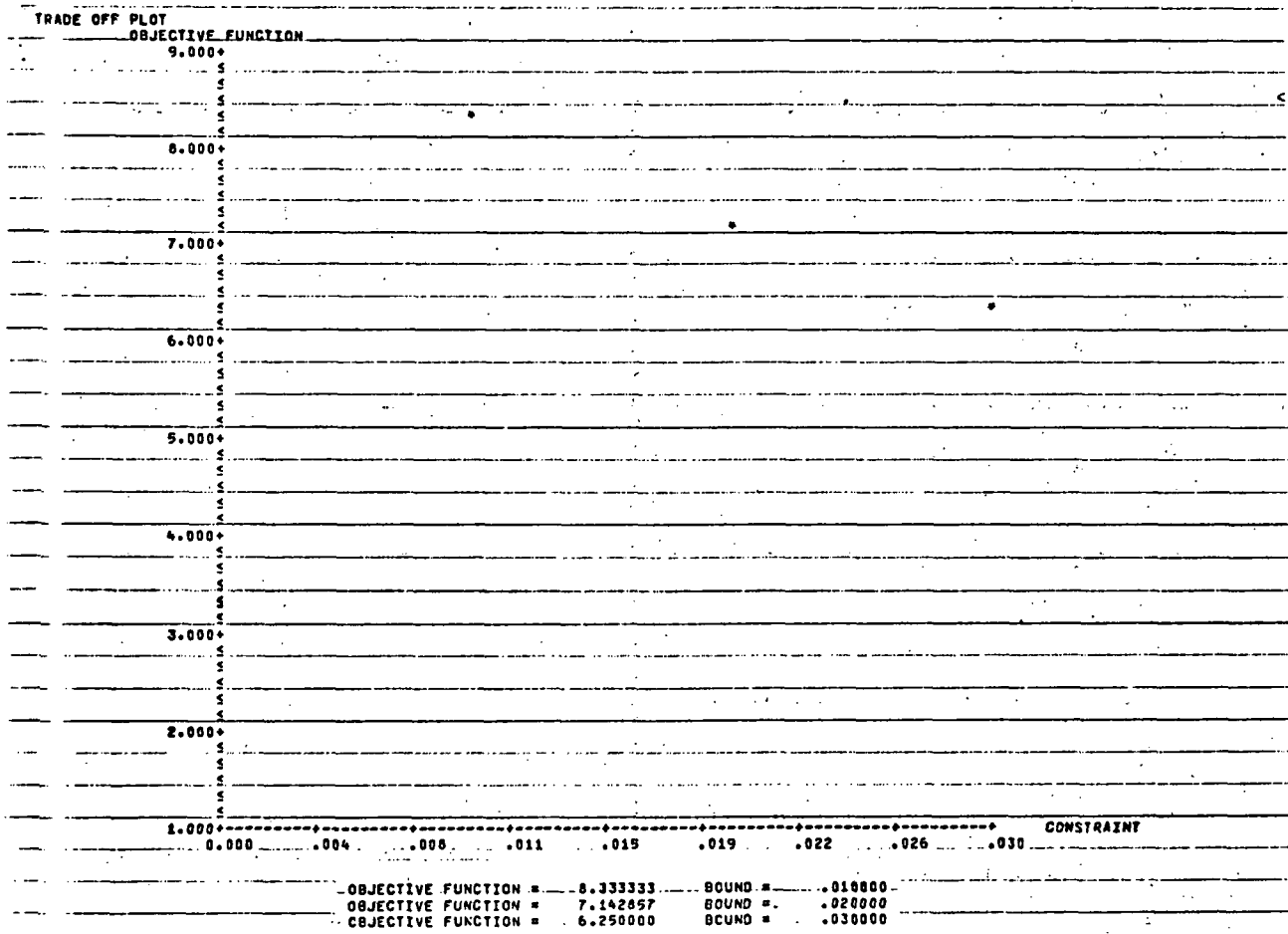


Fig. 6g. Trade-off Diagram for SDF System

B. Multi-Degree-of-Freedom Shock Isolation Systems

To use PERFORM in evaluating the limiting performance characteristics of a shock isolation system the equations of motion of the system, after the control forces are introduced, must be linear. However, many dynamic systems are described by nonlinear equations and we are invariably faced with the problem of approximating the systems with various assumptions and yet not losing sight of the actual system. In this section, in addition to treating some multi-degree-of-freedom shock isolation systems, we will consider some of the reasonable assumptions to be made for the linearization of the equations of motion for some dynamic systems of nonlinear nature.

1. Klein's Three-Degree-of-Freedom System

a. Problem Description

In Ref. 2 a three-degree-of-freedom system as depicted in Fig. 7 was considered. The model to be analyzed has the z_1, z_2 plane as a plane of symmetry. It is assumed that the mass is a rigid body; that principal axes of inertia through the mass center parallel the edges of the body; and that the motion of the mass will not affect the motion of the base. In addition, it is assumed that the points of application of the shock isolator forces u_1, u_2, u_3 and u_4 remain fixed at the corners of the supported mass and retain their horizontal and vertical directions despite the motions of the base and mass. The kinematic conditions of the system are shown in Fig. 7, to which the following definitions apply:

u_i = the shock isolators or control forces which are to be optimized,

y_i = the two orthogonal input motions of the base referred to a fixed reference frame,

z_i = the two orthogonal motions of the center of mass relative to a fixed reference frame,

θ = rigid body rotation of the isolated mass about the center of mass.

The equations of motion for the system shown in Fig. 7 become:

$$\begin{aligned} m\ddot{z}_1 - u_1 + u_4 &= 0 \\ m\ddot{z}_2 - u_2 - u_3 &= 0 \end{aligned} \tag{4}$$

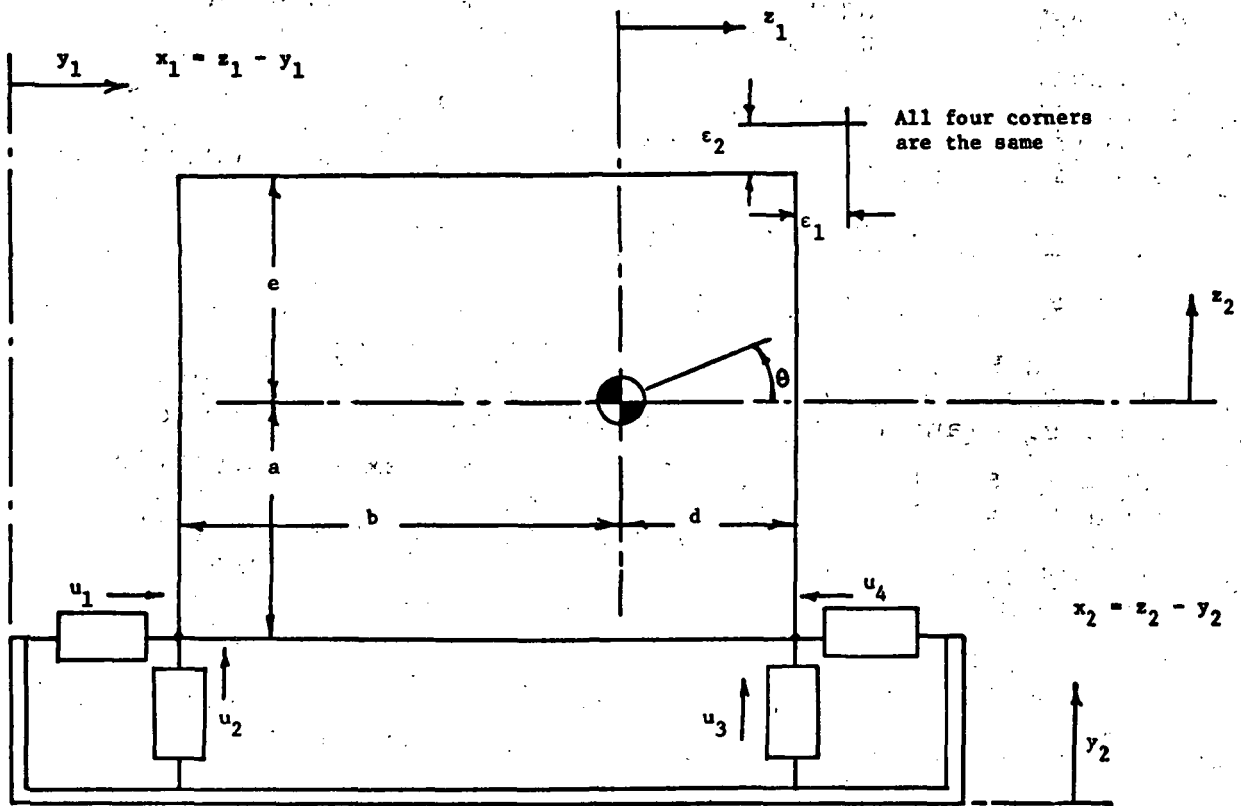


Fig. 7 Active Isolation System Used in Ref. 2

$$I\ddot{\theta} - au_1 \cos \theta + bu_2 \cos \theta - du_3 \cos \theta + au_4 \cos \theta = 0 \quad (4c)$$

where m is the isolated mass and I is the moment of inertia of the isolated mass about its center of mass.

It is further assumed in Ref. 2 that θ is small, therefore allowing the usual small angle approximations to be made. Using the kinematic relations

$$z_1 = x_1 + y_1, \quad \ddot{z}_1 = \ddot{x}_1 + \ddot{y}_1$$

$$z_2 = x_2 + y_2, \quad \ddot{z}_2 = \ddot{x}_2 + \ddot{y}_2$$

Eq. (4) becomes

$$m\ddot{x}_1 - u_1 + u_4 = -m\ddot{y}_1$$

$$m\ddot{x}_2 - u_2 - u_3 = -m\ddot{y}_2 \quad (5)$$

$$I\ddot{\theta} - au_1 + bu_2 - du_3 + au_4 = 0$$

Letting $I = m\rho^2$, where ρ is the radius of gyration, we find for unit mass

$$\ddot{x}_1 - u_1 + u_4 = -\ddot{y}_1$$

$$\ddot{x}_2 - u_2 - u_3 = -\ddot{y}_2 \quad (6)$$

$$\ddot{\theta} - \frac{au_1}{\rho^2} + \frac{bu_2}{\rho^2} - \frac{du_3}{\rho^2} + \frac{au_4}{\rho^2} = 0$$

The above equations define the behavior of the isolated mass as a function of the applied accelerations \ddot{y}_1 and \ddot{y}_2 and the control forces u_1, u_2, u_3 , and u_4 .

For this linearized system the optimization problem considered in Ref. 2 is: Find the control functions $u_1(t), u_2(t), u_3(t)$ and $u_4(t)$ so as to minimize some function of the maximum absolute values of the response acceleration, $f(|\ddot{z}_1|_{\max}, |\ddot{z}_2|_{\max}, |\ddot{\theta}|_{\max})$ when the base is subjected to input \ddot{y}_1 and/or \ddot{y}_2 and the mass is constrained to move within the rattlespaces defined by ϵ_1 and ϵ_2 as shown in Fig. 7.

Since linear programming is selected as a solution technique, the objective function and constraints must be expressible as linear combinations of control forces. The objective function chosen was

$$\Phi = \max \{ \max |w_1(t)|, \max |w_2(t)|, \max |w_3(t)| \} \quad (7)$$

$$\text{where } w_1 = \alpha_1 (u_1 - u_4) = \alpha_1 \ddot{z}_1$$

$$w_2 = \alpha_2 (u_2 + u_3) = \alpha_1 \ddot{z}_2 \quad (8)$$

$$w_3 = \frac{a}{\rho^2} u_1 - \frac{b}{\rho^2} u_2 + \frac{d}{\rho^2} u_3 - \frac{a}{\rho^2} u_4 = \ddot{\theta}$$

with α_1, α_2 as weighting constants.

The constraints are

$$\begin{aligned} |x_1 + a\theta| &\leq \epsilon_1 \\ |x_1 - e\theta| &\leq \epsilon_1 \\ |x_2 - b\theta| &\leq \epsilon_2 \\ |x_2 + d\theta| &\leq \epsilon_2 \end{aligned} \quad (9)$$

The forcing function considered was

$$y(t) = t^2 e^{-t} \quad (10)$$

This gives an acceleration

$$\ddot{y}(t) = e^{-t} (t^2 - 4t + 2) \quad (11)$$

To compare the use of PERFORM with results available in Ref. 2, the forcing function is chosen to act in the y_1 direction only. Other pertinent data include:

No. of time intervals = 40

$$\alpha_1 = 1.0$$

$$\alpha_2 = 1.0$$

$$\epsilon_1 = 0.1$$

$$\epsilon_2 = 0.0$$

$$a = 0.0$$

$$b = 25.0$$

$$d = 25.0$$

$$e = 0.0$$

b. Formulation in PERFORM Format

The Ref. 2 example outlined above will now be reformulated in accordance with the PERFORM format. Since the forcing function acts in the y_1 direction, u_2 and u_3 will be inactive, as will w_2 . Hence only two functions will be included in the objective² function. Due to $\epsilon_2 = 0$, only the constraints on x_1 will be taken into account.

Equations of Motion

Using the definitions for w_1 , w_2 , and w_3 as given in Eq. (8) and the values of the constraints as defined above, the equations of motion can be written as

$$\begin{aligned}\ddot{x}_1 - w_1 &= -\ddot{y}_1 \\ \ddot{x}_2 - w_2 &= 0 \\ \ddot{\theta} - w_3 &= 0\end{aligned}\tag{12}$$

Eq. (12) may be rewritten in the PERFORM format as

$$\underline{M}\ddot{\underline{q}} + \underline{C}\dot{\underline{q}} + \underline{K}\underline{q} + \underline{U}\underline{u} = \underline{F}\underline{\bar{f}}_k\tag{13}$$

where the vectors are defined as

$$\begin{aligned}\underline{\bar{q}} &= \begin{bmatrix} x_1 \\ x_2 \\ \theta \end{bmatrix} & \dot{\underline{\bar{q}}} &= \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{\theta} \end{bmatrix} & \ddot{\underline{\bar{q}}} &= \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \\ \ddot{\theta} \end{bmatrix} \\ \underline{\bar{f}}_k &= [\ddot{y}_1]\end{aligned}$$

$$\bar{u} = \begin{bmatrix} w_1 \\ w_2 \\ w_3 \end{bmatrix}$$

and the coefficient matrices as

$$\underline{M} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\underline{C} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\underline{K} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\underline{U} = \begin{bmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -1 \end{bmatrix}$$

$$\underline{F} = \begin{bmatrix} -1 \\ 0 \\ 0 \end{bmatrix}$$

Objective Function

The objective function given by Eq. (7) is to be minimized. In the PERFORM input format the objective function becomes

$$\underline{PX1}\bar{s} + \underline{PX2}\bar{u} + \underline{PX3}\bar{f}_k \quad (14)$$

where

$$\dot{\underline{s}} = \begin{bmatrix} \dot{q} \\ \dot{q} \end{bmatrix} = \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{\theta} \\ x_1 \\ x_2 \\ \theta \end{bmatrix}$$

and

$$\underline{PX1} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$\underline{PX2} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\underline{PX3} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

Constraints

The constraint is given on the relative displacements as

$$|x_1| \leq \epsilon_1 \quad \text{or}$$

$$-\epsilon_1 \leq x_1 \leq \epsilon_1$$

In the PERFORM format this becomes

$$\overline{YL} \leq \underline{Y1} \, \bar{s} + \underline{Y2} \, \bar{u} + \underline{Y3} \, \bar{f}_k \leq \overline{YU} \quad (15)$$

where

$$\overline{YL} = [-\epsilon_1] = [-0.1]$$

$$\overline{YU} = [\epsilon_1] = [0.1]$$

$$\underline{y_1} = [0 \ 0 \ 0 \ 1 \ 0 \ 0]$$

$$\underline{y_2} = [0 \ 0 \ 0]$$

$$\underline{y_3} = [0]$$

The input deck is shown in Fig. 8.

c. Comparison of Results

The results obtained by using a linear programming optimization procedure for this case given in Ref. 2 are duplicated in Table 1. The results of the same problem solved by PERFORM are given in Table 2a. The values of the objective function from these two solutions are very close to each other. The tabulated output from PERFORM is the w_1 in Ref. 2. Using the values of u_1 and u_4 from Table 1, the w_1 calculated from Eqs. (8) are about the same as those given by PERFORM for the first five time intervals. A comparison of the w_1 values for the first 10 time intervals is given in Table 2b.¹ Since the solution of the optimization problem is not unique after the maximum value of the objective function has been reached, it is not surprising that Table 1 and Table 2a do not agree consistently at later times.

d. Modified System

Based on certain assumptions, the above system can be modified to include large rotations. Additional isolator forces u_α and u_β can be introduced for rotational motion of the isolated mass, and rotational contributions of horizontal and vertical isolator forces can be neglected (i.e., omission of all but $\ddot{\theta}$ in the third of Eqs. (6)). The equations of motion for the system shown in Fig. 9 are written as

$$\begin{aligned}\ddot{x}_1 - u_1 + u_4 &= -\ddot{y}_1 \\ \ddot{x}_2 - u_2 - u_3 &= -\ddot{y}_2 \\ \ddot{\theta} + u_\alpha + u_\beta &= 0\end{aligned}\tag{16}$$

Eqs. (16) are applicable to the case where θ is not necessarily small.

2. Missile-Silo Isolation

Next we consider another problem which is quite similar to the one discussed in Ref. 2 but has a different arrange-

```

2      MULTI-DEGREE-OF-FREEDOM SYSTEM
2      0      3      3      1      1      41      0.15      2      1      0      1
1
M MATRIX
1      1      1.
2      2      1.
3      3      1.
U MATRIX
1      1      -1.
2      2      -1.
3      3      -1.
F MATRIX
1      1      1      -1.0
PX2 MATRIX
0      1      1      1.0
1      2      2      1.0
Y1 MATRIX
1      1      4      1.0
FORCING FUNCTION
1      1
1      1      0
1      1.612179
2      0.941843
3      0.457987
4      0.117346
5      -0.114306
6      -0.263925
7      -0.352623
8      -0.396840
9      -0.409288
10     -0.399715
11     -0.375526
12     -0.342280
13     -0.304089
14     -0.263940
15     -0.223950
16     -0.185566
17     -0.149732
18     -0.117012
19     -0.087688
20     -0.061842
21     -0.03941
22     -0.020233
23     -0.004090
24     0.009276
25     0.020144
26     0.028789
27     0.035481
28     0.040480
29     0.044026
30     0.046339
31     0.047618
32     0.048042
33     0.047769
34     0.046936
35     0.045664

```

Fig. 8. Input Deck for Multi-Degree-of-Freedom System

	36	0.044055
	37	0.042198
	38	0.040166
	39	0.038021
1	40	0.035815
BOUNDS OF CONSTRAINTS		
1	1	0 0
0		
	0.1	
0		
	-0.1	
Q2 MATRIX		
1	1	1 1,0
VERIFY		
1	1	
FINISH INPUT DATA		
STOP		

Fig. 8. Input Deck for Multi-degree-of-Freedom System (concluded)

DEG. NO.	TIME	U(1)	U(2)	U(3)	U(4)
1	0.	2.944257E-01	0.	0.	-2.944257E-01
2	1.500000E-01	2.944257E-01	0.	0.	-2.944257E-01
3	3.000000E-01	2.944257E-01	0.	0.	-2.944257E-01
4	4.500000E-01	2.944257E-01	0.	0.	-2.944257E-01
5	6.000000E-01	2.944257E-01	0.	0.	-2.944257E-01
6	7.500000E-01	0.	0.	0.	0.
7	9.000000E-01	-2.944257E-01	0.	0.	2.944257E-01
8	1.050000E+00	-1.727954E-01	0.	0.	1.727954E-01
9	1.200000E+00	-2.944257E-01	0.	0.	2.944257E-01
10	1.350000E+00	0.	0.	0.	0.
11	1.500000E+00	-2.944257E-01	0.	0.	2.944257E-01
12	1.650000E+00	-2.944257E-01	0.	0.	2.944257E-01
13	1.800000E+00	0.	0.	0.	0.
14	1.950000E+00	-2.246069E-01	0.	0.	2.246069E-01
15	2.100000E+00	0.	0.	0.	0.
16	2.250000E+00	-7.838257E-02	0.	0.	7.838257E-02
17	2.400000E+00	0.	0.	0.	0.
18	2.550000E+00	0.	0.	0.	0.
19	2.700000E+00	0.	0.	0.	0.
20	2.850000E+00	0.	0.	0.	0.
21	3.000000E+00	0.	0.	0.	0.
22	3.150000E+00	0.	0.	0.	0.
23	3.300000E+00	0.	0.	0.	0.
24	3.450000E+00	0.	0.	0.	0.
25	3.600000E+00	0.	0.	0.	0.
26	3.750000E+00	0.	0.	0.	0.
27	3.900000E+00	0.	0.	0.	0.
28	4.050000E+00	0.	0.	0.	0.
29	4.200000E+00	0.	0.	0.	0.
30	4.350000E+00	0.	0.	0.	0.
31	4.500000E+00	0.	0.	0.	0.
32	4.650000E+00	0.	0.	0.	0.
33	4.800000E+00	0.	0.	0.	0.
34	4.950000E+00	0.	0.	0.	0.
35	5.100000E+00	0.	0.	0.	0.
36	5.250000E+00	0.	0.	0.	0.
37	5.400000E+00	0.	0.	0.	0.
38	5.550000E+00	0.	0.	0.	0.
39	5.700000E+00	0.	0.	0.	0.
40	5.850000E+00	0.	0.	0.	0.

MAXIMUM VALUE OF CRITERION FUNCTION = 5.896513E-01

Table 1. Results of Multi-Degree-of-Freedom System given in Ref. 2.

TU= 01°S+ 02°U+ 03°F

WHERE

01= 0.00 0.00 0.00 0.00 0.00 0.00
 02= 1.00 0.00 0.00
 03= 0.00 0.00

TIME INTERVAL	TO
0.000 TO .150	.589653
.150 TO .300	.589650
.300 TO .450	.589650
.450 TO .600	.589650
.600 TO .750	.589650
.750 TO .900	.117460
.900 TO 1.050	-.589650
1.050 TO 1.200	-.589650
1.200 TO 1.350	-.589650
1.350 TO 1.500	0.000000
1.500 TO 1.650	0.000000
1.650 TO 1.800	-.589650
1.800 TO 1.950	0.000000
1.950 TO 2.100	0.000000
2.100 TO 2.250	-.176940
2.250 TO 2.400	0.000000
2.400 TO 2.550	0.000000
2.550 TO 2.700	0.000000
2.700 TO 2.850	0.000000
2.850 TO 3.000	-.589650
3.000 TO 3.150	-.589650
3.150 TO 3.300	-.589650
3.300 TO 3.450	-.159170
3.450 TO 3.600	.589650
3.600 TO 3.750	0.000000
3.750 TO 3.900	0.000000
3.900 TO 4.050	0.000000
4.050 TO 4.200	0.000000
4.200 TO 4.350	0.000000
4.350 TO 4.500	0.000000
4.500 TO 4.650	.148460
4.650 TO 4.800	0.000000
4.800 TO 4.950	0.000000
4.950 TO 5.100	0.000000
5.100 TO 5.250	0.000000
5.250 TO 5.400	.311480
5.400 TO 5.550	0.000000
5.550 TO 5.700	0.000000
5.700 TO 5.850	.008950
5.850 TO 6.000	0.000000

OBJECTIVE FUNCTION = .589653 BCUND = .100000

Table 2.a Results for Multi-Degree-of-Freedom System

i	$u_1(t_i)$	$u_4(t_i)$	$w(t_i) = u_1 - u_4$	$u(t_i)$
1	0.2948257	-0.2948257	0.5896514	0.589653
2	0.2848257	-0.2948257	0.5896514	0.583650
3	0.2948257	-0.2948257	0.5896514	0.589650
4	0.2948257	-0.2948257	0.5896514	0.589650
5	0.2948257	-0.2948257	0.5896514	0.589650
6	0.0	0.0	0.0	0.117460
7	-0.2948257	0.2948257	-0.5896514	-0.589650
8	-0.172954	0.1727954	-0.34559080	-0.589650
9	-0.2948257	0.2948257	-0.5896514	-0.589650
10	0.0	0.0	0.0	0.0

Table 2b. Comparison of Control Forces

Results obtained by Ref. 2 and those by PERFORM. u_1 and u_4 are taken from Ref. 2. u 's were computed by PERFORM.

ment of control forces. It is a problem of suspending a structure within an underground cavity so as to provide optimum shock isolation. We consider the structure to be a missile suspended in a silo in the manner shown by Fig. 10, where u_1, u_2, u_3, u_4 , and u_5 represent shock isolators to be optimized. For purposes of analysis the missile is viewed as a rigid body capable of three modes of in-plane motion, two orthogonal translations and one rotation. The silo is assumed to be disturbed by a shock pulse, resulting in an in-plane motion of the silo enclosure. This motion can be decomposed into two orthogonal input motions, one vertical and one horizontal component. Consider Fig. 11, in which the notation is the same as that used in Fig. 7 except that β_i = angles of deviation of shock isolators from the original preshock directions.

The equations of motion are

$$\begin{aligned}
 m\ddot{z}_1 + u_5 \sin \beta_5 + \sum_{i=1}^4 u_i \cos \beta_i &= 0 \\
 m\ddot{z}_2 + u_5 \cos \beta_5 + \sum_{i=1}^4 u_i \sin \beta_i &= 0 \\
 I\ddot{\theta} + u_5 h_2 \sin (\beta_5 + \theta) \\
 + u_1 L_1 [\cos (\beta_1 - \theta) - \frac{d}{2L_1} \sin (\beta_1 - \theta)] \\
 - u_2 L_2 [\cos (\beta_2 - \theta) + \frac{d}{2L_2} \sin (\beta_2 - \theta)] \\
 + u_3 L_1 [\cos (\beta_3 + \theta) - \frac{d}{2L_1} \sin (\beta_3 + \theta)] \\
 - u_4 L_2 [\cos (\beta_4 + \theta) + \frac{d}{2L_2} \sin (\beta_4 + \theta)] &= 0
 \end{aligned} \tag{17}$$

where m is the total mass of the missile and I is the moment of inertia of the missile. Since β_i are functions of z_1, z_2, y_1, y_2 , the terms such as $\beta_i u_i$ in the above equations are nonlinear.

Now assume, as in the previous section, that the isolator forces retain their horizontal or vertical directions despite the motions of the base and mass. Again, assume the θ is small, and in addition assume β_i is small. Then the equations of motion are rewritten as

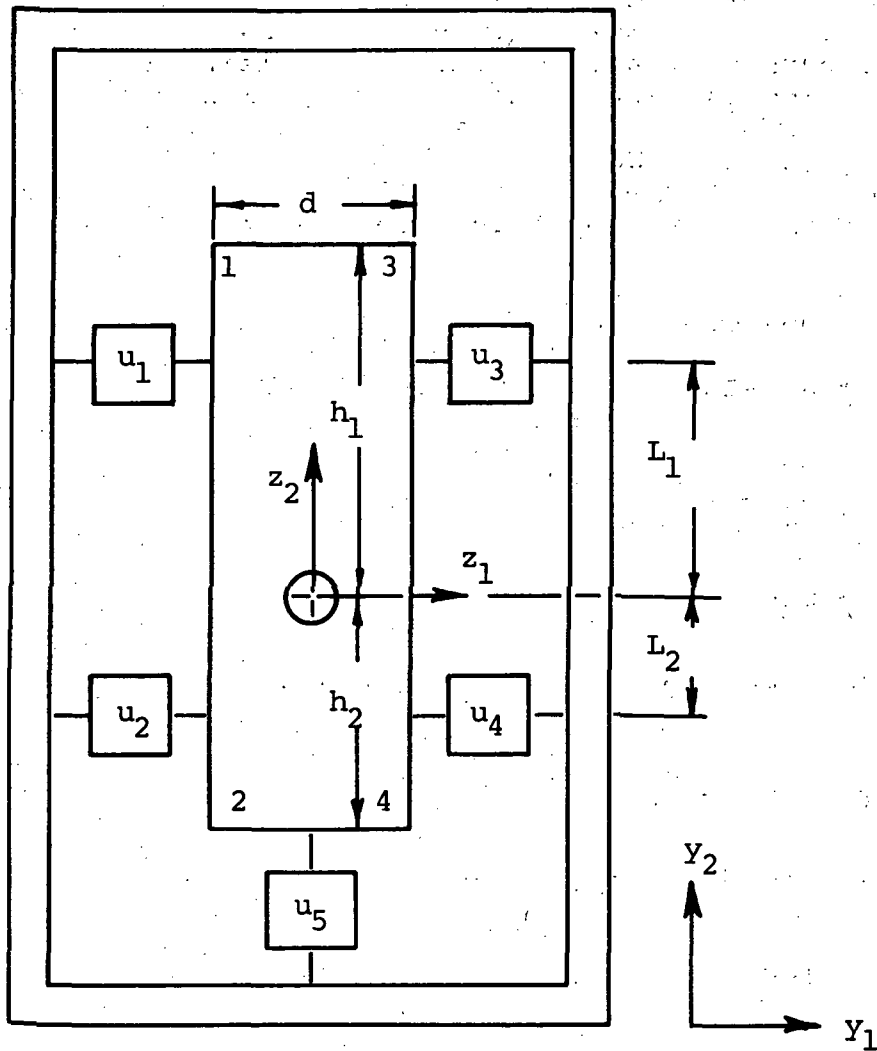


Fig 10. Model Representing the In-Plane Three-Degree-of Freedom Silo-Missile System

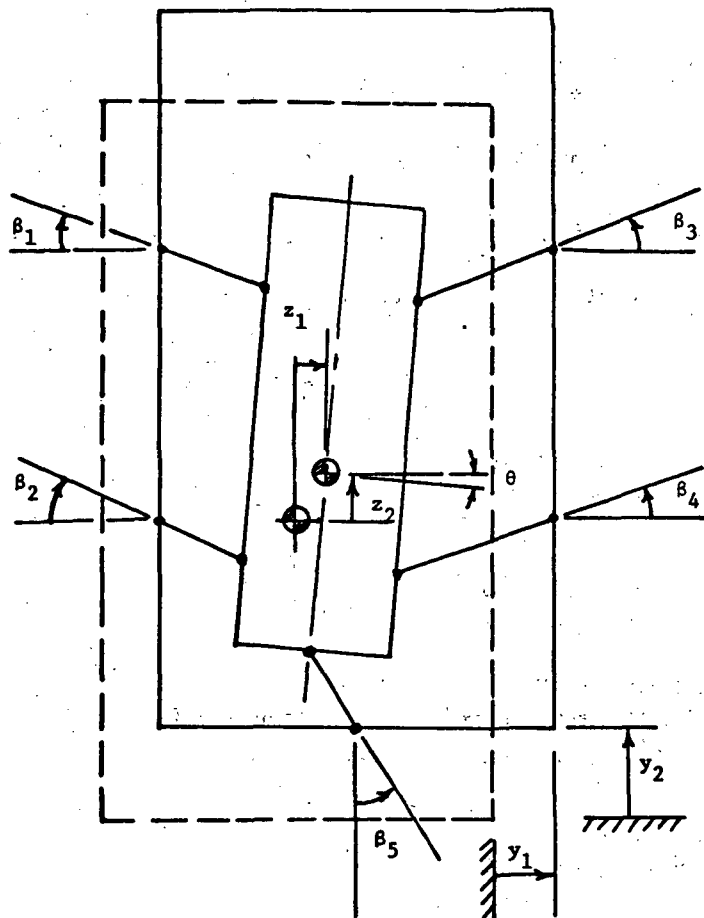


Fig. 11 Kinematics of the Three-Degree-of-Freedom Model

$$m\ddot{z}_1 + \sum_{i=1}^4 u_i = 0$$

$$m\ddot{z}_2 + u_5 = 0 \quad (18)$$

$$I\ddot{\theta} + u_1 L_1 - u_2 L_2 + u_3 L_1 - u_4 L_2 = 0$$

The relations

$$z_1 = x_1 + y_1, \quad \dot{z}_1 = \dot{x}_1 + \dot{y}_1, \quad \ddot{z}_1 = \ddot{x}_1 + \ddot{y}_1$$

$$z_2 = x_2 + y_2, \quad \dot{z}_2 = \dot{x}_2 + \dot{y}_2, \quad \ddot{z}_2 = \ddot{x}_2 + \ddot{y}_2$$

and $I = m\rho^2$ substituted in Eq. (16) yield, for unit mass,

$$\ddot{x}_1 + u_1 + u_2 + u_3 + u_4 = -\ddot{y}_1$$

$$\ddot{x}_2 + u_5 = -\ddot{y}_2 \quad (19)$$

$$\ddot{\theta} + \frac{u_1 L_1}{\rho^2} - \frac{u_2 L_2}{\rho^2} + \frac{u_3 L_1}{\rho^2} - \frac{u_4 L_2}{\rho^2} = 0$$

The above equations are all linear and in the desired form for PERFORM input format.

With additional control forces $u_{\alpha 1}$, $u_{\alpha 2}$, $u_{\alpha 3}$, and $u_{\alpha 4}$ shown in Fig. 12 and neglecting the contribution of u_1 , u_2 , u_3 , and u_4 to rotational motion, the equations of motion can be written as

$$\ddot{x}_1 + u_1 + u_2 + u_3 + u_4 = -\ddot{y}_1$$

$$\ddot{y}_2 + u_5 = -\ddot{y}_2 \quad (20)$$

$$\ddot{\theta} + \frac{u_{\alpha 1}}{\rho^2} + \frac{u_{\alpha 2}}{\rho^2} + \frac{u_{\alpha 3}}{\rho^2} + \frac{u_{\alpha 4}}{\rho^2} = 0$$

Again we have equations of motion in the desired form for the PERFORM input format and the equations are applicable where θ and β_i are not necessarily small.

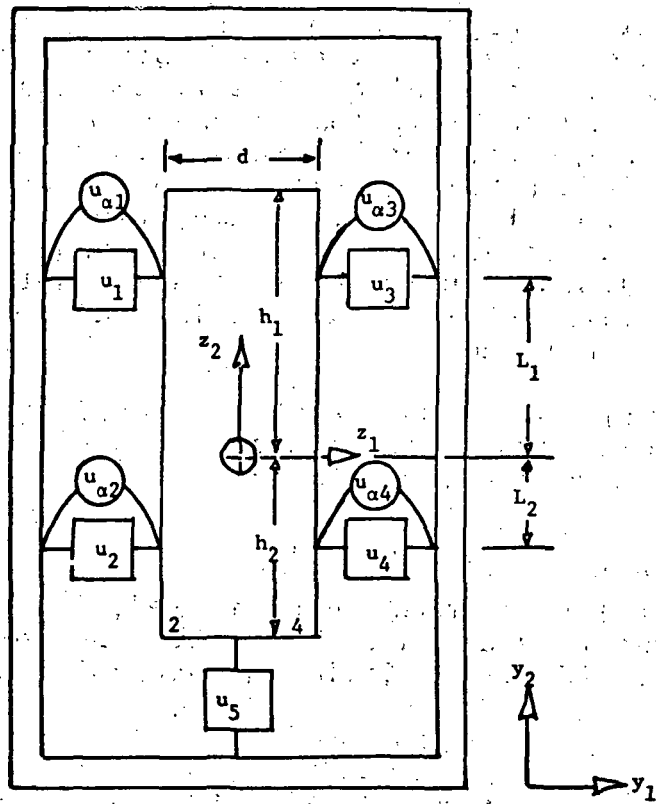


Fig. 12 Modified Silo-Missile System

C. Train Suspension Model

The proper design of the wheel-to-car (or truck) suspension mechanism is essential to the successful operation of a high speed rail passenger car. Simplified vertical and lateral dynamic models of a high speed railroad car have been developed and a trial-and-error optimization procedure has been applied to determine the optimum stiffness and damping properties of the suspension systems in Ref. 3.

The mathematical models used were a four-degree-of-freedom model for vertical responses to vertical inputs and a ten-degree-of-freedom model for lateral responses to lateral or rolling inputs from the rails. The linear equations of motion were solved by digital computer programs for sinusoidal inputs to both models and for one random input to the vertical model. To include nonlinearities in the lateral truck suspension system, a real-time digital simulation computer program was developed and utilized. Both linear and nonlinear acceleration responses to sinusoidal, transient deterministic, and random inputs were obtained for the lateral model by means of this simulation program.

In this work we formulate the application of the computer system PERFORM in evaluating the limiting performance of the lateral train model, subject to transient inputs.

1. Description of the System

The lateral train model used in Ref. 3 is a ten degree-of-freedom system as shown in Fig. 13. The motion of this model is described by the following generalized coordinates:

- $b(t)$ - car lateral bending
- $y_c(t)$ - car lateral rigid-body translation
- $\theta_{co}(t)$ - car rigid body roll
- $\theta_{cl}(t)$ - car torsion
- $\eta(t)$ - car rigid-body yaw
- $y_{lg}(t)$ - transformer lateral translation
- $y_{Ar}(t)$ - rear traction motor lateral translation
- $y_{Af}(t)$ - forward traction motor lateral translation

$\theta_{Ar}(t)$ - rear traction motor roll

$\theta_{Af}(t)$ - forward traction motor roll

For a limiting performance study we replace the spring and damping forces in Fig. 13 by the control or isolator forces as shown in Figs. 14 and 15. Fig. 14 represents a general case where the entire spring and damping forces of the system are replaced by eleven isolator forces. A special case of only 3 isolator forces is shown in Fig. 15. The eleven isolator forces considered are:

u_{cr} - rear lateral bolster force

u_{cf} - forward lateral bolster force

u_{sr} - rear vertical bolster force

u_{sf} - forward vertical bolster force

u_g - transformer lateral bolster force

u_{lr} - rear traction motor rolling torque

u_{lf} - forward traction motor rolling torque

u_{Ar} - rear vertical equalizer force

u_{Af} - forward vertical equalizer force

u_{or} - rear traction motor rolling torque

u_{of} - forward traction motor rolling torque

2. Operating Conditions and Objectives

The railroad car system is subjected to transient lateral and cross-level inputs which simulate the effects of a lateral deviation of the track from a straight course and the bank on a curve, respectively.

The objective is to find the isolator forces that minimize a maximum lateral acceleration of the car. Furthermore, the constraints are on the lateral deflection of the bolster springs. Thus we wish to find the unknown isolator forces such that

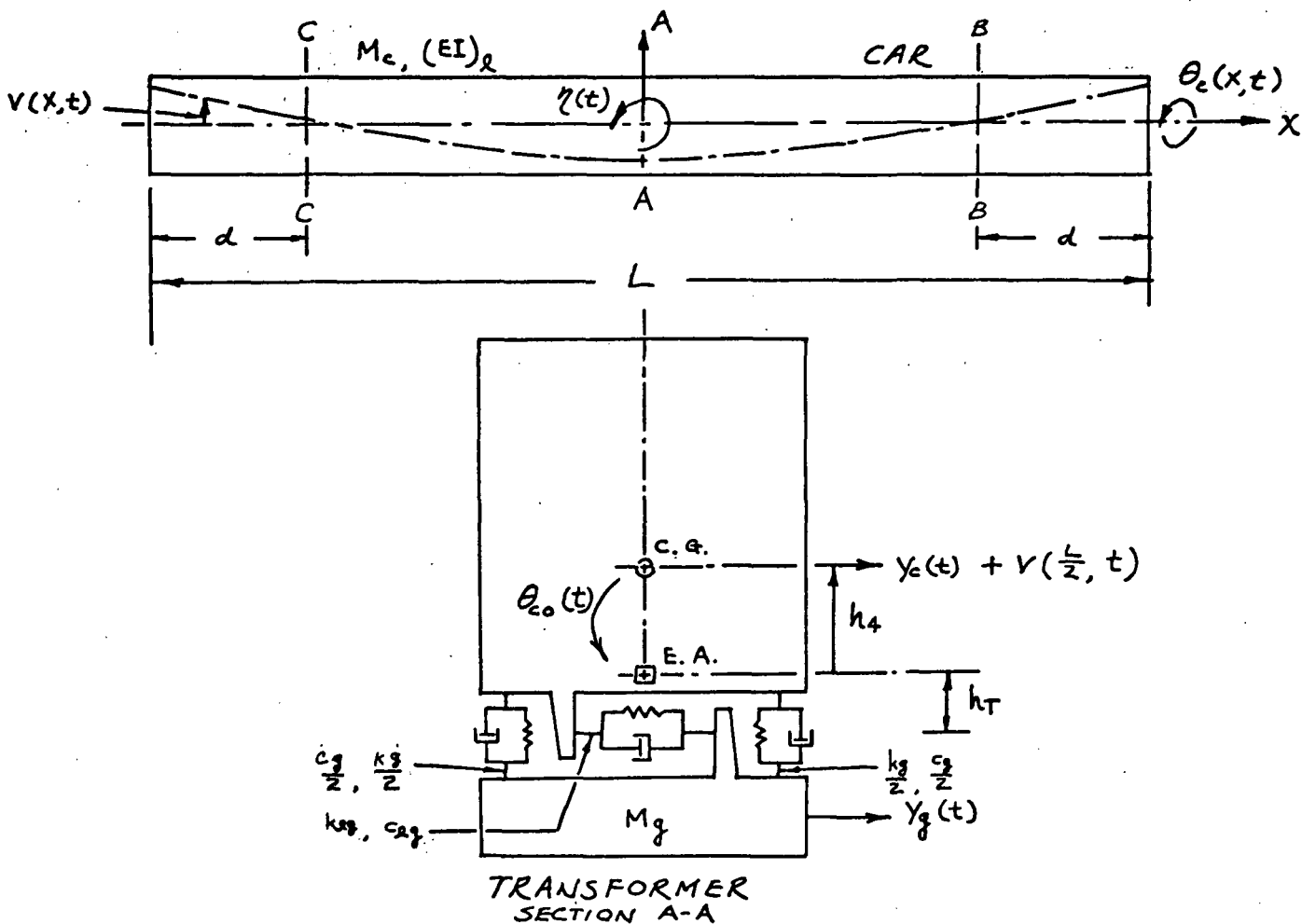


Fig. 13 Mathematical Lateral Model of Railroad Car and Truck Suspension
(a) Top and Mid Section Views

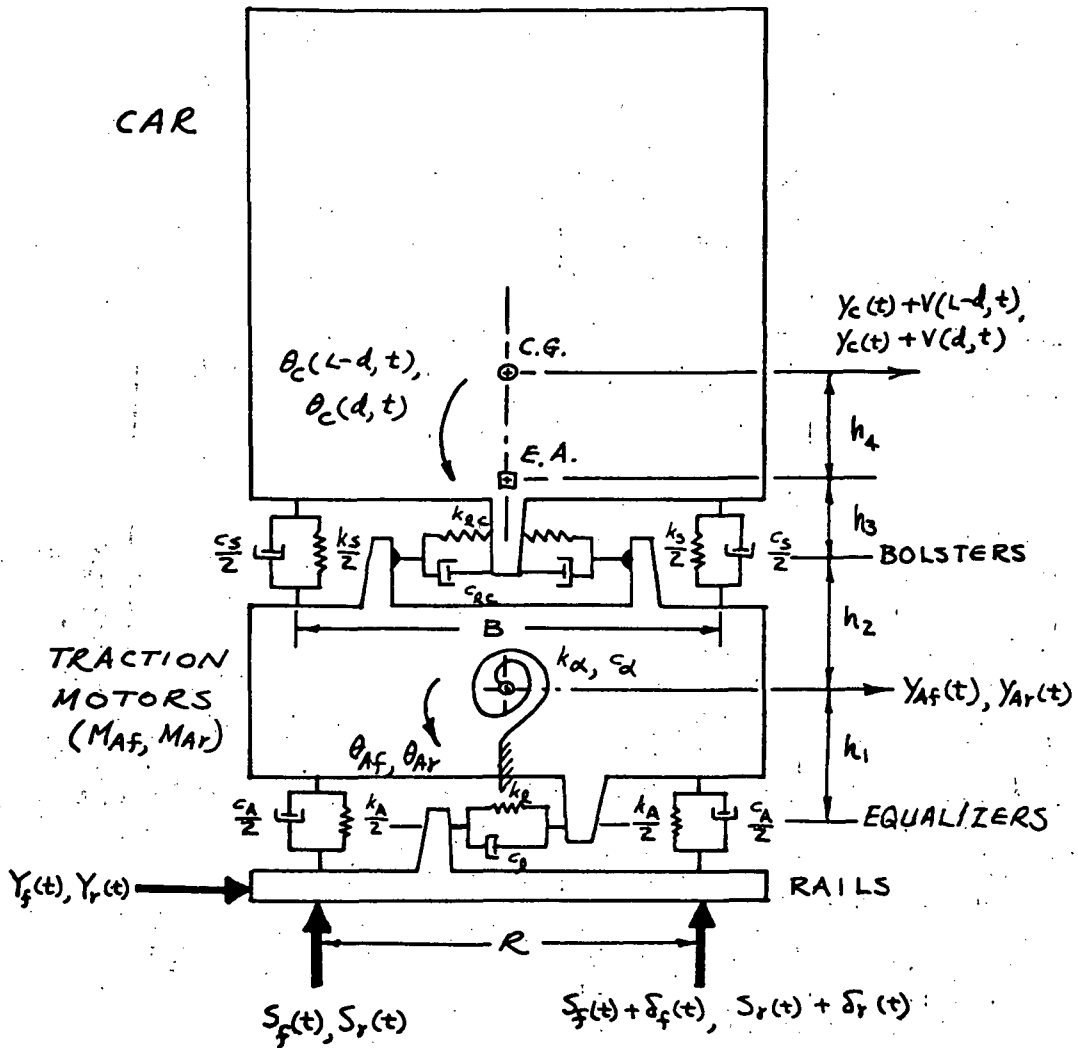


Fig. 13 Concluded

(b) Truck Suspension (Section B-B, and C-C)

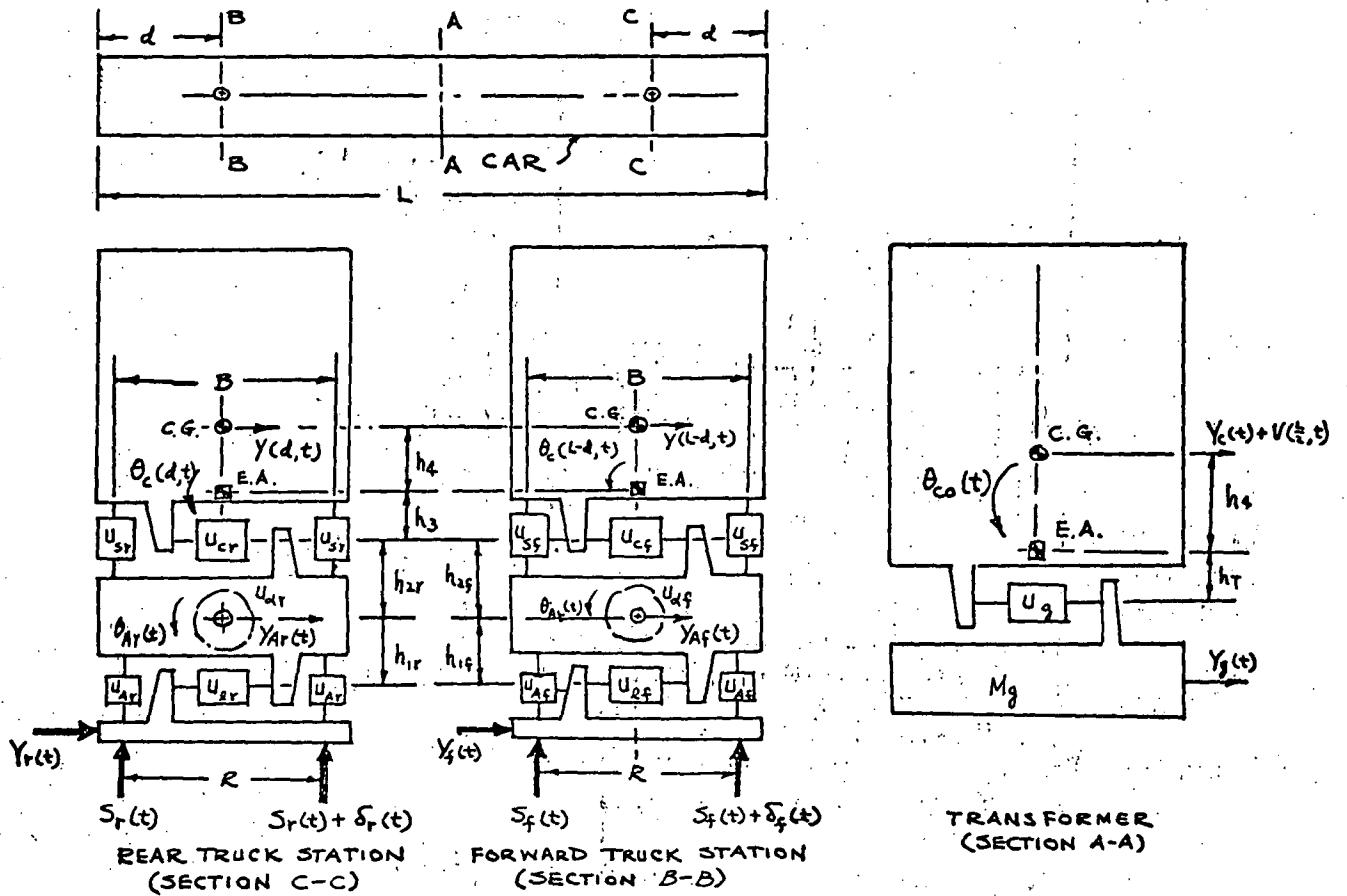


Fig. 14 Schematic View of Lateral Rail Car Model With Eleven Isolator Forces

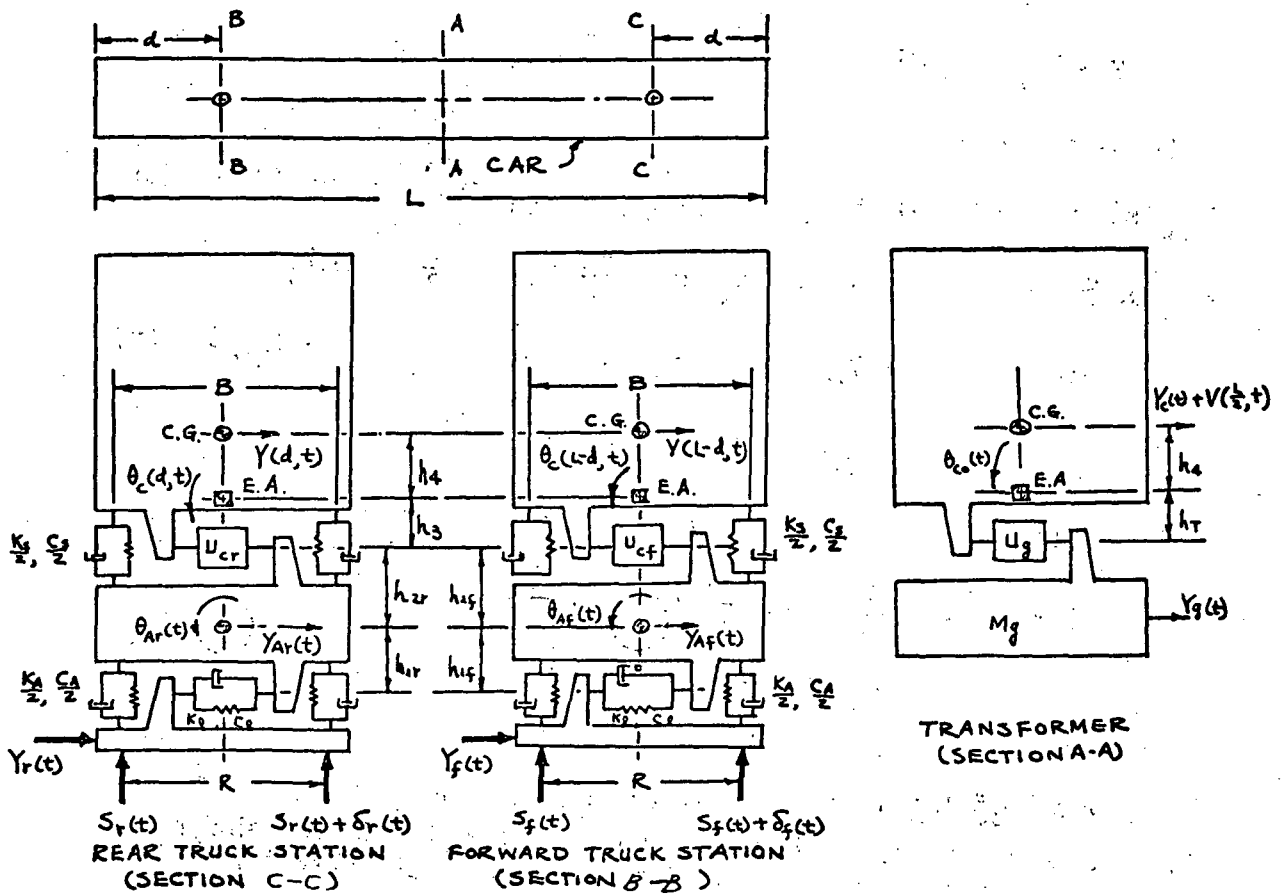


Fig. 15 Schematic View of Lateral Rail Car Model With Three Isolator Forces

$$\max |A_{cl}(x)|$$

is minimized, and

$$YL \leq \Delta Y_r(t) \leq YU$$

$$YL \leq \Delta Y_f(t) \leq YU$$

are satisfied. Here

$$\begin{aligned} A_{cl}(x) &= \ddot{b}(t)W(x) + \ddot{Y}_c - h_4(\ddot{\theta}_{co} + \ddot{\theta}_{cl} \cos \frac{\pi x}{L}) - (\frac{L}{2} - x)\ddot{\eta} \\ &= W(x)\ddot{q}_1 + \ddot{q}_2 - h_4\ddot{q}_3 - (h_4 \cos \frac{\pi x}{L})\ddot{q}_4 - (\frac{L}{2} - x)\ddot{q}_5 \end{aligned}$$

$$\begin{aligned} \Delta Y_r &= -b(t)W(d) - Y_c(t) + (\frac{L}{2} - d)\eta(t) + Y_{Ar}(t) - h_{2r}\theta_{Ar}(t) \\ &\quad - h_3[\theta_{co}(t) + \theta_{cl}(t) \cos \frac{\pi d}{L}] \end{aligned}$$

ΔY_f = same as ΔY_r with $W(d)$ replaced by $W(L-d)$,

$$(\frac{L}{2} - d) \text{ by } -(\frac{L}{2} - d), \frac{\pi d}{L} \text{ by } \frac{\pi(L-d)}{L}$$

and the subscript r by f

3. Modified Equations of Motion for PERFORM

The equations of motion for the original system shown in Fig. 13 were derived in Ref. 3 and expressed in the form

$$\underline{M}\ddot{\underline{q}} + \underline{C}\dot{\underline{q}} + \underline{K}\underline{q} = \underline{F}\bar{f}_k \quad (21)$$

In order to use PERFORM the equations of motion must appear as

$$\underline{M} \ddot{\underline{q}} + \underline{C} \dot{\underline{q}} + \underline{K} \underline{q} + \underline{U} \underline{u} = \underline{F} \bar{f}_k \quad (22)$$

where the u 's are the control forces that replace the spring and damping forces.

Formulation of equations of motion in the form of Eq. (22) is not unique and depends on the choice of the coordinate system as well as the isolator forces to be used. This will be shown in the following illustrations with a two-degree-of-freedom system with its kinematic relations as indicated in Fig. 16a. The equations of motion in the coordinates z_1 and z_2 are written as

$$\begin{aligned} m_1 \ddot{z}_1 + k_1(z_1 - f) + k_2(z_1 - z_2) &= 0 \\ m_2 \ddot{z}_2 + k_2(z_2 - z_1) &= 0 \end{aligned} \quad (23)$$

Using the coordinates x_1 and x_2 the equations of motion become

$$\begin{aligned} m_1 \ddot{x}_1 + k_1 x_1 - k_2 x_2 &= -m_1 \ddot{f} \\ m_2 (\ddot{x}_2 + \ddot{x}_1) + k_2 x_2 &= -m_2 \ddot{f} \end{aligned} \quad (24)$$

Now we write the equations of motion in the form of Eqs. (23) and (24) for the following six different cases of coordinate systems and isolator forces.

Case 1 (Fig. 16b)

$$\begin{aligned} m_1 \ddot{z}_1 + u_1 + u_2 &= 0 \\ m_2 \ddot{z}_2 - u_2 &= 0 \end{aligned} \quad (25)$$

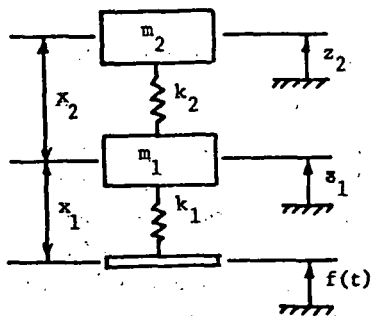
where

$$u_1 = k_1(z_1 - f)$$

$$u_2 = k_2(z_1 - z_2)$$

Case 2 (Fig. 16c)

$$m_1 \ddot{x}_1 + u_1 + u_2 = -m_1 \ddot{f}$$



$$z_1 = x_1 + f$$

$$z_2 = x_1 + x_2 + f$$

Fig. (a)

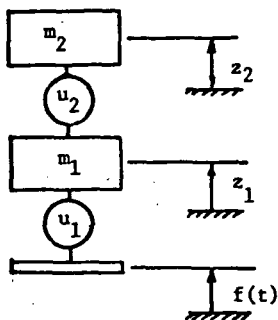


Fig. (b)

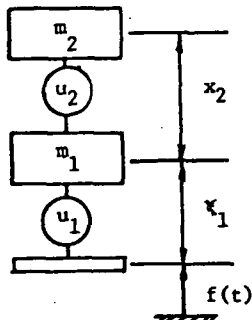


Fig. (c)

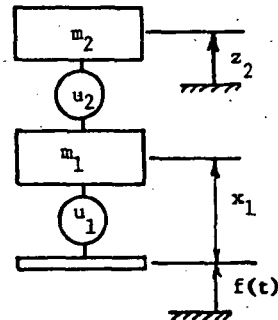


Fig. (d)

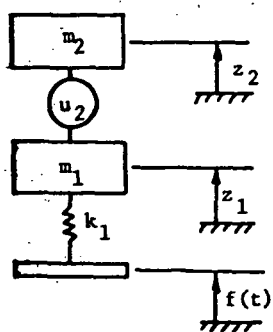


Fig. (e)

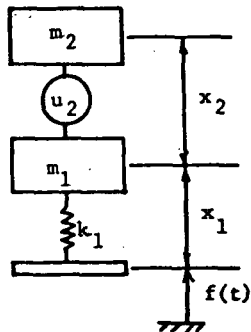


Fig. (f)

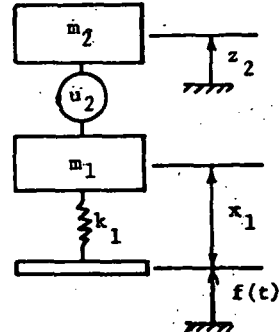


Fig. (g)

Fig. 16 Two-Degree-of-Freedom System

$$m_2(\ddot{x}_2 + \ddot{x}_1) - u_2 = -m_2\ddot{f} \quad (26)$$

where

$$u_1 = k_1 x_1$$

$$u_2 = -k_2 x_2$$

Case 3 (Fig. 16d)

$$m_1\ddot{x}_1 + u_1 + u_2 = -m_1\ddot{f} \quad (27)$$

$$m_2\ddot{z}_2 - u_2 = 0$$

Case 4 (Fig. 16e)

$$m_1\ddot{z}_1 + k_1 z_1 + u_2 = k_1 f \quad (28)$$

$$m_2\ddot{z}_2 - u_2 = 0$$

where

$$u_2 = k_2(z_1 - z_2)$$

Case 5 (Fig. 16f)

$$m_1\ddot{x}_1 + k_1 x_1 + u_2 = -m_1\ddot{f} \quad (29)$$

$$m_2(\ddot{x}_1 + \ddot{x}_2) - u_2 = -m_2\ddot{f}$$

where

$$u_2 = -k_2 x_2$$

Case 6 (Fig. 16g)

$$m_1\ddot{x}_1 + k_1 x_1 + u_2 = -m_1\ddot{f} \quad (30)$$

$$m_2\ddot{z}_2 - u_2 = 0$$

In Case 1, where the coordinates z_1 and z_2 represent absolute displacements of masses m_1 and m_2 , the equations of motion (Eq. (25)) do not have any forcing functions. This would not be an acceptable form unless only initial conditions of these coordinates are specified. Furthermore, if for Case 1 we

define

$$u_1 = k_1 z_1 \text{ and}$$

$$u_2 = k_2 (z_1 - z_2),$$

the equations of motion become

$$\begin{aligned} m_1 \ddot{z}_1 + u_1 + u_2 &= k_1 f \\ m_2 \ddot{z}_2 - u_2 &= 0 \end{aligned} \quad (31)$$

Eq. (31) includes a forcing function and may appear to be as acceptable as Case 4. However, we have here the problem of a term with the system spring characteristics with k_1 not being completely replaced by u_1 or u_2 . Cases 2 through 6 are all acceptable and the choice of a particular coordinate system or isolator forces depends on the initial conditions and the nature of the problem at hand.

a. The Case of Eleven Isolator Forces (Fig. 14).

For this case the equations of motion in the form of Eq. (22) will have the following vectors and coefficient matrices:

. Displacement Vector

$$\bar{q} = \begin{bmatrix} b = q_1 \\ y_c = q_2 \\ \theta_{co} = q_3 \\ \theta_{cl} = q_4 \\ \eta = q_5 \\ y_{lg} = q_6 \\ z_r = q_7 \\ z_f = q_8 \\ \phi_r = q_9 \\ \phi_f = q_{10} \end{bmatrix}$$

where

$$z_r = y_{Ar} - y_r$$

$$z_f = y_{Af} - y_f$$

$$\phi_r = \theta_{Ar} - \frac{\delta_r}{R}$$

$$\phi_f = \theta_{Af} - \frac{\delta_f}{R}$$

The coordinate system used here is similar to that of Case 3 discussed above.

. Forcing Function Vector

$$\bar{f}_1 = \begin{bmatrix} f_{11} \\ f_{12} \\ f_{13} \\ f_{14} \end{bmatrix}$$

where

$$f_{11} = M_{Ar} \ddot{y}_r$$

$$f_{12} = M_{Af} \ddot{y}_f$$

$$f_{13} = I_{Ar} \ddot{\delta}_r$$

$$f_{14} = I_{Af} \ddot{\delta}_f$$

$$y_f = \frac{y_{of}}{2} [1 - \cos \frac{2\pi V(t-t_o)}{\lambda + (\Delta\ell)_t}], \quad \ddot{y}_f = \frac{2y_{of} (\pi V)^2}{[\lambda + (\Delta\ell)_t]^2} \cos \frac{2\pi V(t-t_o)}{\lambda + (\Delta\ell)_t}$$

$$y_r = \frac{y_{or}}{2} [1 - \cos \frac{2\pi V(t-t_2)}{\lambda + (\Delta\ell)_t}], \quad \ddot{y}_r = \frac{2y_{or} (\pi V)^2}{[\lambda + (\Delta\ell)_t]^2} \cos \frac{2\pi V(t-t_2)}{\lambda + (\Delta\ell)_t}$$

$$\delta_r = \frac{\delta_{or}}{2} [1 - \cos \frac{2\pi V(t-t_o)}{\lambda + (\Delta\ell)_t}], \quad \ddot{\delta}_r = \frac{2\delta_{or}(\pi V)^2}{[\lambda + (\Delta\ell)_t]^2} \cos \frac{2\pi V(t-t_o)}{\lambda + (\Delta\ell)_t}$$

$$\delta_f = \frac{\delta_{of}}{2} [1 - \cos \frac{2\pi V(t-t_2)}{\lambda + (\Delta\ell)_t}], \quad \ddot{\delta}_f = \frac{2\delta_{of}(\pi V)^2}{[\lambda + (\Delta\ell)_t]^2} \cos \frac{2\pi V(t-t_2)}{\lambda + (\Delta\ell)_t}$$

The Y's are lateral inputs and the δ 's are the cross-level inputs. The second derivatives of Y's and δ 's with respect to time are expressed as \ddot{Y} 's and $\ddot{\delta}$'s. The quantities V, λ , and $(\Delta\ell)_t$ represent the train speed, the wave length of the input disturbance, and the wheel base of a truck suspension, respectively. In the above equations t_2 is obtained from the relations

$$t_1 - t_o = \frac{\lambda + (\Delta\ell)_t}{V}$$

$$t_2 - t_1 = \frac{L - 2d - (\Delta\ell)_t - \lambda}{V}$$

where $t_1 - t_o$ = time interval for forward truck to roll over the disturbance.

$t_2 - t_1$ = time interval between when the front truck leaves the disturbance and the rear truck encounters it.

. Isolator Force Vector

$$\bar{u} = [u_{cr} = u_1, u_{cf} = u_2, u_{sr} = u_3, \\ u_{sf} = u_4, u_g = u_5, u_{lr} = u_6, \\ u_{lf} = u_7, u_{Ar} = u_8, u_{Af} = u_9, \\ u_{ar} = u_{10}, u_{af} = u_{11}].$$

where the isolator forces are defined in terms of the configuration of Fig. 13. They are

$$u_{cr} = u_1 = c_{lcr} [W(d)\dot{b} + \dot{y}_c + h_3 \dot{\theta}_{co} + h_3 \cos \frac{\pi d}{L} \dot{\theta}_{cl} - (\frac{L}{2} - d)\dot{\eta} - (\dot{z}_r + \dot{y}_r) + h_{2r} (\dot{\phi}_r + \frac{\dot{\delta}_r}{R})] + k_{lcr} [W(d)b + y_c + h_3 \theta_{co} + h_3 \cos \frac{\pi d}{L} \theta_{cl} - (\frac{L}{2} - d)\eta - (z_r + y_r) + h_{2r} (\phi_r + \frac{\delta_r}{R})]$$

$$u_{cf} = u_2 \text{ Same as } u_{cr} \text{ with the subscript } r \text{ replaced by } f, \\ W(d) \text{ by } W(L-d),$$

$$-(\frac{L}{2} - d) \text{ by } (\frac{L}{2} - d), \text{ and } \frac{\pi d}{L} \text{ by } \frac{\pi(L-d)}{L}$$

$$u_{sr} = u_3 = c_s [\frac{1}{2} \dot{\theta}_{co} + \frac{1}{4} \cos \frac{\pi d}{L} \dot{\theta}_{cl} - \frac{1}{4} (\dot{\phi}_r + \frac{\dot{\delta}_r}{R})] + k_s [\frac{1}{2} \theta_{co} + \frac{1}{4} \cos \frac{\pi d}{L} \theta_{cl} - \frac{1}{4} (\phi_r + \frac{\delta_r}{R})]$$

$$u_{sf} = u_4 = \text{Same as } u_{sr} \text{ with } d \text{ replaced by } (L-d) \text{ and the subscript } r \text{ by } f.$$

$$u_g = u_5 = c_{lg} [W(\frac{L}{2})\dot{b} + \dot{y}_c + h_T \dot{\theta}_{co} - \dot{y}_g] + k_{lg} [W(\frac{L}{2})b + y_c + h_T \theta_{co} - y_g]$$

$$u_{lr} = u_6 = c_{lr} [\dot{z}_r + h_{1r} (\dot{\phi}_r + \frac{\dot{\delta}_r}{R})] + k_{lr} [z_r + h_{1r} (\phi_r + \frac{\delta_r}{R})]$$

$$u_{lf} = u_7 = \text{Same as } u_{lr} \text{ with subscript } r \text{ replaced by } f.$$

$$u_{Ar} = u_8 = c_{Ar} (\dot{\phi}_r + \frac{\dot{\delta}_r}{R}) + k_{Ar} (\phi_r + \frac{\delta_r}{R})$$

$$u_{Af} = u_9 = \text{Same as } u_{Ar} \text{ with subscript } r \text{ replaced by } f.$$

$$u_{ar} = u_{10} = c_{ar} (\dot{\phi}_r + \frac{\dot{\delta}_r}{R}) + k_{ar} (\phi_r + \frac{\delta_r}{R})$$

$$u_{af} = u_{11} = \text{Same as } u_{ar} \text{ with subscript } r \text{ replaced by } f.$$

. Damping Matrix

$$\underline{C} = [0]$$

Spring Matrix

$$\underline{K} = [0]$$

except

$$K_{11} = (EI)_L \frac{4}{L^3}$$

$$K_{44} = \frac{GJL}{2} \left(\frac{\pi}{L}\right)^2$$

MASS MATRIX, \underline{M}

	1	2	3	4	5	6	7	8	9	10
1	M_C	0	0	$-\dot{m}h_4\delta_1\{ \}$	0	0	0	0	0	0
2	0	M_C	$-M_C h_4$	0	0	0	0	0	0	0
3	0	$-M_C h_4$	$I_{EA} L$	0	0	0	0	0	0	0
4	$-\dot{m}h_4\delta_1\{ \}$	0	0	$I_{EA} \frac{L}{2}$	$2\dot{m}h_4\left(\frac{L}{\pi}\right)^2$	0	0	0	0	0
5	0	0	0	$2\dot{m}h_4\left(\frac{L}{\pi}\right)^2$	$M_C \frac{L^2}{12}$	0	0	0	0	0
6	0	0	0	0	0	M_G	0	0	0	0
7	0	0	0	0	0	0	M_{Ar}	0	0	0
8	0	0	0	0	0	0	0	M_{Af}	0	0
9	0	0	0	0	0	0	0	0	I_{Ar}	0
10	0	0	0	0	0	0	0	0	0	I_{Af}

$$(a) \quad \{ \} = - \left[\frac{\sin h\beta_1 L}{\beta_1^2 + \left(\frac{\pi}{L}\right)^2} + \frac{\sin \beta_1 L}{\beta_1^2 - \left(\frac{\pi}{L}\right)^2} \right] + \alpha_1 \left[\frac{\cos h\beta_1 L + 1}{\beta_1^2 + \left(\frac{\pi}{L}\right)^2} - \frac{\cos \beta_1 L + 1}{\beta_1^2 - \left(\frac{\pi}{L}\right)^2} \right] \quad \beta_1 L = 4.730 \quad \alpha_1 = 0.9825$$

Control Force Matrix

	(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)
1	$W(d)$	$W(L-d)$	0	0.	$W(\frac{L}{2})$	0	0	0	0	0	0
2	1	1	0	0	1	0	0	0	0	0	0
3	h_3	h_3	B^2	B^2	h_T	0	0	0	0	0	0
4	$h_3 \cos \frac{\pi d}{L}$	$h_3 \cos \frac{\pi(L-d)}{L}$	$B^2 \cos \frac{\pi d}{L}$	$B^2 \cos \frac{\pi(L-d)}{L}$	0	0	0	0	0	0	0
5	$-(\frac{L}{2} - d)$	$(\frac{L}{2} - d)$	0	0	0	0	0	0	0	0	0
6	0	0	0	0	-1	0	0	0	0	0	0
7	-1	0	0	0	0	1	0	0	0	0	0
8	0	-1	0	0	0	0	0	0	0	0	0
9	h_{2r}	0	-B	0	0	h_{r1}	0	$\frac{R^2}{4}$	0	1	0
10	0	h_{2f}	0	-B	0	0	h_{1f}	0	$\frac{R^2}{4}$	0	1

Forcing Function Matrix

$$F = \begin{bmatrix} & (1) & (2) & (3) & (4) \\ (1) & 0 & 0 & 0 & 0 \\ (2) & 0 & 0 & 0 & 0 \\ (3) & 0 & 0 & 0 & 0 \\ (4) & 0 & 0 & 0 & 0 \\ (5) & 0 & 0 & 0 & 0 \\ (6) & 0 & 0 & 0 & 0 \\ (7) & -1 & 0 & 0 & 0 \\ (8) & 0 & -1 & 0 & 0 \\ (9) & 0 & 0 & -\frac{1}{R} & 0 \\ (10) & 0 & 0 & 0 & -\frac{1}{R} \end{bmatrix}$$

b. The Case of Three Isolator Forces (Fig. 15)

The vectors and coefficient matrices of the equations of motion in the form of Eq. (22) are defined as follows:

. Displacement Vector

$$\bar{q} = \begin{bmatrix} b = q_1 \\ y_c = q_2 \\ \theta_{co} = q_3 \\ \theta_{cl} = q_4 \\ n = q_5 \\ y_g = q_6 \\ y_{Ar} = q_7 \\ y_{Af} = q_8 \\ \theta_{Ar} = q_9 \\ \theta_{Af} = q_{10} \end{bmatrix}$$

Here we are using a coordinate system similar to that of Case 4.

. Forcing Function Vector

$$\bar{f}_1 = \begin{bmatrix} f_{11} \\ f_{12} \\ f_{13} \\ f_{14} \end{bmatrix}$$

where

$$f_{11} = k_{lr} Y_r + c_{lr} \dot{Y}_r$$

$$f_{12} = k_{lf} Y_f + c_{lf} \dot{Y}_f$$

$$f_{13} = k_{Ar} \delta_r + c_{Ar} \dot{\delta}_r$$

$$f_{14} = k_{Af} \delta_f + c_{Af} \dot{\delta}_f$$

The rail inputs Y 's and δ 's are the same as in the first case. \dot{Y} 's and $\dot{\delta}$'s are the time derivatives

$$\dot{Y}_r = \frac{Y_{or} \pi V}{\lambda + (\Delta \ell)_t} \sin \frac{2\pi V (t-t_2)}{\lambda + (\Delta \ell)_t}$$

$$\dot{Y}_f = \frac{Y_{of} \pi V}{\lambda + (\Delta \ell)_t} \sin \frac{2\pi V (t-t_o)}{\lambda + (\Delta \ell)_t}$$

The expressions for $\dot{\delta}_r$ and $\dot{\delta}_f$ are of the same form as for the \dot{Y}_r and \dot{Y}_f with δ_{of} and δ_{or} replacing Y_{of} and Y_{or} .

. Control Force Vector

$$\bar{u} = \begin{bmatrix} u_{cr} = u_1 \\ u_{cf} = u_2 \\ u_g = u_3 \end{bmatrix}$$

where the isolator forces are defined in terms of the configuration of Fig. 13. These are

$$\begin{aligned} u_1 = c_{lcr} [W(d)\dot{b} + \dot{y}_c + h_3 \dot{\theta}_{co} + h_3 \cos \frac{\pi d}{L} \dot{\theta}_{cl} - (\frac{L}{2} - d)\dot{\eta} \\ - \dot{y}_{Ar} + h_{2r} \dot{\theta}_{Ar}] \\ + k_{lcr} [W(d)b + y_c + h_3 \theta_{co} + h_3 \cos \frac{\pi d}{L} \theta_{cl} - (\frac{L}{2} - d)\eta \\ - y_{Ar} + h_{2r} \theta_{Ar}] \end{aligned}$$

u_2 = Same as u_1 with the subscript r replaced by f , and $W(d)$ by $W(L-d)$, $-(\frac{L}{2} - d)$ by $(\frac{L}{2} - d)$, and $\frac{\pi d}{L}$ by $\frac{\pi(L-d)}{L}$

$$u_3 = c_{lg} \left[W\left(\frac{L}{2}\right) \dot{b} + \dot{y}_c + h_T \dot{\theta}_{co} - \dot{y}_g \right] + k_{lg} \left[W\left(\frac{L}{2}\right) b + h_T \theta_{co} + y_c - y_g \right]$$

. Mass Matrix

\underline{M} = same as in the previous case of 11 isolator forces

.. Stiffness Matrix, \underline{K}

$$K_{11} = (EI) L \beta_1^4 L$$

$$K_{12} = \dots = K_{1,10} = 0$$

$$K_{21} = \dots = K_{2,10} = 0$$

$$K_{31} = K_{32} = 0$$

$$K_{33} = \frac{k_s B^2}{2}$$

$$K_{34} = \frac{k_s B^2}{4} \left[\cos \frac{\pi d}{L} + \cos \frac{\pi(L-d)}{L} \right] = K_{43}$$

$$K_{35} = \dots = K_{38} = 0$$

$$K_{39} = \frac{-k_s B^2}{4} = K_{93} = K_{3,10} = K_{10,3} = K_{49} = K_{4,10} = K_{10,4} = K_{94}$$

$$K_{44} = \frac{k_s B^2}{4} \left[\cos^2 \frac{\pi d}{L} + \cos^2 \frac{\pi(L-d)}{L} \right] + \frac{GJL}{2} \left(\frac{\pi}{L} \right)^2$$

$$K_{45} = \dots = K_{48} = 0$$

$$K_{51} = \dots = K_{5,10} = 0$$

$$K_{61} = \dots = K_{6,10} = 0$$

$$K_{71} = \dots = K_{76} = 0$$

$$K_{77} = \dots = k_{lr}$$

$$K_{78} = K_{87} = 0$$

$$K_{88} = k_{lf}$$

$$K_{89} = K_{98} = 0$$

$$K_{8,10} = K_{10,8} = k_{lf} h_{lf}$$

$$K_{91} = K_{92} = K_{95} = K_{96} = K_{9,10} = 0$$

$$K_{97} = K_{79} = k_{lr} h_{lr}$$

$$K_{99} = \frac{k_s B^2}{4} + \frac{k_{Ar} R^2}{4} + k_{ar} + h_{lr}^2 k_{lr}$$

$$K_{10,10} = \frac{k_s B^2}{4} + \frac{k_{Af} R^2}{4} + k_{af} + k_{lf} h_{lf}^2$$

. Damping Matrix, C

Identical in form to \underline{K} except $C_{11} = 0$,

$$C_{44} = \frac{c_s B^2}{4} \left[\cos^2 \frac{\pi d}{L} + \cos^2 \frac{\pi(L-d)}{L} \right]$$

For other elements k_s, k_A, k_a are replaced by c_s, c_A, c_a respectively.

. Control Force Matrix, U

$$U_{11} = W(d) \quad U_{52} = \frac{L}{2} - d$$

$$U_{12} = W(L-d) \quad U_{53} = U_{61} = U_{62} = 0$$

$$U_{13} = W\left(\frac{L}{2}\right) \quad U_{63} = U_{71} = -1$$

$$U_{21} = U_{22} = U_{23} = 1 \quad U_{72} = U_{73} = U_{81} = 0$$

$$U_{31} = U_{32} = h_3 \quad U_{82} = -1$$

$$U_{33} = h_T \quad U_{83} = 0$$

$$U_{41} = h_3 \cos \frac{\pi d}{L}$$

$$U_{91} = h_{2r}$$

$$U_{42} = h_3 \cos \frac{\pi(L-d)}{L}$$

$$U_{92} = U_{93} = U_{10,1} = U_{10,3} = 0$$

$$U_{43} = 0$$

$$U_{10,2} = h_{2f}$$

$$U_{51} = -(\frac{L}{2} - d)$$

. Forcing Function Matrix

	(1)	(2)	(3)	(4)
(1)	0	0	0	0
(2)	0	0	0	0
(3)	0	0	0	0
(4)	0	0	0	0
(5)	0	0	0	0
(6)	0	0	0	0
(7)	1	0	0	0
(8)	0	1	0	0
(9)	h_{lr}	0	$\frac{R}{4}$	0
(10)	0	h_{lf}	0	$\frac{R}{4}$

4. Notation

$A_{cl}(x)$	lateral acceleration of car
B	lateral distance between bolster springs (see Fig. 14)
$b(t)$	generalized coordinate for lateral car bending
C_{hi}	$(h-1)^{th}$ element of damping matrix
d	distance from end of car to centerline of trucks (see Fig. 13)

E	Young's modulus
f_q	frequency of q^{th} degree of freedom, $\frac{\omega_q}{2\pi}$, Hz
G	modulus of rigidity
h_1	vertical distance from traction-motor center of gravity to line of action of lateral equalizer spring (see Fig. 13(b))
h_2	vertical distance from traction-motor center of gravity to line of action of lateral bolster spring (see Fig. 13(b))
h_3	vertical distance between car elastic axis and line of action of lateral bolster spring (see Fig. 13(b))
h_4	vertical distance of car section center of gravity from car elastic axis, positive for center of gravity above elastic axis (see Fig. 13(b))
h_T	vertical distance between car elastic axis and line of action of lateral transformer spring (see Fig. 13(a))
I	flexural moment of inertia of car cross-section
I_A	mass moment of inertia of traction motor in roll about its center of gravity
I_{EA}	mass moment of inertia of car in roll about car elastic axis, per unit length
J	torsional constant of car cross-section
k	spring constant
K_{hi}	$(h-i)^{\text{th}}$ element of stiffness matrix
L	length of car (see Figs. 13(a))
M_{hi}	$(h-i)^{\text{th}}$ element of mass matrix
m	mass of car per unit length
M_A	traction-motor mass

M_c	car mass, mL
M_g	transformer mass
n_q	viscous damping coefficient for q^{th} degree of freedom, where $q = A, cl, cT$, etc., also see subscripts
R	lateral distance between equalizer springs (see Fig. 13(b))
$S(t)$	vertical displacement forcing function at rails (see Fig. 13(b))
v	car speed
$v(x,t)$	lateral bending deformation of car (see Fig. 13(a))
$W(x)$	car bending mode-shape value at x
x	length along car, measured from rear of car
$Y(t)$	lateral displacement forcing function at rails (see Fig. 13(b))
Y_L	lower limit
Y_U	upper limit
$y_A(t)$	generalized coordinate of lateral translation of traction motor
$y_c(t)$	generalized coordinate of lateral rigid-body translation of car (see Fig. 13(b))
y_{lg}	generalized coordinate of lateral transformer translation
$\delta(t)$	increment of vertical displacement at rails associated with cross-level (or rolling) displacement input (see Fig. 13(b))
$(\Delta l)_t$	center-to-center distance between axles of a truck suspension system
$\Delta y(t)$	displacement relation in lateral bolster springs for nonlinear spring behavior

$\eta(t)$	generalized coordinate of car in rigid-body yaw
$\theta_A(t)$	generalized coordinate of traction-motor rolling degree of freedom
$\theta_c(x,t)$	rigid-body roll and torsion of car
$\theta_{co}(t)$	generalized coordinate for rigid-car roll
$\theta_{cl}(t)$	generalized coordinate for 1 st torsion mode of car

Subscripts

A	identifies properties associated with the traction-motor-equalizer system
c	associated with car
f	identifies forward trucks
g	associated with transformer
h,i	integers identifying matrix elements
l	identifies properties of traction-motor-lateral-equalizer system
lc	identifies properties of lateral bolster spring-damper system
o	identifies amplitude of forcing function
r	identifies rear trucks
s	identifies properties of vertical bolster spring-damper system

Dots over quantities denote differentiation with respect to time.

D. Aircraft Ride Control System

To evaluate the candidate designs for the ride control system in a STOL airplane, a limiting performance problem was formulated. Specifically, it is desired to minimize the maximum vertical center-of-gravity (c.g.) acceleration subject to constraints on flap and elevator deflections. These two deflections are used as controls.

The airplane is assumed to behave as a rigid body. The nomenclature is:

α = wing angle of attack

θ = rigid-body pitch of airplane

v = perturbation in forward velocity

$\alpha_g(t)$ = angle of attack due to gust

$\alpha_g(t-T)$ = delayed gust angle of attack (at tail)

T = time delay between impingement of gust on wing and tail

u_1 = elevator angular deflection, a control function

u_2 = flap angular deflection, a control function

α_o = gust amplitude

ω = gust frequency

Assuming quasi-steady aerodynamics, the equations of motion for the airplane in first order PERFORM format are

$$\dot{\bar{s}} = \underline{A} \bar{s} + \underline{B} \bar{u} + \underline{D} \bar{f}_k \quad (32)$$

where

$$s = \begin{bmatrix} s_1 \\ s_2 \\ s_3 \\ s_4 \end{bmatrix} = \begin{bmatrix} \theta \\ \dot{\theta} \\ \alpha \\ v \end{bmatrix} \quad (33)$$

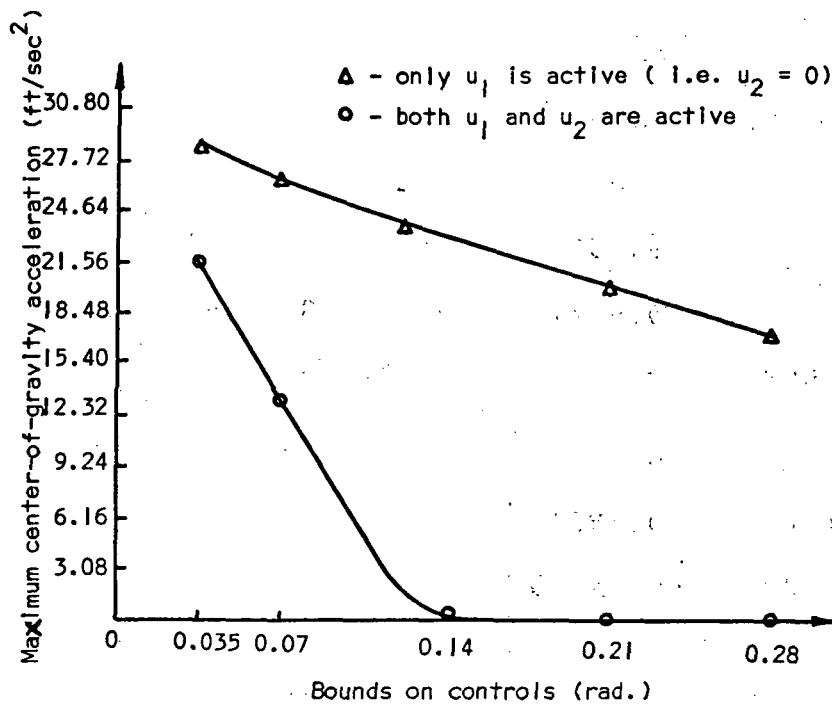


Fig. 17 Limiting Performance for a STOL Airplane Ride Control System.

$$\bar{u} = \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} \quad (34)$$

$$\bar{f}_k = \begin{bmatrix} f_{11} \\ f_{12} \end{bmatrix} = \begin{bmatrix} \alpha_g(t) \\ \alpha_g(t - T) \end{bmatrix} \quad (35)$$

Consider the specific case:

$$\underline{A} = \begin{bmatrix} 0 & 1.0 & 0 & 0 \\ 0 & -0.05662 & -0.58024 & -0.0000262 \\ 0 & 0.97710 & -1.75148 & -0.001 \\ -4.77992 & 0 & 0.96138 & 0 \end{bmatrix}$$

$$\underline{B} = \begin{bmatrix} 0 & 0 \\ -0.64961 & -0.18396 \\ -0.15183 & -0.64855 \\ 0 & 0 \end{bmatrix}$$

$$\underline{D} = \begin{bmatrix} 0 & 0 \\ -0.13587 & -0.10674 \\ -1.65057 & -0.14425 \\ 0 & 0 \end{bmatrix}$$

Select $v_0(\dot{s}_1 - \dot{s}_3)$ as the objective function, with $v_0 = 308$ ft/sec. The constraints are imposed on the magnitude of the control. Numerical solutions are obtained for two cases. In Case 1 only u_1 is active and $u_2 = 0$. In Case 2, both u_1 and u_2 are active. The disturbance in both instances is a step input, i.e., $\alpha_g(t) = 0.649H(t)$ where $H(t)$ is a unit step function. The time delay is $T = .08207$ sec. The total time interval used was 0.95 sec with a time increment of 0.05 sec. The trade-off curves for these two cases are shown in Fig. 17.

E. Shock Absorbers for Freight Cars

Consider the limiting performance of the shock-absorber system (or cushion) of railroad vehicles used in protecting passengers or cargos under crash conditions. Typical analyses of freight car lading protection problems are described in Refs. 4 and 5.

The dynamic system model of Fig. 18 is taken from Ref. 5, with the following nomenclature:

S_o = lading contact area

c = damping coefficient, due to friction in lading

k = elastic constant, representing resilience in lading

M_c = mass of struck car body

M_L = mass of lading

M_s = mass of striking car

u = cushion force

$d = y_1 - y_2$ = cushion travel

V = impact velocity

The equations of motion are given by

$$M_s \ddot{y}_1 + u = 0$$

$$M_c \ddot{y}_2 - k(y_3 - y_2) - c(\dot{y}_3 - \dot{y}_2) - u = 0 \quad (36)$$

$$M_L \ddot{y}_3 + k(y_3 - y_2) - c(\dot{y}_3 - \dot{y}_2) = 0$$

We will treat the impact conditions

$$y_1(0) = y_2(0) = \dot{y}_2(0) = 0$$

$$\dot{y}_2(0) = V$$

where $t = 0$ is the time at which impact occurs.

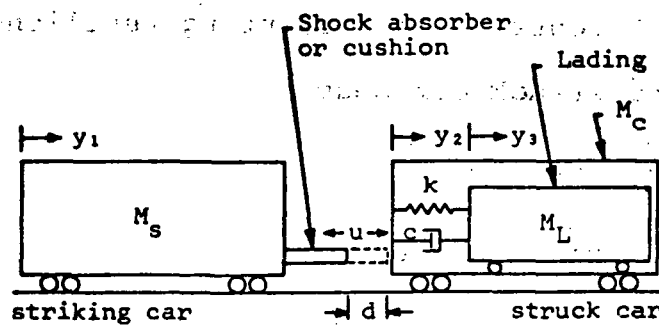


Fig 18. Model of striking car, struck car and lading.

For specified impact velocities, the problem is to minimize the peak force transmitted to the lading while the cushion travel distance is bounded. Thus, the u is sought that minimizes

$$\max |k(y_3 - y_2)| \quad (37)$$

with the restriction that

$$0 \leq d \leq A \quad (38)$$

where A is prescribed.

The problem has been put in PERFORM format for the following physical and material constraints:

$$c = 23,000 \text{ lb sec/ft}$$

$$k = 341,667 \text{ lb/ft}$$

$$M_c = 1630 \text{ lb sec}^2/\text{ft}$$

$$M_L = 1590 \text{ lb sec}^2/\text{ft}$$

$$M_s = 5280 \text{ lb sec}^2/\text{ft}$$

$$S_o = 33.7 \text{ ft}^2$$

$$V = 10 \text{ mph}$$

A PERFORM generated trade-off diagram between maximum transmitted force and cushion travel distance is shown in Fig. 19.

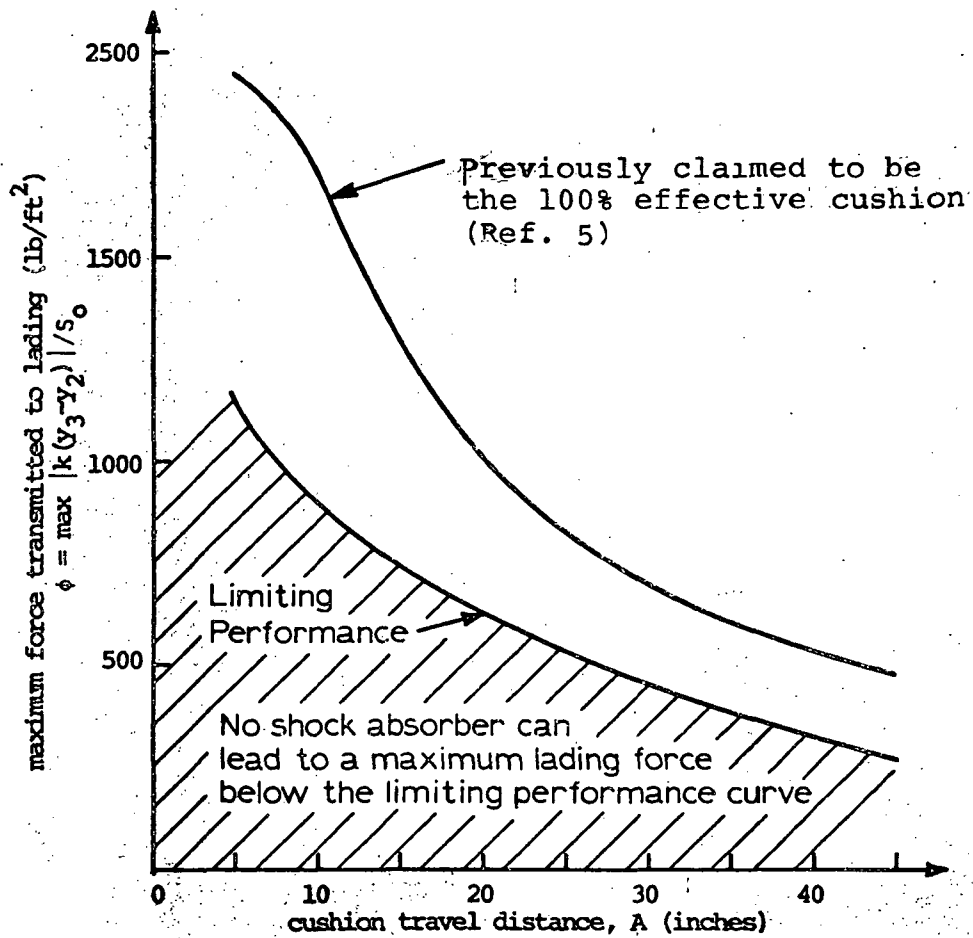


Fig 19. Trade-off diagram for rail vehicle cushioning system

F. A Launch Booster Control Problem

We consider here a booster control problem known as the constrained bending moment minimax drift problem. This is the problem of minimizing the lateral drift from a reference trajectory along a flight path where the magnitude of the bending moment cannot exceed a critical value (Refs. 6, 7). This problem will be placed in the PERFORM format in the following subsections.

1. Equations of Motion

The rigid body equations of a typical launch booster are given in the following form (Ref. 6):

$$\ddot{\phi} + C_1 \alpha + C_2 \beta = 0 \quad (39)$$

$$\ddot{z} = K_1 \phi + K_2 \alpha + K_3 \beta \quad (40)$$

$$\alpha = \phi - \frac{\dot{z}}{V} + \alpha_\omega \quad (41)$$

where ϕ , α , β , z represent angular deviation from reference, angle of attack, engine gimble angle, and lateral positional deviation from reference, respectively. The wind contribution to the angle of attack is denoted by α_ω and the vehicle speed by V . We assume several transient wind disturbance profiles which might be encountered by the launch vehicle during flight are known.

By substituting Eq. (41) into Eqs. (39) and (40), we have

$$\begin{aligned} \ddot{\phi} &= -C_1 \phi + \frac{C_1}{V} \dot{z} - C_1 \alpha_\omega - C_2 \beta \\ \ddot{z} &= (K_1 + K_2) \phi - \frac{K_2}{V} \dot{z} + K_2 \alpha_\omega + K_3 \beta \end{aligned}$$

Let

$$\bar{s} = \begin{bmatrix} \dot{\phi} \\ \dot{z} \\ \phi \\ z \end{bmatrix} = \begin{bmatrix} s_1 \\ s_2 \\ s_3 \\ s_4 \end{bmatrix}$$

and $u = \beta$, and $f_k = \alpha_\omega$

Then the rigid body equations of motion for the booster take the PERFORM compatible form

$$\dot{\underline{s}} = \underline{A} \underline{s} + \underline{B} \underline{u} + \underline{D} \bar{f}_k$$

where

$$\underline{A} = \begin{bmatrix} 0 & \frac{C_1}{V} & -C_1 & 0 \\ 0 & \frac{-K_2}{V} & K_1 + K_2 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix}$$

$$\underline{B} = \begin{bmatrix} -C_2 \\ K_3 \\ 0 \\ 0 \end{bmatrix} \quad \text{and} \quad \underline{D} = \begin{bmatrix} -C_1 \\ K_2 \\ 0 \\ 0 \end{bmatrix}$$

2. Objective Function and Constraints

The bending moment, given by a linear combination of α and β is constrained as follows:

$$| M'_\alpha \alpha + M'_\beta \beta | \leq M_{\max} \quad (42)$$

where M'_α and M'_β are bending moment coefficients and M_{\max} is the maximum allowable bending moment. We choose as an objective the minimization of the maximum $|\dot{z}(t)|$ of the booster subject to the constraint given by Eq. (42).

In the PERFORM format the objective function is written as

$$\underline{PX1}\bar{s} + \underline{PX2}\bar{u} + \underline{PX3} \bar{f}_k$$

where

$$\underline{PX1} = [0 \ 1 \ 0 \ 0]$$

$$\underline{PX2} = [0]$$

$$\underline{PX3} = [0]$$

In the PERFORM input format the constraint given by Eq. (42) can be expressed as

$$\overline{YL} \leq \underline{Y1}\bar{s} + \underline{Y2}\bar{u} + \underline{Y3} \bar{f}_k \leq \overline{YU}$$

where

$$\overline{YL} = -|M_{\max}|$$

$$\overline{YU} = |M_{\max}|$$

$$\underline{Y1} = [0 \quad -\frac{M_{\alpha}}{V} \quad M_{\alpha} \quad 0]$$

$$\underline{Y2} = [M'_{\beta}]$$

$$\underline{Y3} = [M'_{\alpha}]$$

The specification matrix is given by

$$MSP = [0 \ 0 \ 0]$$

3. Output

The rate of change of the lateral positional deviation from reference, $\dot{z}(t)$, can be tabulated versus time. Also, a trade-off relation between the minmax $\dot{z}(t)$ and the maximum bending moment can be obtained by varying the bounds of the bending moment.

G. A Pressurized-Water Nuclear Reactor Power Plant

As a potential application of the computer program to a large system, we consider the control of a pressurized-water nuclear power plant. This system was first used as an example in Ref. [8]. Fig. 20 shows the schematic diagram of the pressurized water reactor. Heat is produced in the reactor by nuclear fission, with the rate controlled by insertion and withdrawal of control rods. This heat is carried away by the primary coolant which then flows to a heat exchanger where it gives up its heat to make steam. The steam goes to a turbine that converts the energy to shaft work to produce electric power. Pumps cause the primary coolant to circulate through the primary loop.

A pressurizer rides above the primary loop with saturated water in the lower part and saturated steam in the upper. Having saturated conditions in the pressurizer assures that the water in the primary loop is subcooled. The steam in the upper part of the pressurizer acts as a "cushion" to allow expansion or contraction of the water as its temperature varies. Spray water taken from the coldest part of the primary loop condenses steam and lowers the pressure. An electric heater boils the saturated water, thus lowering the water level and increasing pressure.

The principal disturbance to the plant operation comes from sudden changes in steam demand from electrical load changes. The most difficult case is a load drop from maximum load. The reduced steam flow takes less heat from the heat exchanger, causing temperature and pressure to rise rapidly in the primary loop.

A ten percent step drop in steam flow from full load is applied with the plant initially at equilibrium. This load change is treated as a forcing function.

The objective is to maximize the minimum value of the pressure of the pressurizer with continuous constraints on maximum pressure and the three controls plus terminal constraints on a temperature and its rate of change. We sketch the formulation of this problem in the PERFORM format in the following subsections. The specific coefficients involved can be found in Ref. 8.

1. Governing Equations

The equations describing the system are expressed as

$$\dot{\bar{s}} = \underline{A} \bar{s} + \underline{B} \bar{u} + \underline{D} \bar{f}_k$$

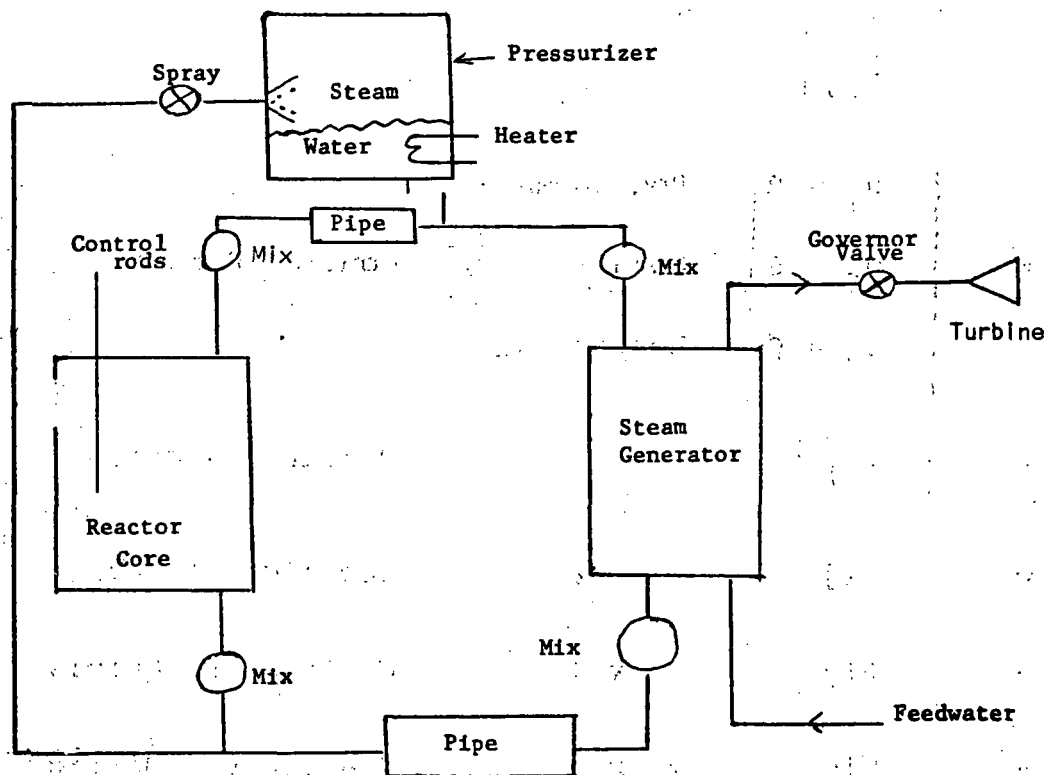


Fig.20 Schematic Diagram of Pressurized-Water Reactor

where

$$\bar{s} = \begin{bmatrix} s_1 \\ s_2 \\ \cdot \\ \cdot \\ s_{25} \end{bmatrix} \quad \text{state vector}$$

$$\bar{u} = \begin{bmatrix} u_1 = R \\ u_2 = S \\ u_3 = Q \end{bmatrix} \quad \left. \begin{array}{l} \text{Rod speed} \\ \text{Spray} \\ \text{Heater} \end{array} \right\} \quad \text{Control Forces}$$

$$\bar{f}_k = \begin{bmatrix} f_{11} \end{bmatrix} \quad \text{Forcing Function}$$

$$\underline{A} = \begin{bmatrix} A_{ij} \end{bmatrix} \quad 25 \times 25 \quad \text{Coefficient Matrix}$$

$$\underline{B} = \begin{bmatrix} B_{ij} \end{bmatrix} \quad 25 \times 3 \quad \text{Coefficient Matrix}$$

$$\underline{D} = \begin{bmatrix} D_{ij} \end{bmatrix} \quad 25 \times 1 \quad \text{Coefficient Matrix}$$

2. Objective Function

The objective function is expressed in the matrix form

$$\underline{PX1} \bar{s} + \underline{PX2} \bar{u} + \underline{PX3} \bar{f}_k$$

where

\bar{s} , \bar{u} , and \bar{f}_k are defined above.

$$\underline{PX1} = \begin{bmatrix} PX_{ij} \end{bmatrix} \quad 1 \times 25 \quad \text{Coefficient Matrix}$$

$$\underline{PX2} = \begin{bmatrix} PX_{ij} \end{bmatrix} \quad 1 \times 3 \quad \text{Coefficient Matrix}$$

$$\underline{PX3} = \begin{bmatrix} PX_{ij} \end{bmatrix} \quad 1 \times 1 \quad \text{Coefficient Matrix}$$

3. Constraints

Constraints in matrix form are expressed as

$$\underline{YL} \leq \underline{Y1}\bar{s} + \underline{Y2}\bar{u} + \underline{Y3}\bar{f}_k \leq \underline{YU}$$

where

\bar{s} , \bar{u} , and \bar{f}_k are defined above.

$$\underline{YL} = \begin{bmatrix} YL_{ij} \end{bmatrix} \quad 6 \times 1 \quad \text{Lower Limit}$$

$$\underline{Y1} = \begin{bmatrix} Y1_{ij} \end{bmatrix} \quad 6 \times 25 \quad \text{Coefficient Matrix}$$

$$\underline{Y2} = \begin{bmatrix} Y2_{ij} \end{bmatrix} \quad 6 \times 3 \quad \text{Coefficient Matrix}$$

$$\underline{Y3} = \begin{bmatrix} Y3_{ij} \end{bmatrix} \quad 6 \times 1 \quad \text{Coefficient Matrix}$$

$$\underline{YU} = \begin{bmatrix} YU_{ij} \end{bmatrix} \quad 6 \times 1 \quad \text{Upper limit}$$

The specification matrix is given by

$$MSP = \begin{bmatrix} 0 & 0 \\ 0 & 1 \\ 0 & 3 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$$

4. Output

The desired output vector \bar{V} is given by

$$\bar{V} = \underline{Q1} \bar{s} + \underline{Q2} \bar{u} + \underline{Q3} \bar{f}_k$$

where

$$\bar{V} = \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \\ V_5 \\ V_6 \end{bmatrix} \quad \begin{array}{l} \text{Pressure} \\ \text{Temperature} \\ \text{Time derivative of temperature} \\ \text{Rod speed} \\ \text{Spray} \\ \text{Heater} \end{array}$$

$$\underline{Q1} = \begin{bmatrix} Q_{ij} \end{bmatrix} \quad 6 \times 25 \quad \text{Coefficient Matrix}$$

$$\underline{Q2} = \begin{bmatrix} Q_{ij} \end{bmatrix} \quad 6 \times 3 \quad \text{Coefficient Matrix}$$

$$\underline{Q3} = \begin{bmatrix} Q_{ij} \end{bmatrix} \quad 6 \times 1 \quad \text{Coefficient Matrix}$$

Trade-off relations between the minimum value of the pressurizer pressure and the output vector \bar{V} shown above can be obtained by varying the bounds $\bar{Y}L$ and $\bar{Y}U$.

SECTION V

CONCLUSIONS

A computational capability, PERFORM, for the evaluation of the limiting performance of transient dynamic systems has been developed and is described in this report. This capability is intended to be used by a designer of dynamic systems to determine the feasibility of the proposed design specifications. Thus, PERFORM is meant to be a new design tool.

In addition to being able to use PERFORM to scrutinize design specifications, this capability can be used during the actual design process to measure the relative success of proposed designs with the characteristics of the theoretically best design provided by PERFORM.

PERFORM is used in an engineering problem-oriented form. The user prescribes in a simple fashion the system equations of motion, sets of constraints, objective functions, and classes of possible inputs. The capability then automatically computes the limiting performance characteristics requested by the user.

SECTION VI

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APPENDIX I

USERS GUIDE FOR PERFORM

PERFORM is a computer system that can be used to determine the limiting performance characteristics of a dynamic system described by a system of first or second order equations of motion. The information, including input requirements, necessary to use PERFORM is described in this appendix.

A. PERFORM Utilization Procedure

This section describes the steps necessary to solve a limiting performance problem with the PERFORM system. Essentially this is a statement of the details of the system flowchart of Fig. 1, Section III.

1. Prepare the limiting performance problem specification data. This input is described in detail in the following sections of this appendix. In the system flowchart this input is labeled "PERFORM problem specification data."
2. Run PREPROC using the data of Step 1. There are two card outputs of this program; the PSTPROC Report data and the linear programming problem data for the LP Solver.

Hold the PSTPROC report data output for use in Step 6.

If several sets of constraints are being run for trade-off relations, one LP Solver data deck will be produced for each different constraint.

Deck preparation for compiling and executing the PREPROC program is shown in Fig. I-1. The details of the leading control cards depend on the operating system of the computer and any user desired system option.*

3. Transmit the linear programming program data to the external computer, i.e. the computer with either MPS/360 or a MPS/360 compatible linear programming software, for solution of the linear programming problem.

* If recurring use of PERFORM were anticipated, excessive recompilation can be avoided by storing the program, in object form, on the system library. The indicated deck structure would then have to be appropriately modified.

4. Run MPS/360, or compatible software, to obtain the problem solution. For each constraint deck produced one execution of MPS is required; however, only one job and transmission is required.

The deck contents for an MPS/360 run is shown in Fig. I-2. This model, in general, would be correct for any MPS/360 installation using OS/360. Words in upper case letters are invariant among jobs and installations. Words in lower case letters depend on the job and installation. Those dependent on the job are user chosen to identify the problem. Those dependent on the installation should be obtained from system personnel.

Because of possible idiosyncrasies of the external computer, consultation with system personnel before attempted use is imperative.

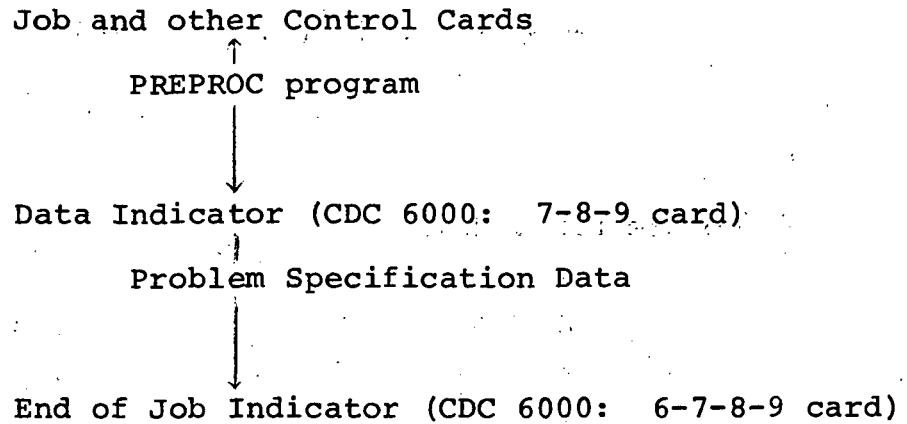
5. Receive from the external computer the linear programming problem solution. This can be either in card form via courier or by telecommunications if facilities are available.
6. Run PSTPROC using the MPS/360 linear programming solution data received in Step 5 and the PSTPROC report data of Step 1.

Fig. I-3 shows the deck structure for this run. The details of the leading control cards depend on the operating system being used and any user desired system options.*

The different linear programming solution decks must be physically concentrated behind the PSTPROC data. The importance of careful card handling cannot be understated since the existing PERFORM system has no facilities for error detection.

The limiting performance problem solution is output in this step.

* As indicated in the discussion of Step 2, it may be advisable to place the PSTPROC program on the system library.



(Lines Represent Decks of Cards)

Figure I-1 PREPROC Deck Structure.

Compile and Execute

```
// Job-name      JOB      account data
//              EX      MPS-procedure-name
// Compile-step-name. SYSIN      DD      *
```

MPS/360 CONTROL PROGRAM

/*

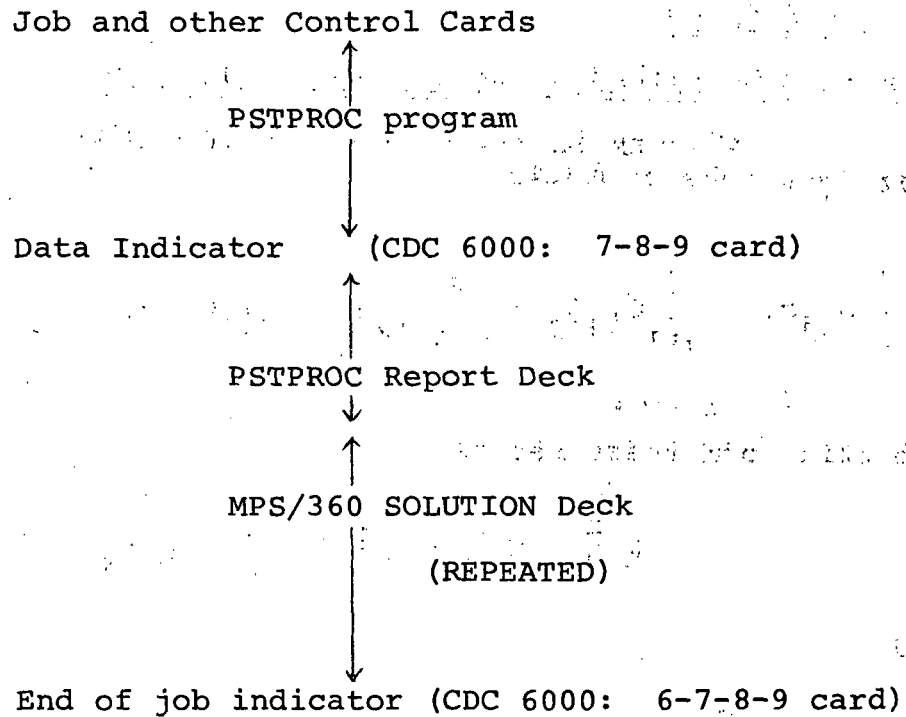
```
// Go-stepname.SYSIN      DD      *
```

MPS/360 LINEAR PROGRAMMING DATA

/*

(Lines Represent Decks of Card)

Figure I-2 MPS/360 Execution Deck



(Lines Represent Decks of Card)

Figure I-3 PSTPROC Deck Structure

Compile and Execute

B. Input for PERFORM

1. System Described by Second Order Equations

PERFORM treats svstems described by the second order equations of motion

$$\sum_{j=1}^n M_{ij} \ddot{q}_j + \sum_{j=1}^n C_{ij} \dot{q}_j + \sum_{j=1}^n K_{ij} q_j + \sum_{j=1}^{nu} U_{ij} u_j = \sum_{j=1}^{nf} F_{ij} f_{kj} \quad (I-1)$$

$i = 1 \text{ to } n$

in matrix form these become

$$\underline{M} \ddot{\underline{q}} + \underline{C} \dot{\underline{q}} + \underline{K} \underline{q} + \underline{U} \underline{u} = \underline{F} \underline{\bar{f}}_k \quad (I-2)$$

where

$$\underline{\bar{q}} = \begin{bmatrix} q_1 \\ q_2 \\ \vdots \\ q_n \end{bmatrix} \quad \begin{array}{l} \text{displacement vector} \\ n \times 1 \end{array}$$

$$\dot{\underline{q}} = \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \vdots \\ \dot{q}_n \end{bmatrix} \quad \begin{array}{l} \text{velocity vector} \\ n \times 1 \end{array}$$

$$\ddot{\mathbf{q}} = \begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \\ \vdots \\ \ddot{q}_n \end{bmatrix} \quad n \times 1$$

acceleration vector

$$\bar{\mathbf{u}} = \begin{bmatrix} u_1 \\ u_2 \\ \vdots \\ u_{nu} \end{bmatrix} \quad nu \times 1$$

control force vector

$$\mathbf{f}_k = \begin{bmatrix} f_{k1} \\ f_{k2} \\ \vdots \\ f_{knf} \end{bmatrix} \quad nf \times 1$$

forcing function vector. The subscript k identifies the set of forcing functions, e.g. f_{21} is the first element of the second set of forcing functions. This allows the system to encounter alternate sets of forcing functions which might occur with equal probability.

$$\underline{\mathbf{M}} = \begin{bmatrix} M_{11} & M_{12} & \cdots & M_{1n} \\ M_{21} & M_{22} & \cdots & M_{2n} \\ \vdots & & & \\ M_{n1} & M_{n2} & \cdots & M_{nn} \end{bmatrix} = [\mathbf{M}_{ij}]_{n \times n} \quad \text{mass matrix}$$

$$\underline{C} = [C_{ij}]_{n \times n}$$

damping matrix

$$\underline{K} = [K_{ij}]_{n \times n}$$

spring matrix

$$\underline{U} = [U_{ij}]_{n \times nu}$$

matrix of constants
associated with control force

$$\underline{F} = [F_{ij}]_{n \times nf}$$

matrix of constants
associated with external
disturbances

The user should place his equations of motion in the form of Eq. (I-2). The non-zero elements of the matrices \underline{M} , \underline{C} , \underline{K} , \underline{U} , \underline{F} are then entered as inputs in the form explained subsequently. This is accomplished by identifying the matrix, e.g., \underline{M} MATRIX, and then specifying an element and its value, e.g., i , j and M_{ij} . Elements not entered are assumed to be zero.

Example 1

The equations of motion for a system shown in Fig. I-4 can be written as

$$m_1 \ddot{x} + k(x-y) + u = m_1 g + h_k(t) \quad (I-3)$$

$$m_2 \ddot{y} + c\dot{y} + k(y-x) = m_2 g$$

Put in matrix form

$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{x} \\ \ddot{y} \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & c \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} + \begin{bmatrix} k & -k \\ -k & k \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} [u] =$$

$$\begin{bmatrix} m_1 & 1 \\ m_2 & 0 \end{bmatrix} \begin{bmatrix} g \\ h_k(t) \end{bmatrix} \quad (I-4)$$

Now define

$$x = q_1 \quad y = q_2$$

$$\bar{q} = \begin{bmatrix} x \\ y \end{bmatrix}$$

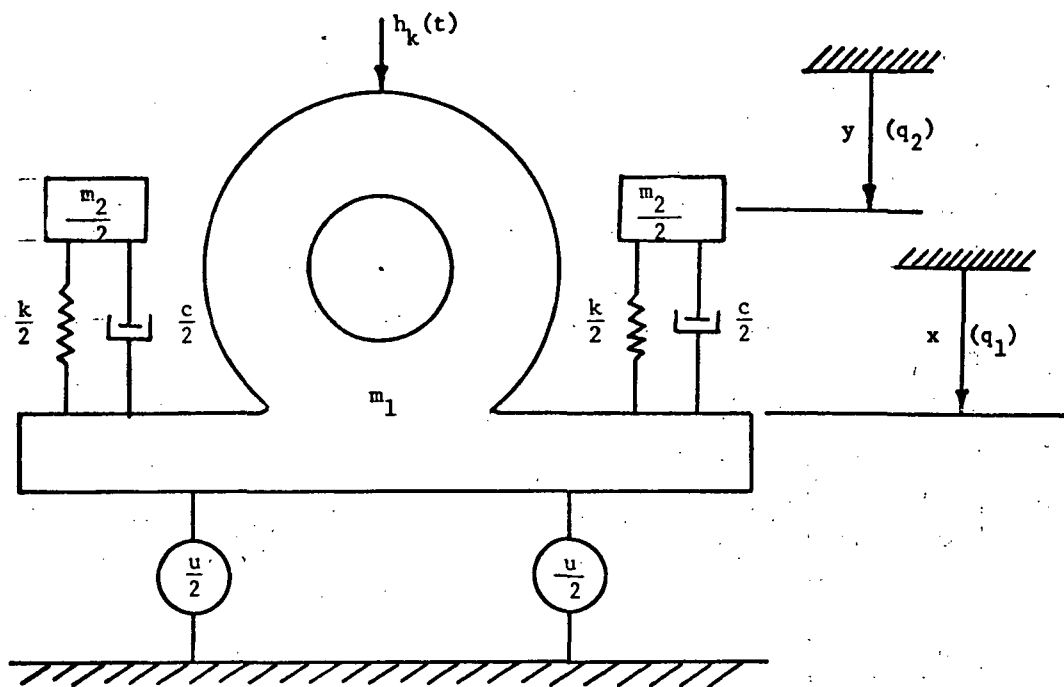


Fig. I-4

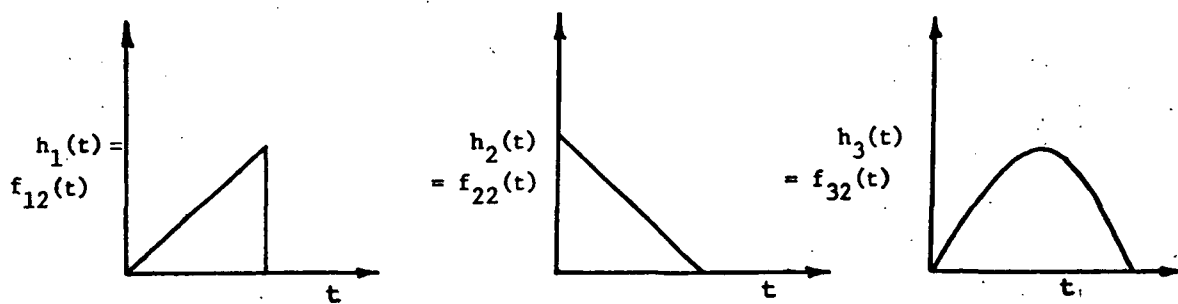


Fig. I-5

$$\dot{\underline{q}} = \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix}$$

$$\ddot{\underline{q}} = \begin{bmatrix} \ddot{x} \\ \ddot{y} \end{bmatrix}$$

$$\underline{u} = \begin{bmatrix} u \end{bmatrix}$$

$$\underline{M} = \begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix}$$

(I-5)

$$\underline{C} = \begin{bmatrix} 0 & 0 \\ 0 & c \end{bmatrix}$$

$$\underline{K} = \begin{bmatrix} k & -k \\ -k & k \end{bmatrix}$$

$$\underline{U} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

$$\underline{F} = \begin{bmatrix} m_1 & 1 \\ m_2 & 0 \end{bmatrix}$$

$$\underline{\bar{f}}_k = \begin{bmatrix} g \\ h_k(t) \end{bmatrix}$$

Note that the k subscript of \bar{f} designates one set of forcing functions. In our case $f_{k1} = g =$ gravitational acceleration constant while $f_{k2} = h_k(t) =$ some function of time, e.g. those in Fig. I-5. If f_{12} , f_{22} , and f_{32} of Fig. I-5 were all to be included in the input, then these disturbances would be treated as though all are potential forcing functions that may occur with equal probability. Using Eqs. (I-5), Eq. (I-4) becomes

$$\underline{M} \ddot{\underline{q}} + \underline{C} \dot{\underline{q}} + \underline{K} \underline{q} + \underline{U} \underline{u} = \underline{F} \underline{f}_k \quad (\text{I-6})$$

2. System Described by First Order Equations

The first order equations of motion accepted by the computer system are expressed as

$$\dot{\underline{s}} = \underline{A} \underline{s} + \underline{B} \underline{u} + \underline{D} \underline{f}_k \quad (\text{I-7})$$

where

$$\underline{s} = \begin{bmatrix} s_1 \\ s_2 \\ \vdots \\ s_m \end{bmatrix}$$

state vector

m x 1

$$\dot{\underline{s}} = \begin{bmatrix} \dot{s}_1 \\ \dot{s}_2 \\ \vdots \\ \dot{s}_m \end{bmatrix}$$

time derivative of state vector

m x 1

$$\underline{A} = [A_{ij}]_{m \times m} \quad \text{coefficient matrix}$$

$$\underline{B} = [B_{ij}]_{m \times nu} \quad \text{coefficient matrix}$$

$$\underline{D} = [D_{ij}]_{m \times nf} \quad \text{coefficient matrix}$$

m = number of equations in the system of equations

The user should input non-zero elements of matrices A, B, D in the form explained later. This is accomplished by identifying the matrices; e.g., A MATRIX, and then specifying an element and its value, e.g., i, j and A(i,j). Elements not entered are assumed to be zero.

Example 2

Equations of motion for the system shown in Fig. I-6 can be written as

$$C_1 \frac{dh_1}{dt} = -\frac{h_1 - h_2}{R_1} + e(t)$$

$$C_2 \frac{dh_2}{dt} = \frac{h_1 - h_2}{R_1} - \frac{h_2}{R_2} + E_k(t) \quad \text{or}$$

$$\frac{dh_1}{dt} = \frac{-1}{R_1 C_1} h_1 + \frac{1}{R_1 C_1} h_2 + \frac{1}{C_1} e(t) \quad (\text{I-8})$$

$$\frac{dh_2}{dt} = \frac{1}{R_1 C_2} h_1 - \left(\frac{1}{R_1 C_2} + \frac{1}{R_2 C_2} \right) h_2 + \frac{1}{C_2} E_k(t)$$

The system of Eqs. (I-8) is equivalent to

$$\dot{\bar{s}} = \underline{A} \bar{s} + \underline{B} \bar{u} + \underline{D} \bar{f}_k \quad (\text{I-9})$$

where

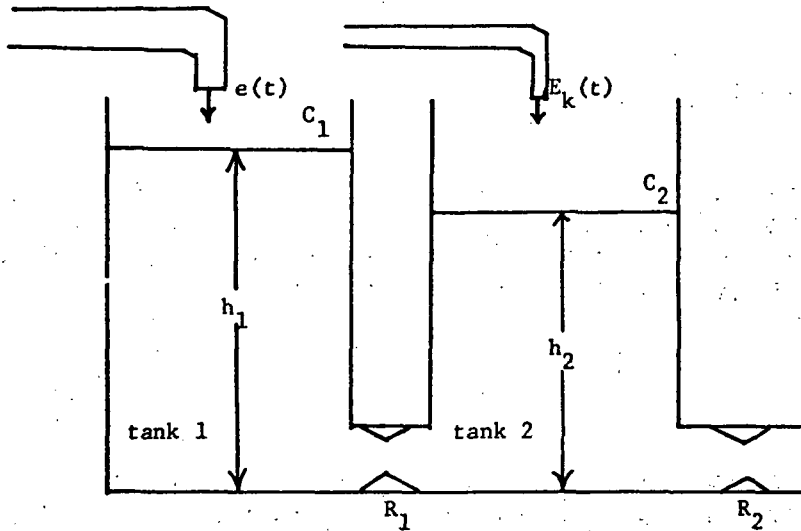
$$\bar{s} = \begin{bmatrix} h_1 \\ h_2 \end{bmatrix}$$

$$\bar{u} = [e(t)]$$

$$\bar{f}_k = [E_k(t)]$$

$$\underline{A} = \begin{bmatrix} -\frac{1}{R_1 C_1} & \frac{1}{R_1 C_1} \\ \frac{1}{R_1 C_2} & -\left(\frac{1}{R_1 C_2} + \frac{1}{R_2 C_2} \right) \end{bmatrix}$$

$$\underline{B} = \begin{bmatrix} \frac{1}{C_1} \\ 0 \end{bmatrix}$$



h_1, h_2 = liquid level in tank 1,2 respectively

C_1, C_2 = cross sectional area of tank 1, 2 respectively

R_1, R_2 = orifice resistances

Flow rate through orifice = $\frac{h}{R}$ (assumption)

Fig. I-6 Two-tank liquid-level system

$$\underline{D} = \begin{bmatrix} 0 \\ \frac{1}{C_2} \end{bmatrix}$$

3. Objective Function

Regardless of the form (first or second order) used to describe the equations of motion, the format for the objective function is the same. In the case of the second order equations, the user should establish a state variable vector \bar{s} as

$$\bar{s} = \begin{bmatrix} \dot{\bar{q}} \\ \ddots \\ \bar{q} \end{bmatrix} \quad (I-10)$$

The user can choose any linear combination of state variables, derivatives of state variables, or control forces as an objective function. In the case of the system described by second order equations, these become linear combinations of accelerations, velocities, displacements and control forces. PERFORM finds the vector \bar{u} that minimizes the maximum (ISP = 0) (or maximizes the minimum (ISP = 1)) time values of the functions used as objective functions while satisfying the constraints. The objective function is formed as

$$\underline{PX1}\bar{s} + \underline{PX2}\bar{u} + \underline{PX3}\bar{f}_k \quad (I-11)$$

If more than one row of the matrices in Eq. (I-11) contains non-zero elements, then the peak values in time of the vectors resulting from the meaningful rows are to be compared. PERFORM minimizes (maximizes) the maximum (minimum) of the peak values.

Example 3

To illustrate the formation of an objective function, consider the 2-degree-of-freedom (DOF) system in Example 1. The equations of motion are given as Eqs. (I-3). Suppose we have only one set of forcing functions. We assume the objective function is to minimize the maximum of the peak values of $|\ddot{x}|$; $|\ddot{y}|$; $|\dot{x} - \dot{y}|$. From Eqs. (I-3) \ddot{y} and \ddot{x} can be expressed as

$$\ddot{x} = \frac{-k}{m_1} x + \frac{k}{m_1} y - u + g + \frac{h_k(t)}{m_1}$$

$$\ddot{y} = \frac{-c}{m_2} \dot{y} + \frac{k}{m_2} x - \frac{k}{m_2} y + g$$

Then the objective function involves

$$\begin{aligned} & \left| -\frac{k}{m_1} x + \frac{k}{m_1} y - u + g + \frac{h_k(t)}{m_1} \right| \\ & \left| -\frac{c}{m_2} \dot{y} + \frac{k}{m_2} x - \frac{k}{m_2} y + g \right| \\ & \left| \dot{x} - \dot{y} \right| \end{aligned} \quad (I-12)$$

PERFORM will minimize the maximum of peak values of these three relations. In terms of the form required for PERFORM, we write

$$\bar{s} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ x \\ y \end{bmatrix}$$

$$\bar{u} = [u]$$

$$\bar{f}_k = \begin{bmatrix} g \\ h_k(t) \end{bmatrix}$$

so that the objective function becomes

$$\begin{bmatrix} 0 & 0 & \frac{-k}{m_1} & \frac{k}{m_1} \\ 0 & -\frac{c}{m_2} & \frac{k}{m_2} & \frac{-k}{m_2} \\ 1 & -1 & 0 & 0 \end{bmatrix} \bar{s} + \begin{bmatrix} -1 \\ 0 \\ 0 \end{bmatrix} \bar{u} + \begin{bmatrix} 1 & \frac{1}{m_1} \\ 1 & 0 \\ 0 & 0 \end{bmatrix} \bar{f}_k \quad (I-13)$$

Thus in Eq. (I-11),

$$\underline{PX1} = \begin{bmatrix} 0 & 0 & \frac{-k}{m_1} & \frac{k}{m_1} \\ 0 & \frac{-c}{m_2} & \frac{k}{m_2} & \frac{-k}{m_2} \\ 1 & -1 & 0 & 0 \end{bmatrix}$$

$$\underline{PX2} = \begin{bmatrix} -1 \\ 0 \\ 0 \end{bmatrix}$$

$$\underline{PX3} = \begin{bmatrix} 1 & \frac{1}{m_1} \\ 1 & 0 \\ 0 & 0 \end{bmatrix}$$

4. Constraints

Constraints, like objective functions, are treated the same regardless of whether the equations of motion are expressed in first or second order form. Constraints may be placed on state variables, derivatives of state variables, and control forces (accelerations, velocities, displacements and control forces for systems described by second order equations). The general form is

$$\underline{YL} \leq \underline{Y1s} + \underline{Y2u} + \underline{Y3f_k} \leq \underline{YU} \quad (I-14)$$

Each row in Eq. (I-14) represents one constraint. A specification matrix (MSP) is needed to specify the nature of each constraint. MSP is a matrix of two columns with rows equal in numbers to the rows in Eq. (I-14). The elements of MSP are given integer values defined as follows:

$$\begin{aligned}
 \text{MSP}(I,1) &= \begin{cases} 0 & \text{if the } i^{\text{th}} \text{ constraint (row) is continuous} \\ & \text{(i.e., is to be imposed at many times)} \\ 1 & \text{if the } i^{\text{th}} \text{ constraint is imposed only at} \\ & \text{some specific time.} \end{cases} \\
 \text{MSP}(I,2) &= \begin{cases} 0 \\ 1 \\ 2 \\ 3 \end{cases} \begin{array}{l} \text{means the } i^{\text{th}} \text{ constraints} \\ \text{are of the type respectively} \end{array} \left\{ \begin{array}{l} \leq \leq \\ \leq \\ \geq \\ = \end{array} \right\}
 \end{aligned}$$

Example 4

For the same system of Example 1 suppose we want the constraints

$$\begin{aligned}
 b(t) &\leq u(t) \leq a(t) && \text{for all } t \\
 d_1 &\leq x \leq d_2 && \text{for } t_1 \text{ only} \\
 y &\leq d_3 && \text{for all } t \\
 \dot{x}(t_2) &= v_0 && \text{for } t_2 \text{ only}
 \end{aligned}$$

In matrix form

$$\begin{bmatrix} b(t) \\ d_1 \\ - \\ - \end{bmatrix} \leq \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \\ x \\ y \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} [u] + \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} g \\ h(t) \end{bmatrix} \begin{array}{l} \leq \\ \text{or} \\ = \end{array} \begin{bmatrix} a(t) \\ d_2 \\ d_3 \\ v_0 \end{bmatrix}$$

The specification matrix is given by

$$\underline{\text{MSP}} = \begin{bmatrix} 0 & 0 \\ 1 & 0 \\ 0 & 1 \\ 1 & 3 \end{bmatrix}$$

5. Output

Any linear combination of \bar{s} , \bar{u} , \bar{f} can be tabulated versus time. The user inputs matrices Q1, Q2, Q3 in the equation

$$\underline{Q1} \bar{s} + \underline{Q2} \bar{u} + \underline{Q3} \bar{f}_k$$

The dimensions of matrices Q1, Q2, Q3 are $m \times \text{not}$, $\text{nu} \times \text{not}$, $\text{nf} \times \text{not}$, respectively, where m is the number of state variables and not is the number of outputs required. A specific set of forcing functions, i.e., ISET(I), must be designated for each quantity to be tabulated. The user can also get trajectories of any one of the quantities tabulated.

A trade-off curve between the objective function and any one constraint can be obtained by varying the bound of that constraint. The bounds that can be varied must be of the constant type (i.e., NCN = 0). For a constraint with both upper and lower bounds the user can either vary both bounds at some increment or keep one bound constant and only vary the other one. The details of the implementation of the constraint variation are given later in this Appendix.

Example 5

Suppose for the system in Example 2 we want to have the water level $h_1(t)$, $h_2(t)$ and the controlled input $e(t)$ to be tabulated as functions of time. Then

$$\underline{Q1} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ 0 & 0 \end{bmatrix}$$

$$\underline{Q2} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

$$\underline{Q3} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

If we set $ITR(1) = 1, ITR(2) = 1, ITR(3) = 1$ then the time trajectories of $h_1(t)$, $h_2(t)$ and $e(t)$ will be tabulated and plotted.

Let the goal in Example 2 be to minimize the maximum value of objective functions $|h_1(t)|$ and $|h_2(t)|$ with the constraint $|h_1(t)| \leq D$. Then for each prescribed value of D we can obtain a minmax value of the objective functions. By varying D we can compute a tradeoff curve.

6. Input Format

Words not underlined are variables used in the code. The underlined words marked with * are required in the input. Those underlined words marked with ** are required only if the data they designate are to be entered as part of the problem. For example, for a problem with no initial conditions (i.e. all initial conditions are zero), the card with INITIAL CONDITIONS is not needed.

The order of the word-cards is immaterial as long as the appropriate data follows the proper word. For example, the K MATRIX card and its data can be placed before or after the M MATRIX card and its data.

7. Limitations as to Size of Problems

The size of problems that can be solved by the program listed in this report is restricted by the DIMENSION statements in the program. The following are the current maximum sizes of important parameters.

$NU=5, NF=5, NSETS=1, II=20, NOB=3, NOC=5, NOT=10$, and the combination of the above parameters should be such that

$R_H \leq 120$, $C_H \leq 40$ (See Section D of Appendix III)*.

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
1	1	blank		
	2-6	NPB	(I5)	problem number
	7-10	blank		
	11-70	TITLE	(12A5)	any written title or description of the problem
	71-80	blank		
2	1-5	blank		
	6	NOE	(I1)	= 1 input system of 1 st order equations = 2 input system of 2 nd order equations
	7-10	blank		
	11-15	blank		
	16-18	blank		
	19-20	NDF	(I2)	number of equations of motion
	21-23	blank		
	24-25	NU	(I2)	number of controllers of the system
	26-30	NF	(I5)	number of elements in each set of forcing functions of the system
	31-35	NSETS	(I5)	number of sets of forcing functions (= 1 even if there are no forcing functions)

* A variable dimensioned version of PREPROC is available for use on the NASA Langley Computer Operating System (CDC 6600). Dimensional constraints are removed in an automated version of PERFORM at the University of Virginia Computer Science Center (CDC 6400)

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
	36-40	II	(I5)	= 1 + number of time intervals for discretizing control forces
	41-50	TM	(F10.6)	value of time interval
	51-55	NOB	(I5)	total number of objective functions
	56-60	NOC	(I5)	total number of constraints
	61-64	blank		
	65	ISP	(I1)	= 0 minimize the maximum of objective functions = 1 maximize the minimum of objective functions
	66-70	NOT	(I5)	number of outputs
	71-80	blank		
3	1-60	ISET (1) ISET (2) ⋮ ISET (NOT)	(6I10)	where ISET (I) designates the set forcing functions required by ith output; read in up to 6 values per
	61-80	blank		with additional cards as needed
----- FORCING FUNCTION -----				
4	1-16	<u>FORCING FUNCTION</u>	**	
	17-80	blank		
4-1	1	KEY2	(I1)	= 0 continue to read data, e.g., cards 4-2 are still to be read in = 1 last data card, e.g., if NSETS = 1, then last set has been reached
	2-6	I	(I5)	the ith set of forcing functions
	7-80	blank		

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
4-1-1	1	KEY1	(I1)	= 0 continue to read data, e.g. 4-1-2 = 1 last data card
	2-6	J	(I5)	the j th element of i th set
	7-10	blank		
	11-80	blank		
4-1-1-1	1	KEY	(I1)	= 0 continue to read data = 1 last data card
	2-6	K	(I5)	discretized time (1 to (II-1))
	7-11	blank		
	12-23	F(I,K,J)	(F12.6)	value of j th element of i th set forcing function at time K
	24-80	blank		repeat until all non-zero elements of F(I,K,J) are input
				The whole deck would look like
				4
				4-1 4-2
				4-1-1 4-2-1
				4-1-1-1 4-2-1-1
				4-1-1-2 4-2-1-2
				4-1-1-3 4-2-1-3
				⋮ ⋮
				4-1-2 4-2-2
				4-1-2-1 4-2-2-1
				4-1-2-2 4-2-2-2

<u>Card No.</u>	<u>Columns</u>	<u>Variable Format</u>	<u>Comments</u>
		4-1-2-3	4-2-2-3
		:	: etc.

 INITIAL CONDITIONS

5	1-17	<u>INITIAL CONDITION**</u>	only non-zero initial conditions are to be entered
	18-80	blank	
5- 1	1	KEY (I1)	= 0 continue to read data cards = 1 last data card
	2-6	I (I5)	the i^{th} element of the state vector \bar{s}
	7-10	blank	
	11-22	S (1,I) (F 12.6)	the value of s(1,I)
	23-80	blank	continue with card 5-2, etc. until all non-zero elements of S(1,I) are input
			5-2 has the same format as 5-1
			The initial conditions are the values of the response (state) variables at the initial time

 FIRST ORDER EQUATIONS OF MOTION ($\dot{\bar{s}} = \underline{A}\bar{s} + \underline{B}\bar{u} + \underline{D}\bar{f}_k$)

6	1-8	<u>A MATRIX**</u>	
	9-80	blank	
6-1	1	KEY (I1)	= 0 continue to read data of <u>A</u> = 1 last data card of <u>A</u>
	2-6	I (I5)	

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
	7-11	J	(I5)	
	12-23	A(I,J)	(F12.6)	value of A(I,J)
	24-80	blank		repeat card 6-2, etc. until all non-zero elements of <u>A</u> are input
7	1-8	<u>B MATRIX**</u>		
	9-80	blank		
7-1	1	KEY	(I1)	= 0 continue to read data of <u>B</u> = 1 last data card of <u>B</u>
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	B(I,J)	(F12.6)	value of B(I,J)
	24-80	blank		repeat card 7-2, etc., until all non-zero elements of <u>B</u> are input.
8	1-8	<u>D MATRIX**</u>		
	9-80	blank		
8-1	1	KEY	(I1)	= 0 continue to read data of <u>D</u> = 1 last data card of <u>D</u>
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	D(I,J)	(F12.6)	value of D(I,J)
	24-80	blank		repeat 8-2, etc. until all non-zero elements of <u>D</u> are input.

 SECOND ORDER EQUATIONS OF MOTION ($\underline{M}\ddot{\underline{q}} + \underline{C}\dot{\underline{q}} + \underline{K}\underline{q} + \underline{U}\underline{u} = \underline{F}\underline{f}_k$)

9	1-8	<u>M MATRIX**</u>		
	9-80	blank		
9-1	1	KEY	(I1)	= 0 continue to read data of <u>M</u> = 1 last data of <u>M</u>

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	M(I,J)	(F12.6)	value of M(I,J)
	24-80	blank		repeat until all non-zero elements of <u>M</u> are input
10	1-8	<u>C MATRIX</u> **		
	9-80	blank		
10	1	KEY	(I1)	= 0 continue to read data of <u>C</u> = 1 last data card of <u>C</u>
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	C(I,J)	(F12.6)	value of C(I,J)
	24-80	blank		repeat until all non-zero elements of <u>C</u> are input
11	1-8	<u>K MATRIX</u> **		
	9-80	blank		
11-1	1	KEY	(I1)	= 0 continue to read data of <u>K</u> = 1 last data card of <u>K</u>
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	K(I,J)	(F12.6)	value of K(I,J)
	24-80	blank		repeat until all non-zero elements of <u>K</u> are input
12	1-8	<u>F MATRIX</u> **		
	9-80	blank		
12-1	1	KEY	(I1)	= 0 continue to read data of <u>F</u> = 1 last data card of <u>F</u>
	2-6	I	(I5)	

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
	7-11	J	(I5)	
	12-23	F(I,J)	(F12.6)	value of F(I,J)
	24-80	blank		repeat until all non-zero elements of <u>F</u> are input
13	1-8	<u>U MATRIX**</u>		
	9-80	blank		
13-1	1	KEY	(I1)	= 0 continue to read data of <u>U</u> = 1 last data card of <u>U</u>
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	U(I,J)	(F12.6)	value of U(I,J)
	24-80	blank		repeat until all non-zero elements of <u>U</u> are input
<p>----- OBJECTIVE FUNCTION (<u>PX1</u>\bar{s} + <u>PX2</u>\bar{u} + <u>PX3</u>\bar{f}_k) -----</p>				
14	1-10	<u>PX1 MATRIX**</u>		
	11-80	blank		
14-1	1	KEY	(I1)	= 0 continue to read data of <u>PX1</u> = 1 last data card of <u>PX1</u>

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	PX1(I,J)	(F12.6)	value of PX1(I,J)
	24-80	blank		repeat until all non-zero elements of <u>PX1</u> are input
15	1-10	<u>PX2 MATRIX**</u>		
	11-80	blank		
15-1	1	KEY	(I1)	= 0 continue to read data of <u>PX2</u> = 1 last data card of PX2
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	PX2(I,J)	(F12.6)	value of PX2(I,J)
	24-80	blank		repeat until all non-zero elements of <u>PX2</u> are input
16	1-10	<u>PX3 MATRIX**</u>		
	11-80	blank		
16-1	1	KEY	(I1)	= 0 continue to read data of <u>PX3</u> = 1 last data of <u>PX3</u>
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	PX3(I,J)	(F12.6)	value of PX3(I,J)
	24-80	blank		repeat until all non-zero elements of <u>PX3</u> are input

CONSTRAINTS ($\bar{Y}_L < \bar{Y}_{1s} + \bar{Y}_{2u} + \bar{Y}_{3f_k} < \bar{Y}_U$)				

17	1-9	<u>Y1 MATRIX**</u>		
	10-80	blank		

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
	1	KEY	(I1)	= 0 continue to read data of <u>Y1</u> = 1 last data card of <u>Y1</u>
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	Y1(I,J)	(F12.6)	value of Y1(I,J)
	24-80	blank		repeat until all non-zero elements of <u>Y1</u> are input
18	1-10	<u>Y2 MATRIX**</u>		
	11-80	blank		
18-1	1	KEY	(I1)	= 0 continue to read data of <u>Y2</u> = 1 last data card of <u>Y2</u>
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	Y2(I,J)	(F12.6)	value of Y2(I,J)
	24-80	blank		repeat until all non-zero elements of <u>Y2</u> are input
19	1-10	<u>Y3 MATRIX**</u>		
	11-80	blank		
19-1	1	KEY	(I1)	= 0 continue to read data of <u>Y3</u> = 1 last data of <u>Y3</u>
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	Y3(I,J)	(F12.6)	value of Y3(I,J)
	24-80	blank		repeat until all non-zero elements of <u>Y3</u> are input
20	1-21	<u>BOUNDS OF CONSTRAINTS**</u>		
	22-80	blank		

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
20-1	1	KEY1	(I1)	= 0 continue to read data card (20-2) = 1 last data card
	2-6	I	(I5)	the i^{th} constraint
	7-9	blank		
	10	MSP(I,1)	(I1)	= 0 i^{th} constraint is for all times = 1 i^{th} constraint is for specific time
	11-19	blank		
	20	MSP(I,2)	(I1)	= 0 $\leq \leq$ type constraint = 1 \leq type constraint = 2 \geq type constraint = 3 = type constraint
	21-80	blank		
If MSP(I,1) = 0 and				MSP(I,2) = 0 GOTO 22-1AU then go to 22-1AL MSP(I,2) = 1 GOTO 22-1BU MSP(I,2) = 2 GOTO 22-1CL MSP(I,2) = 3 GOTO 22-1DU
If MSP(I,1) = 1 and				MSP(I,2) = 0 GOTO 22-1EU then go to 22-1EL MSP(I,2) = 1 GOTO 22-1FU MSP(I,2) = 2 GOTO 22-1GL MSP(I,2) = 3 GOTO 22-1HU
(Use the following if MSP(I,1) = 0, MSP(I,2) = 0)				
22-1AU	1	blank		

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
	2	NCN	(I1)	= 0 constant upper bound (GO TO 22-1AU-A) = 1 piecewise constant upper bound (GO TO 22-1AU-1)
	3-80	blank		
22-1AU-A	1-12	SVA1	(F12.6)	starting value
	13-17	NIC1	(I5)	number of increments (use 0 if there are no increments)
	18-29	VIC1	(F12.6)	value of increment
	30-80	blank		(GO TO 22-1AL)
22-1AU-1	1	KEY	(I1)	= 0 continue to read data = 1 last data card
	2-6	K	(I5)	discretized time
				NOTE: K = 2 to II if Y2(I,J) = 0 for all J K = 1 to II - 1 if Y1(I,J) = 0 for all J K = 2 to II - 1 if Y1(I,J) \neq 0 and Y2(I,J) \neq 0 for some J
	7-11	blank		
	12-23	YU(K,1)	(F12.6)	
	24-80	blank		repeat 11-1AU-2, etc.
22-1AL	1	blank		
	2	NCN	(I1)	= 0 constant lower bound (GO TO 22-1AL-A) = 1 piecewise constant lower bound (GO TO 22-1AL-1)
	3-80	blank		
22-1AL-A	1-12	SVA2	(F12.6)	starting value
	13-17	NIC2	(I5)	number of increments (use 0 if there are no increments)

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
	18-29	VIC2	(F12.6)	value of increment
	30-80	blank		
22-1AL-1	1	KEY	(I1)	= 0 continue to read data = 1 last data card
	2-6	K	(I5)	discretized time
NOTE: K = 2 to II if Y2(I,J) = 0 for all J K = 1 to II-1 if Y1(I,J) = 0 for all J K-2 to II-1 if Y1(I,J) \neq 0 and Y2(I,J) \neq 0 for some J				
	7-11	blank		
	12-23	YL(K,I)	(F12.6)	
	24-80	blank		repeat 22-1AL-2, etc.
(Use the following if MPS(I,1) = 0 and MPS(I,2) = 1)				
22-1BU	1	blank		
	2	NCN	(I1)	= 0 constant upper bound (GO TO 22-1BU-A) = 1 piecewise constant upper bound (GO TO 22-1BU-1)
	3-80	blank		
22-1BU-A	1-12	SVA1	(F12.6)	starting value
	13-17	NIC1	(I5)	number of increments (use 0 if there are no increments)
	18-29	VIC1	(F12.6)	value of increment
	30-80	blank		

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
22-1BU-1	1	KEY	(I1)	= 0 continue to read data = 1 last data card
	2-6	K	(I5)	discretized time
				NOTE: K = 2 to II if Y2(I,J) = 0 for all J K = 1 to II - 1 if Y1(I,J) = 0 for all J K = 2 to II-1 if Y1(I,J) \neq 0 and Y2(I,J) \neq 0 for some J
	7-11	blank		
	12-23	YU(K,I)	(F12.6)	
	24-80	blank		repeat 22-1BU-2, etc.
(Use the following if MSP(I,1) = 0, MSP(1,2) = 2)				
22-1CL	1	blank		
	2	NCN	(I1)	= 0 constant lower bound (GO TO 22-1CL-A) = 1 piecewise constant lower bound (GO TO 22-1CL-1)
	3-80	blank		
22-1CL-A	1-12	SVA2	(F12.6)	starting value
	13-17	NIC2	(I5)	number of increments (use 0 if there are no increments)
	18-29	VIC2	(F12.6)	value of increment
	30-80	blank		
22-1CL-1	1	KEY	(I1)	= 0 continue to read data = 1 last data card
	2-6	K	(I5)	discretized time
				NOTE: K = 2 to II if Y2(I,J) = 0 for all J

<u>Card No.</u>	<u>Columns</u>	<u>Variable Format</u>	<u>Comments</u>
			$K = 1$ to $II-1$ if $Y1(I,J) = 0$ for all J $K = 2$ to $II-1$ if $Y1(I,J) \neq 0$ and $Y2(I,J) \neq 0$ for some J
	7-11	blank	
	12-23	YL(K,I) (F12.6)	
	24-80	blank	repeat 22-1CL-2, etc.
(Use the following if $MSP(I,1) = 0$, $MSP(I,2) = 3$)			
22-IDU	1	blank	
	2	NCN (I,1)	$= 0$ constant right hand side value (GO TO 22-1DU-A) $= 1$ piecewise constant right hand side value (GO TO 22-1DU-1)
	3-80	blank	
22-1DU-A	1-12	SVA1 (F12.6)	starting value
	13-17	NIC1 (I5)	number of movements (use 0 if there are no increments)
	18-29	VIC1 (F12.6)	value of increment
	30-80	blank	
22-1DU-1	1	KEY (I1)	$= 0$ continue to read data $= 1$ last data card
	2-6	K (I5)	discretized time
NOTE: $K = 2$ to II if $Y2(I,J) = 0$ for all J $K = 1$ to $II-1$ if $Y1(I,J) = 0$ for all J $K = 2$ to $II-1$ if $Y1(I,J) \neq 0$ and $Y2(I,J) \neq 0$ for some J			

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
	7-11	blank		
	12-23	YU(K,I)	(F12.6)	
	24-80	blank		repeat 22-1DU-2, etc.
(Use the following if MSP(I,1) = 1, MSP(I,2) = 0)				
22-1EU	1	blank		
	2	NCN	(I1)	= 0 constant upper bound (GO TO 22-1EU-A)
	3-80	blank		
22-1EU-A	1-12	SVA1	(F12.6)	starting value
	13-17	NIC1	(I5)	number of increments (use 0 if there are no increments)
	18-29	VIC1	(F12.6)	value of increment
	30-34	K	(I5)	specify the time
	35-80	blank		
22-1EL	1	blank		
	2	NCN	(I1)	= 0 constant lower bound (GO TO 22-1EL-A)
	3-80	blank		
22-1EL-A	1-12	SVA2	(F12.6)	starting value
	13-17	NIC2	(I5)	number of increments (use 0 if there are no increments)
	18-29	VIC2	(F12.6)	value of increment
	30-34	K	(I5)	specify the time
	35-80	blank		
(Use the following if MSP(I,1) = 1, MSP(I,2) = 1)				
22-1FU	1	blank		
	2	NCN	(I1)	= 0 constant upper bound (GO TO 22-1FU-A)
	3-80	blank		
22-1FU-A	1-12	SVA1	(F12.6)	starting value
	13-17	NIC1	(I5)	number of increments (use 0 if there are no increments)
	18-29	VIC1	(F12.6)	value of increment

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
	30-34	K(I)	(I5)	specify the time
	35-80	blank		
(Use the following if MSP(I,1) = 1, MSP(I,2) = 2)				
22-1GL	1	blank		
	2	NCN	(I1)	= 0 constant lower bound (GO TO 22-1GL-A)
	3-80	blank		
22-1GL-A	1-12	SVA2	(F12.6)	starting value
	13-17	NIC2	(I5)	number of increments (use 0 if there are no increments)
	18-29	VIC2	(F12.6)	value of increment
	30-34	K	(I5)	specify the time
	35-80	blank		
(Use the following if MSP(I,L) = 1, MSP(I,2) = 3)				
22-1HU	1	blank		
	2	NCN	(I1)	= 0 constant right-hand side (GO TO 22-1HU-A)
	3-80	blank		
22-1HU-A	1-12	SVA1	(F12.6)	starting value
	13-17	NIC1	(I5)	number of increments (use 0 if there are no increments)
	18-29	VIC1	(F12.6)	value of increment
	30-34	K	(I5)	
	35-80	blank		
----- OUTPUT (<u>Q1</u> \bar{s} + <u>Q2</u> \bar{u} + <u>Q3</u> \bar{f}_k) -----				
23	1-9	<u>Q1 MATRIX**</u>		
	10-80	blank		

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
23-1	1	KEY	(I1)	= 0 continue to read data = 1 last data card
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	Q1(I,J)		value of Q1(I,J)
	24-80	blank		repeat until all non-zero elements of <u>Q1</u> are input
24	1-9	<u>Q2 MATRIX**</u>		
	10-80	blank		
24-1	1	KEY	(I1)	= 0 continue to read data = 1 last data card
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	Q2(I,J) (F12.6)		value of Q2(I,J)
	24-80	blank		repeat until all non-zero elements of <u>Q2</u> are input
25	1-9	<u>Q3 MATRIX**</u>		
	10-80	blank		
25-1	1	KEY	(I1)	= 0 continue to read data = 1 last data card
	2-6	I	(I5)	
	7-11	J	(I5)	
	12-23	Q3(I,J) (F12.6)		value of Q3(I,J)
	24-80	blank		repeat until all non-zero elements of <u>Q3</u> are input
26	1-10	<u>TRAJECTORY**</u>		
	11-80	blank		

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
26-1	1	KEY	(I1)	= 0 continue to read data e.g. 26-2 = 1 last data card
	2-6	I	(I5)	the i th output
	7-10	blank		
11		ITR	(I1)	= 0 no plot wanted = 1 want to plot i th output
	12-80	blank		 repeat until all needed trajectories are specified
27	1-17	<u>TRADE OFF DIAGRAM**</u>		
	18-80	blank		
27-1	1-4	blank		
	5	ITD	(I1)	= 0 no plot wanted = 1 want tradeoff diagram
	6-9	blank		
	10	KSWT	(I1)	= 0 the ordinate of tradeoff curve starts from 0 = 1 the ordinate of tradeoff curve starts from the minimum value of objective function
	11-80	blank		
----- VERIFICATION OF INPUT AND CALCULATED DATA -----				
28	1-6	<u>VERIFY**</u>		
	7-80	blank		
28 - 1	1-4	blank		
	5	INP	(I1)	= 0 does not print input data = 1 print out input data

<u>Card No.</u>	<u>Columns</u>	<u>Variable</u>	<u>Format</u>	<u>Comments</u>
	6-9	blank		
	10	INT	(I1) = 0	does not print data calculated by PREPROC
			= 1	print data calculated by PREPROC
	11-80	blank		
		----- FINISH INPUT DATA -----		
29	1-17	<u>FINISH INPUT DATA*</u>		
	18-80	blank		
		----- MODIFICATION -----		
30	1-14	<u>MODIFY PROBLEM**</u>		
	15-80	blank		Put the modified data between cards 30 and 31. The user can modify all but the data in the first three cards. The format of the modified data are the same as described before.
31	1-18	<u>FINISH MODIFY DATA**</u>		
	19-80	blank		
		----- RESTARTING A NEW PROBLEM -----		
32	1-7	<u>RESTART**</u>		
	8-80	blank		Put data from card 1 through card 31 after this card. This permits the user to run two or more different problems at a time.
		----- END OF THE PROBLEM -----		
33	1-4	<u>STOP*</u>		
	5-80	blank		Use this card when there is no more data to be read

APPENDIX II

LINEAR PROGRAMMING FORMULATION OF THE LIMITING PERFORMANCE PROBLEM

In this appendix the limiting performance problem is formulated as a linear programming (LP) problem. We consider dynamical systems in which those portions for which the performance is to be measured are represented by time dependent control forces. Although the control forces can replace non-linear system segments, the remaining portions of the system must be linear. In addition, the kinematics of the whole system must be linear. Although the engineer frequently describes a dynamical system with second order differential equations, it is more convenient for us to work with first order equations. Hence, Section A of this appendix considers the conversion from second to first order equations.

The unknown control forces are discretized in time. Integration of the equations of motion for known disturbances yields the response (state) variables as linear combinations of the control forces. The objective functions and constraints comprising the limiting performance problem are formed from these response variables and hence are also linear functions of the discretized control forces. The limiting performance problem then can be formulated as a linear programming problem. Section B of this appendix treats the integration of the first order equations of motion containing the unknown control forces. Finally, we formulate the limiting performance problem as a linear programming problem in Section C.

A. Conversion of Equations of Motion of a Dynamic System to a System of First Order Equations

Consider the general equations of motion of a multi-degree-of-freedom system in the form

$$\underline{\ddot{q}} + \underline{C}\dot{\underline{q}} + \underline{K}\underline{q} + \underline{U}\underline{\bar{u}} = \underline{F}\underline{\bar{f}} \quad (\text{II-1})$$

where

\underline{q} = displacement vector (n x 1)

$\underline{\bar{u}}$ = control force vector (nu x 1)

$\underline{\bar{f}}$ = forcing function vector (nf x 1)

\underline{M} = mass matrix (n x n)

\underline{C} = damping matrix (n x n)

\underline{K} = stiffness matrix (n x n)

\underline{U} = matrix of constants associated with control forces
(n x nu)

\underline{F} = matrix of constants associated with external disturbances
(n x nf)

Letters with bars over them refer to vectors, e.g.,

$$\underline{\bar{q}} = \begin{bmatrix} q_1 \\ q_2 \\ \vdots \\ q_n \end{bmatrix} \text{ is the displacement vector,}$$

while letters with bars under them refer to matrices, e.g.,

$$\underline{C} = \begin{bmatrix} c_{11} & c_{12} & \dots & c_{1n} \\ c_{21} & c_{22} & \dots & c_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ c_{n1} & \dots & \dots & c_{nn} \end{bmatrix} \text{ is the damping coefficient matrix.}$$

These equations can be converted by the following procedure into a system of first order equations.

$$\text{Let } \bar{s} = \begin{bmatrix} \dot{q} \\ q \end{bmatrix}$$

where \bar{s} is a partitioned vector. Also define

$$\underline{W} = \begin{bmatrix} \underline{O} & \underline{M} \\ \underline{M} & \underline{C} \end{bmatrix}_{2n \times 2n}$$

$$\underline{X} = \begin{bmatrix} \underline{M} & \underline{O} \\ \underline{O} & \underline{K} \end{bmatrix}_{2n \times 2n}$$

$$\underline{Y} = \begin{bmatrix} \underline{O} \\ \underline{U} \end{bmatrix}_{2n \times n_u}$$

$$\underline{Z} = \begin{bmatrix} \underline{O}_2 \\ \underline{F} \end{bmatrix}_{2n \times n_f}$$

Then the system of second order equations can be written as

$$\underline{W} \dot{\bar{s}} + \underline{X} \bar{s} + \underline{Y} \bar{u} = \underline{Z} \bar{f} \quad (\text{II-2})$$

$$\text{or } \dot{\bar{s}} = \underline{A} \bar{s} + \underline{B} \bar{u} + \underline{D} \bar{f}$$

where

$$\underline{A} = \underline{W}^{-1} \underline{X} = \begin{bmatrix} \underline{M}^{-1} \underline{C} & \underline{M}^{-1} \underline{K} \\ \underline{I} & \underline{O} \end{bmatrix}_{2n \times 2n}$$

$$\underline{B} = -\underline{W}^{-1} \underline{Y} = \begin{bmatrix} \underline{M}^{-1} \underline{U} \\ \underline{O}_1 \end{bmatrix}_{2n \times n_u}$$

$$\underline{D} = \underline{W}^{-1} \underline{Z} = \begin{bmatrix} \underline{M}^{-1} \underline{F} \\ \underline{O}_2 \end{bmatrix}_{2n \times n_f}$$

\underline{O} , \underline{O}_1 and \underline{O}_2 are null matrices of order $n \times n$, $n \times n_u$ and $n \times n_f$ respectively.

\underline{I} is an $n \times n$ identity matrix. Here we have been made use of

$$\underline{W}^{-1} = \left[\begin{array}{c|c} -\underline{M}^{-1} \underline{C} \underline{M}^{-1} & \underline{M}^{-1} \\ \hline \underline{M}^{-1} & \underline{O} \end{array} \right]_{2n \times 2n}$$

Note that \underline{A} , \underline{B} , \underline{D} , \underline{W} and \underline{W}^{-1} are partitioned matrices.

B. Integration of a System of First Order Equations

We wish to integrate the system of first order equations

$$\dot{\underline{s}} = \underline{A}\underline{s} + \underline{B}\underline{u} + \underline{D}\underline{f} \quad (\text{II-3})$$

with initial conditions

$$\underline{s}|_{t=0} = \underline{s}(0) = \begin{bmatrix} \dot{\underline{q}}(0) \\ -\underline{q}(0) \end{bmatrix}$$

The vectors \underline{s} , \underline{u} , \underline{f} , and matrices \underline{A} , \underline{B} , \underline{D} are defined in the previous appendix.

To solve Eqs (II-3) let

$$\underline{s}(t) = e^{\underline{A}t} \underline{z}(t) \quad (\text{II-4})$$

Substitute Eq. (II-4) into Eqs. (II-3) to find

$$\underline{A}e^{\underline{A}t} \underline{z} + e^{\underline{A}t} \frac{d\underline{z}}{dt} = \underline{A}e^{\underline{A}t} \underline{z} + \underline{B}\underline{u} + \underline{D}\underline{f} \quad (\text{II-5})$$

If we subtract $\underline{A}e^{\underline{A}t}\underline{z}$ from both sides of Eq (II-5) and then premultiply both sides by $e^{-\underline{A}t}$ we obtain

$$\frac{d\underline{z}}{dt} = e^{-\underline{A}t} [\underline{B}\underline{u} + \underline{D}\underline{f}]$$

and $\bar{z}(0) = \bar{s}(0)$, since $\bar{s}(0) = e^{\underline{A}(0)} \bar{z}(0) = \underline{I} \bar{z}(0) = \bar{z}(0)$.

Then,

$$\bar{z}(t) = \bar{s}(0) + \int_0^t e^{-\underline{A}y} [\underline{B}\bar{u}(y) + \underline{D}\bar{f}(y)] dy \quad (\text{II-6})$$

We see from Eqs. (II-4) and (II-6) that the solution of the system (II-3) can be written as

$$\bar{s}(t) = e^{\underline{A}t} [\bar{s}(0) + \int_0^t e^{-\underline{A}y} [\underline{B}\bar{u}(y) + \underline{D}\bar{f}(y)] dy] \quad (\text{II-7})$$

where y is a dummy variable for integration.

To complete the integration in Eq. (II-7) we must know $\bar{u}(t)$ and $\bar{f}(t)$. The loading functions $\bar{f}(t)$ are prescribed. The forces $\bar{u}(t)$ are unknowns to be found as solutions of an optimization problem. We discretize $\bar{u}(t)$ so that between two discretized times \bar{u} is represented by constants. This will permit Eq. (II-7) to be integrated. For convenience, $\bar{f}(t)$ is discretized in the same fashion as $\bar{u}(t)$.

Piecewise Constant Discretization

Assume \bar{u} is discretized as a piecewise constant function of time as shown in Fig. II-1. Here, between $t = iT$ and $t = (i+1)T$, $\bar{u}(t) = \bar{u}(iT)$, where T is the time increment Δt .

Then, at any time kT

$$\begin{aligned} \bar{s}(kT) &= e^{\underline{A}kT} [\bar{s}(0) + \int_0^{kT} e^{-\underline{A}y} [\underline{B}\bar{u}(y) + \underline{D}\bar{f}(y)] dy] \\ &= e^{\underline{A}kT} \bar{s}(0) + e^{\underline{A}kT} \sum_{i=0}^{k-1} \int_{iT}^{(i+1)T} e^{-\underline{A}y} [\underline{B}\bar{u}(y) + \underline{D}\bar{f}(y)] dy \end{aligned}$$

Now,

$$\begin{aligned} &\int_{iT}^{(i+1)T} e^{-\underline{A}y} [\underline{B}\bar{u}(y) + \underline{D}\bar{f}(y)] dy \\ &= \int_{iT}^{(i+1)T} e^{-\underline{A}y} [\underline{B}\bar{u}(iT) + \underline{D}\bar{f}(iT)] dy \\ &= e^{-\underline{A}(i+1)T} \underline{A}^{-1} [e^{\underline{A}T} - \underline{I}] [\underline{B}\bar{u}(iT) + \underline{D}\bar{f}(iT)] \end{aligned}$$

Thus,

$$\begin{aligned} \bar{s}(kT) &= e^{\underline{A}kT} \bar{s}(0) \\ &+ \sum_{i=0}^{k-1} e^{\underline{A}(k-i-1)T} \underline{A}^{-1} (e^{\underline{A}T} - \underline{I}) [\underline{B}\bar{u}(iT) + \underline{D}\bar{f}(iT)] \quad (\text{II-8}) \end{aligned}$$

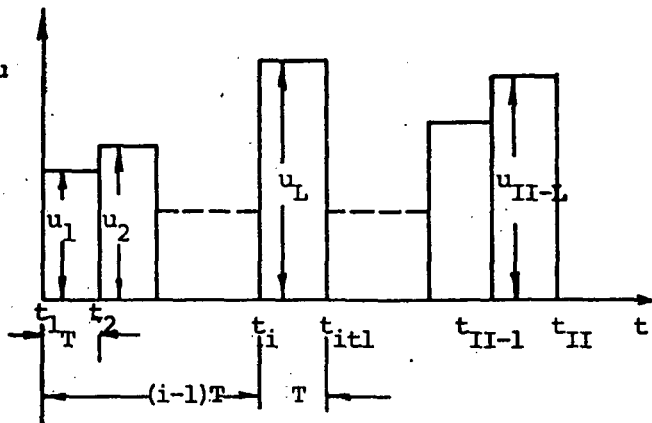


Fig. II-1 Piecewise Constant Discretization of u (u is any Control Force Function).

is the required discrete formal integration of Eq. (II-3), for a piecewise constant representation of $\bar{u}(t)$. Note, here

$$\begin{aligned}\underline{A}^{-1}(\underline{e}^{\underline{A}T} - \underline{I}) &= \underline{A}^{-1}(\underline{I} + \underline{A}T + \frac{\underline{A}^2T^2}{2!} + \frac{\underline{A}^3T^3}{3!} + \dots - \underline{I}) \\ &= \underline{I}T + \frac{\underline{A}T^2}{2!} + \frac{\underline{A}^2T^3}{3!} + \frac{\underline{A}^3T^4}{4!} + \dots \quad (\text{II-9})\end{aligned}$$

Even if \underline{A} is singular, the solution, i.e., Eq. (II-8), is still valid since the series on the right-hand side of Eq. (II-9) always exists.

C. Formulation of the Linear Programming Problem

In this Section the limiting performance problem is formulated as a linear programming (LP) problem, with discretized control forces as unknowns. This is accomplished using the objective functions and constraints in the form described in Appendix I together with the solution of the equations of motion given in Section B of this Appendix.

The solution of the first order equations of motion are given in Section B for the piecewise constant discretization of the control forces as:

$$\bar{s}(kT) = \underline{e}^{\underline{A}kT}\bar{s}(0) + \sum_{i=0}^{k-1} \underline{e}^{\underline{A}(k-i-1)T} \underline{A}^{-1}(\underline{e}^{\underline{A}T} - \underline{I}) [\underline{B} \bar{u}(iT) + \underline{D} \bar{f}(iT)] \quad (\text{II-10})$$

In order to be compatible with indices in FORTRAN, let $\bar{s}(1)$ be the initial condition $\bar{s}(0)$. We rewrite equation (II-10) as:

$$\bar{s}(k) = (\underline{e}^{\underline{A}T})^{k-1} \bar{s}(1) + \sum_{i=1}^{k-1} (\underline{e}^{\underline{A}T})^{k-1-i} \underline{A}^{-1}(\underline{e}^{\underline{A}T} - \underline{I}) [\underline{B} \bar{u}(i) + \underline{D} \bar{f}(i)] \quad (\text{II-11})$$

where $\bar{s}(1) = \bar{s}(0)$

$$\bar{s}(k) = \bar{s}((k-1)T)$$

Now, define the following matrices:

$$\underline{P} = e^{\underline{A}T}$$

$$\underline{AEI} = \underline{A}^{-1} (e^{\underline{A}T} - \underline{I}) \quad (\text{II-12})$$

$$\underline{R}(n) = \underline{P}^{n-1} \underline{AEI} \underline{B}$$

$$\underline{T}(n) = \underline{P}^{n-1} \underline{AEI} \underline{D}$$

Note that $\underline{R}(1) = \underline{AEI} \underline{B}$, $\underline{T}(1) = \underline{AEI} \underline{D}$

Here $\underline{R}(i)$ and $\underline{T}(i)$ ($i = 1, 2, \dots, n$) are matrices of order $m \times n_u$, $m \times n_f$, respectively, where m = number of first order equations to be integrated and n is the number of discretized time intervals. In terms of those new matrices Eq. (II-11) becomes

$$\bar{s}(k) = \underline{P}^{k-1} \bar{s}(1) + \sum_{i=1}^{k-1} [\underline{R}(k-i) \bar{u}(i) + \underline{T}(k-i) \bar{f}(i)] \quad (\text{II-13})$$

Now, define

$$\underline{RG}(k) = [\underline{R}(k-1) : \underline{R}(k-2) : \dots : \underline{R}(1)]$$

$$\underline{TG}(k) = [\underline{T}(k-1) : \underline{T}(k-2) : \dots : \underline{T}(1)]$$

$$\bar{f}(k) = \begin{bmatrix} \bar{f}(1) \\ \bar{f}(2) \\ \vdots \\ \bar{f}(k-1) \end{bmatrix} \quad (\text{II-14})$$

$$\bar{u}(k) = \begin{bmatrix} \bar{u}(1) \\ \vdots \\ \bar{u}(2) \\ \vdots \\ \bar{u}(k-1) \end{bmatrix}$$

Using Eqs. (II-14), Eq. (II-13) becomes

$$\bar{s}(k) = \underline{P}^{k-1} \bar{s}(1) + \underline{RG}(k) \bar{u}(k) + \underline{TG}(k) \bar{f}(k) \quad (\text{II-15})$$

Let

$$\bar{C}(k) = \bar{C1}(k) + \bar{C2}(k) \quad (II-16)$$

$$\text{where } \bar{C1}(k) = p^{k-1} \bar{s}(1) \quad (II-17)$$

$$\bar{C2}(k) = \underline{TG}(k) \bar{f}(k)$$

We can simplify Eq. (II-15) to

$$\bar{s}(k) = \bar{C}(k) + \underline{RG}(k) \bar{u}(k) \quad (II-18)$$

For a system subject to several sets of forcing functions, Eq. (II-18) becomes

$$\bar{s}(s,k) = \bar{C}(s,k) + \underline{RG}(k) \bar{u}(k) \quad (II-19)$$

where

$$\bar{C}(s,k) = \bar{C1}(k) + \bar{C2}(s,k)$$

$\bar{C1}(k)$ is given in Eq (II-17)

$$\bar{C2}(s,k) = \underline{TG}(k) \bar{f}(s,k)$$

$$\bar{f}(s,k) = \begin{bmatrix} \bar{f}(s,1) \\ \vdots \\ \bar{f}(s,2) \\ \vdots \\ \bar{f}(s,k-1) \end{bmatrix}$$

Eq. (II-19) expresses the state variable vector \bar{s} as a linear function of the control forces, initial conditions, and forcing functions. Here the initial conditions and forcing functions are prescribed, the only unknowns are the control forces (u).

Since the objective functions and constraints are all formed as linear combinations of \bar{s} , \bar{u} , \bar{f} , they are all linear functions of the u 's. Then the problem of finding the u 's that minimize the maximum or maximize the minimum value of the objective functions subject to constraints becomes a problem in linear programming. We will now define the limiting performance

problem in terms of the LP problem and explain how to set up the data in the proper form.

The LP problem is to find \bar{z} such that $\bar{c} \bar{z}$ is minimized (or maximized) subject to $\underline{H}\bar{z} \leq \bar{G}$ (II-20)

Where $\bar{c} = (1, 0, 0, \dots, 0)$ is a row vector

$$\bar{z} = \begin{bmatrix} \phi \\ \bar{u} \text{ (II)} \end{bmatrix} \quad \text{(II-21)}$$

$$\text{with } \bar{u} \text{ (II)} = \begin{bmatrix} \bar{u}(1) \\ \bar{u}(2) \\ \vdots \\ \bar{u}(\text{II}-1) \end{bmatrix}$$

\underline{H} and \bar{G} are a matrix and a vector constructed from the objective functions and constraints, respectively.

The objective function is formed as

$$\bar{\psi} = \underline{PX1}\bar{s} + \underline{PX2}\bar{u} + \underline{PX3}\bar{f}(s) \quad \text{(II-22)}$$

where the index s designates the s^{th} set of forcing functions are being used. There are two cases of interest: minimizing the maximum value of $\bar{\psi}$ or maximizing the minimum value. The minimization of the maximum value of $\bar{\psi}$ is equivalent to finding the minimum of ϕ such that

$$|\psi_i| \leq \phi \text{ for all } i = 1 \text{ to NOB}$$

$$\text{or } -\phi + \psi_i \leq 0 \quad \text{(II-23)}$$

$$\phi + \psi_i \geq 0 \quad \text{(II-24)}$$

where ψ_i is the i^{th} row of $\bar{\psi}$

Using Eqs. (II-19), (II-22), Eqs. (II-23), (II-24) become

$$-\phi + \underline{PX1}_i \underline{RG}(k) \bar{u}(k) + \underline{PX2}_i \bar{u}(k) \leq -\underline{PX1}_i \bar{C}(s,k) - \underline{PX3}_i \bar{f}(s,k) \quad \text{(II-25)}$$

$$\phi + \underline{PX1}_i \underline{RG}(k) \bar{u}(k) + \underline{PX2}_i \bar{u}(k) \geq -\underline{PX1}_i \bar{C}(s,k) - \underline{PX3}_i \bar{f}(s,k) \quad \text{(II-26)}$$

Eqs. (II-25), (II-26) are valid for $k = I1, I1 + 1, \dots L$

$$s = 1, 2, \dots NSETS$$

where $PX1_i, PX2_i, PX3_i$ are the i^{th} rows of the matrices $PX1, PX2, PX3$ respectively. The values of $I1$ and L depend on whether $PX1_i$ or $PX2_i$ are zero. If $PX1_i = (0 \ 0 \ \dots \ 0)$ then $I1 = 1, L = II-1$. If $PX2_i = (0 \ 0 \ \dots \ 0)$, then $I1 = 2, L = II$. If $PX1_i \neq (0 \ 0 \ \dots \ 0)$ and $PX2_i \neq (0 \ 0 \ \dots \ 0)$, then $I1 = 2, L = II-1$. The contribution to \underline{H} and \underline{G} for a typical objective function (e.g., i^{th} row of $\bar{\Psi}$) can be found from Eqs. (II-25) and (II-26). It is put in matrix form in Table II-1. The total contribution to \underline{H} and \underline{G} from the objective functions is a matrix containing NOB submatrices in the form of Table (II-1), where NOB is the number of objective functions.

To maximize the minimum value of $\bar{\Psi}$ is equivalent to finding the maximum of ϕ such that $|\bar{\Psi}_i| > \phi$. Note that to find maximum ϕ is equivalent to finding minimum $-\phi$. Thus the LP problem for this case is still in the form of Eq. (II-20) except now the row vector \bar{C} is $(-1, 0, 0, \dots 0)$. The formation of arrays \underline{H} and \underline{G} for the objective functions remain the same as above except the inequality signs are reversed.

The constraints are formed as

$$\underline{Y1}\bar{s} + \underline{Y2}\bar{u} + \underline{Y3}\bar{f}(s)$$

The type of i^{th} constraint depends on the value of the i^{th} row of the specification matrix, i.e. $MSP(i,1)$ and $MSP(i,2)$. The specification matrix has been defined in Appendix I. For $MSP(i,1) = 0$, the constraint is applied at all times.

$$1. \quad MSP(i,2) = 0$$

The constraint is

$$\bar{Y}L_i < \underline{Y1}_i \bar{s} + \underline{Y2}_i \bar{u} + \underline{Y3}_i \bar{f}(s) < \bar{Y}U_i \quad (II-27)$$

$$\begin{bmatrix}
 -1 & \underline{D}_{i1} & \underline{E}_i & \underline{0} & \cdot & \cdot & \cdot & \underline{0} \\
 -1 & \underline{D}_{i1} & \underline{D}_{i1} & \underline{E}_i & \underline{0} & \cdot & \cdot & \underline{0} \\
 \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\
 -1 & \underline{D}_i(k-1) & \underline{D}_i(k-2) & \cdot & \cdot & \underline{D}_{i1} & \underline{E}_i & \underline{0} \\
 \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\
 -1 & \underline{D}_i(II-1) & \underline{D}_i(II-2) & \cdot & \cdot & \underline{D}_i(k-1) & \cdot & \underline{D}_{i1}
 \end{bmatrix}
 \begin{bmatrix}
 \underline{0} \\
 \underline{0} \\
 \vdots \\
 \underline{0} \\
 \vdots \\
 \underline{E}_i
 \end{bmatrix}
 \begin{bmatrix}
 \phi \\
 \underline{u}(1) \\
 \underline{u}(2) \\
 \vdots \\
 \underline{u}(k-1) \\
 \vdots \\
 \underline{u}(II-1)
 \end{bmatrix}
 \begin{bmatrix}
 < \\
 < \\
 < \\
 <
 \end{bmatrix}
 \begin{bmatrix}
 B_1 \dots \\
 B_2 \dots \\
 \vdots \\
 B_k \dots \\
 \dots \\
 \vdots \\
 B_{II-1}
 \end{bmatrix}$$

$$\begin{bmatrix}
 1 & \underline{D}_{i1} & \underline{E}_i & \underline{0} & \cdot & \cdot & \cdot & \underline{0} \\
 1 & \underline{D}_{i2} & \underline{D}_{i1} & \underline{E}_i & \underline{0} & \cdot & \cdot & \underline{0} \\
 \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\
 1 & \underline{D}_i(k-1) & \underline{D}_i(k-2) & \cdot & \cdot & \underline{D}_{i1} & \underline{E}_i & \underline{0} \\
 \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\
 1 & \underline{D}_i(II-1) & \underline{D}_i(II-2) & \cdot & \cdot & \underline{D}_i(k-1) & \cdot & \underline{D}_{i1}
 \end{bmatrix}
 \begin{bmatrix}
 \underline{0} \\
 \underline{0} \\
 \vdots \\
 \underline{0} \\
 \vdots \\
 \underline{E}_i
 \end{bmatrix}
 \begin{bmatrix}
 \phi \\
 \underline{u}(1) \\
 \underline{u}(2) \\
 \vdots \\
 \underline{u}(k-1) \\
 \vdots \\
 \underline{u}(II-1)
 \end{bmatrix}
 \begin{bmatrix}
 > \\
 > \\
 > \\
 >
 \end{bmatrix}
 \begin{bmatrix}
 B_1 \dots \\
 B_2 \dots \\
 \vdots \\
 B_k \dots \\
 \dots \\
 \vdots \\
 B_{II-1}
 \end{bmatrix}$$

where

$$\underline{D}_{ij} = \underline{PX1}_i \underline{R}(j)$$

$$\underline{E}_i = \underline{PX2}_i$$

$$B_k = -\underline{PX1}_i \underline{C}(s, k+1) - \underline{PX3}_i \underline{f}(s, k+1)$$

TABLE II-1

Using Eq. (II-19), Eq. (II-27) can be written as

$$\underline{Y1}_i \underline{RG}(k) \bar{u}(k) + \underline{Y2}_i \bar{u}(k) \leq \bar{YU}_i(k) - \underline{Y1}_i \bar{C}(s,k) - \underline{Y3}_i \bar{f}(s,k) \quad (\text{II-28})$$

$$\underline{Y1}_i \underline{RG}(k) \bar{u}(k) + \underline{Y2}_i \bar{u}(k) \geq \bar{YL}_i(k) - \underline{Y1}_i \bar{C}(s,k) - \underline{Y3}_i \bar{f}(s,k) \\ \text{for } K = \text{II to } L \quad (\text{II-29})$$

The contribution to \underline{H} and \bar{G} of Eqs. (II-28), (II-29) are summarized in Table II-2A, and Table II-2B, respectively. The value of II and L depends on whether $\underline{Y1}_i$ or $\underline{Y2}_i$ is zero. If $\underline{Y1}_i = (0 \ 0 \ \dots \ 0)$, then $\text{II} = 1$, $L = \text{II}-1$. If $\underline{Y2}_i = (0 \ 0 \ \dots \ 0)$, then $\text{II} = 2$, $L = \text{II}$. If $\underline{Y1}_i \neq (0 \ 0 \ \dots \ 0)$ and $\underline{Y2}_i \neq (0 \ 0 \ \dots \ 0)$, then $\text{II} = 2$, $L = \text{II}-1$.

2. $\text{MSP}(i,2) = 1$

The i^{th} constraint is

$$\underline{Y1}_i \bar{s} + \underline{Y2}_i \bar{u} + \underline{Y3}_i \bar{f}(s) \leq \bar{YU}_i \quad (\text{II-30})$$

The contribution to \underline{H} and \bar{G} is the same as Eq. (II-28).

3. $\text{MSP}(i,2) = 2$

Here the constraint is expressed as

$$\underline{Y1}_i \bar{s} + \underline{Y2}_i \bar{u} + \underline{Y3}_i \bar{f}(s) \geq \bar{YL}_i \quad (\text{II-31})$$

The contribution to \underline{H} and \bar{G} is the same as Eq. (II-29).

4. $\text{MSP}(i,2) = 3$

In this case the constraint is given by

$$\underline{Y1}_i \bar{s} + \underline{Y2}_i \bar{u} + \underline{Y3}_i \bar{f}(s) = \bar{YU}_i \quad (\text{II-32})$$

The contribution to \underline{H} and \bar{G} is the same as Eq. (II-28), except now the inequality becomes an equality. For $\text{MSP}(i,1) = 1$, the constraint is applied at a specified time only. The formal contribution to \underline{H} and \bar{G} for all cases is the same as for $\text{MSP}(i,1) = 0$, except k is now restricted to a specific time, i.e., $\text{KS}(i)$.

0	$\underline{D_{i1}}$	$\underline{E_i}$	$\underline{0}$	$\underline{0}$	$\underline{\phi \dots}$	$\underline{B_1 \dots}$
0	$\underline{D_{i2}}$	$\underline{D_{i1}}$	$\underline{0}$	$\underline{0}$	$\underline{\bar{u}(i)}$	$\underline{B_2 \dots}$
\vdots	\vdots	\vdots	\vdots	\vdots	\vdots	\vdots
0	$\underline{D_{i(k-1)}}$	$\underline{D_{i(k-2)}}$	$\underline{D_{i1}}$	$\underline{E_i}$	$\underline{\vdots}$	$\underline{B_k \dots}$
\vdots	\vdots	\vdots	\vdots	\vdots	$\underline{\bar{u}(k-1)}$	\vdots
0	$\underline{D_{i(II-1)}}$	$\underline{D_{i(II-2)}}$	$\underline{D_{i(k-1)}}$	$\underline{D_{i1}}$	$\underline{\bar{u}(II-1)}$	$\underline{B_{iI-1}}$

where $\underline{D_{ij}} = \underline{Y1_i R(j)}$

$\underline{E_i} = \underline{Y2_i}$

$\underline{B_k} = \underline{\bar{Y}L_i(k+1)} - \underline{Y1_i \bar{C}(s,k+1)} - \underline{Y3_i \bar{f}(s,k+1)}$

TABLE II-2B

D. Dimension of the Linear Programming Problem

The dimension of the linear programming problem depends on the number of controllers of the system, the number and nature of objective functions and constraints, the number of time intervals, and the number of sets of forcing functions. It is independent of the number of degrees of freedom of the system. The dimensions of the matrix \underline{H} and vector \bar{G} can be calculated as following:

$$R_H = [(II-1) \times (2N_1 + 2C_1 + C_3) + (II-2) \times (2N_2 + 2C_2 + C_4) + 2C_5 + C_6] \times \text{NSETS}$$

$$C_H = 1 + Nu \times (II-1)$$

$$R_G = R_H$$

where

R_H = Number of rows of matrix \underline{H}

C_H = Number of columns of matrix \underline{H}

R_G = Number of rows of vector \bar{G}

N_1 = Number of objective functions for which $\underline{PX1}_i = 0$ or $\underline{PX2}_i = 0$,

N_2 = Number of objective functions for which $\underline{PX1}_i \neq 0$ and $\underline{PX2}_i \neq 0$

C_1 = Number of constraints for which

$MSP(I,1) = 0, MSP(I,2) = 0$ and $\underline{Y1}_i = 0$ or $\underline{Y2}_i = 0$

C_2 = Number of constraints for which
 $MSP(I,1) = 0, MSP(I,2) = 0$ and $\underline{Y1}_i \neq 0$ and $\underline{Y2}_i \neq 0$

C_3 = Number of constraints for which
 $MSP(I,1) = 0, MSP(I,2) \neq 0$ and $\underline{Y2}_i = 0$ or $\underline{Y1}_i = 0$

C_4 = Number of constraints for which
 $MSP(I,1) = 0, MSP(I,2) \neq 0$ and $\underline{Y1}_i \neq 0$ and $\underline{Y2}_i \neq 0$

C_5 = Number of constraints with $MSP(I,1) = 1, MSP(I,2) = 0$

C_6 = Number of constraints with $MSP(I,1) = 1, MSP(I,2) \neq 0$

II = Number of time intervals used (see Appendix I)

NSETS = Number of sets of forcing functions

As an example, consider the dimensions of the linear programming problem for the SDF problem shown on page 17. Here II=10, $N_2 = 1$,
 $C_1 = 1$, NSETS = 1, Nu = 1

$$R_H = [(10-1) \times (2 \times 1 + 2 \times 1)] \times 1 = 36$$

$$C_H = 1 + 1 \times (10-1) = 10.$$

APPENDIX III

PROGRAMMING DESCRIPTION OF THE COMPONENTS OF PERFORM

This appendix contains descriptions of the three major components of PERFORM: PREPROC, MPS/360, PSTPROC.

A. PREPROC

This section includes a description of program PREPROC. Appendix IV A contains a listing of program PREPROC.

Table III-1 contains a listing of the arrays used in the program with explanatory notes.

The variables beginning with an IVE card followed by a number are used to communicate to the printing routine those arrays which contain nonzero elements or special conditions. Table III-2 relates IVE numbers to program arrays.

1. Main Section

The main section of the program is described in the PREPROC section of Section III of this report.

2. Subroutines (Alphabetical Order)

a. BODATA

This subroutine punches the BOUNDS action of the MPS/360 linear programming problem. The default bounds for MPS/360 variables are zero lower and unlimited upper; because solutions to limiting performance problems can be negative, the default overriding BOUNDS section is necessary.

b. BRIDGE

This subroutine calculates the arrays R , T , \overline{CI} , $\overline{C2}$, and \overline{C} as described in Appendix II. It is called from the main section.

<u>Array Identifiers</u>	<u>Dimension</u>	<u>Notes</u>	<u>Common Block</u>
A	m* x m	First order system A is input. Second order A computed by subroutine COVERT	ABD
B	m* x nu	First order B is input. Second order computed by subroutine COVERT	ABD
CAY	n x n	Matrix K in model	EKC
CC	n x n	Matrix C in model	EKC
CM	n x n	Becomes $\underline{M}^{-1}\underline{C}$ in subroutine COVERT.	INV
CYM	n x n	Becomes $\underline{M}^{-1}\underline{K}$ in subroutine COVERT.	INV
D	m* x nf	First order <u>D</u> is input. Second order computed by COVERT.	ABD
EM	n x n	Matrix M in model	EKC
EMI	n x n	Becomes \underline{M}^{-1} in subroutine MIV.	INV
F	nsets x II x nf	Subscript 1: forcing function set number, 2: time interval, 3: row of equations of motion with which associated. This is not model matrix <u>F</u> .	FOFUN
FF	n x nf	Matrix <u>F</u> in model.	EKC
FM	n x nf	Becomes $\underline{M}^{-1}\underline{F}$ in subroutine COVERT	EKC
G	number of LP rows (See Dimension of LP problem)	Right-hand side of LP tableau	RHV
H	number of LP rows; number of LP columns (See Dimension of LP problem)	Linear programming tableau.	PVAL

TABLE III-1. PREPROC ARRAYS

<u>Array Identifiers</u>	<u>Dimension</u>	<u>Notes</u>	<u>Common Block</u>
ISSET	not	ISSET(1) identifies forcing function of the set to be used in tabulation row I	TAB
ITITL		Alphanumeric problem title	TIT
ITR	not	ITR(I) is 0 if plot of I th output is not desired. Otherwise plot is made	
IXX	noc	IXX(I) indicates the behavior of the bounds of I th constraint = 0 no varying bounds = 1 \overline{YU} varies = 2 \overline{YL} varies = 3 \overline{YL} and \overline{YU} vary	
KS	noc	KS(I) specifies the specific time for I th constraints	
MSP	noc x 2	Specific type of constraint See Appendix I for description.	ISP
NRE	number of LP rows	Identifies relation of each row with its right-hand side "G" means \geq "L" means \leq "E" means $=$	RHV
PX1	nob x m	* *	OBJ
PX2	nob x nu	* *	OBJ
PX3	nob x nf	* *	OBJ
Q1	not x m	* * *	TAB
Q2	not x nu	* * *	TAB
Q3	not x nf	* * *	TAB
S	2n	Used for initial condition in program	INIT
UM	n x nu	Becomes $M^{-1}U$ in subroutine COVERT	INV
UU	n x n	Matrix U in model	EKC

TABLE III-1. PREPROC Arrays (continued).

<u>Array Identifiers</u>	<u>Dimension</u>	<u>Notes</u>	<u>Common Block</u>
Y	member of varying bounds	Array of varying bounds PSTPROC tradeoff diagram	UPLO
Y1	noc x m	* * * *	CONST
Y2	noc x nu	* * * *	CONST
Y3	noc x nf	* * * *	CONST
YU	II x noc	Upper bound vector. Subscript 1: time interval 2: number of constraints	UPLO
YL	II x noc	Lower bound vector, subscripts have same meaning as above.	UPLO
C	nsets x II x m	Arrays pertinent to the formation of right-hand side of the LP problem. (See Appendix II). Subscript 1: forcing function set 2: time 3: row number in state (response) vector	CCS
P	m x m	Becomes $e^{\underline{A}T}$ in BRIDGE	
C2		Arrays used in form array C.	
C1	II x m	Arrays used to form array C.	
R	II x m x m	Arrays pertinent to expressing responses as function of the control forces.	BRG
T	II x m x nf	Arrays pertinent to expressing responses as functions of forcing functions.	BRG
AEI	m x m	Becomes $-\underline{A}^{-1}(e^{\underline{A}t} - \underline{I})$ in BRIDGE	MYAP

TABLE III-1. PREPROC Arrays (continued)

Symbols used in array table.

nob = Number of objective functions (rows in PX1, PX2, PX3 expression).

noc = Number of constraint expressions.

nsets = Number of sets of forcing functions.

not = Number of tabulation expressions.

nf = Number of forcing functions.

nu = Number of isolators (control forces).

* m = NDF For first order system. m = 2(NDF) for second order system.

** Arrays related to input of objective functions, see Appendix I.

*** Arrays related to input of required output, see Appendix I.

**** Arrays related to input of constraints, see Appendix I.

NDF Number of equations in the system of equations.

TABLE III-1. PREPROC Arrays (concluded)

<u>IVE</u>	<u>Array Read or Command</u>
1	A
2	B
3	C
4	EM
5	CL
6	CAY
7	FF
8	UU
9	S (initial condition)
10	F (forcing function)
11	PX1
12	PX2
13	PX3
14	Y1
15	Y2
16	Y3
17	MSP
18	(Not used)
19	Q1
20	Q2
21	Q3

TABLE III-2. IVE Variable Array Relation

c. CODATA

This section punches the COLUMNS section of the MPS/360 file. The coefficients of the tableau array H are in this section, CODATA is called by LPDATA which is called by the main section.

d. COVERT

This subroutine reduces the equations of a second order system to those of a first order system. It is called from the main section.

e. ELEMTP

ELEMTP is called from the main section to compute the objective function portions of the \underline{H} and \bar{G} arrays.

f. ELEMTQ

The constraint portions of the \underline{H} and \bar{G} arrays are computed by subroutines called by ELEMTQ which is called from the main section. The routines called depend on whether the programming tableau rows are equalities or inequalities and whether $\underline{Y}L$, $\underline{Y}U$, or both are part of problem constraints.

g. ELEMTR

Subroutine ELEMTR computes the appropriate portions of the \underline{H} and \bar{G} array for the problem constraint I which is a passed parameter from ELEMTQ. Table II-2A of Appendix II shows the computation of ELEMTR. As can be noted, this routine computes only the $\underline{Y}U$ array.

h. ELEMTS

This subroutine completes portions of the \underline{H} and \bar{G} arrays dependent on problem constraint I which is a passed parameter of ELEMTQ. Table II-2B of Appendix II shows the computation of ELEMTS. Note that this routine works only with $\underline{Y}L$.

i. ELEMTT

Routine ELEMTT is called when the constraint of passed parameter I is an equality. Note that equalities always involve the $\underline{Y}U$ vector.

j. LPDATA

The subroutine LPDATA punches section header cards for the MPS/360 linear programming problem and calls other subroutines to punch the actual section records. Subroutines RODATA, RHDATA, BODATA, and CODATA are called. LPDATA is called from the main section.

k. M12X3

This subroutine multiplies a two-dimensional array times a portion of a three-dimensional one, both of which are parameters.

l. M22X2

This routine multiplies two passed arrays.

m. MEXAP

This subroutine evaluates the matrices P and AEI used in Section C of Appendix III. These matrix functions are computed using approximate formulas described in Ref. 9. This routine can be replaced by any routine that uses other algorithms to compute matrix exponential functions.

n. MIV

This routine computes the inverse of array EM and stores it in array EMI.

o. POST

Subroutine POST punches the PSTPROC report specifications. It includes arrays Q1, Q2, Q3, Y, R, F, C, ISET and ITC. No subroutines are called by POST.

p. PRNT

After the linear programming problem has been compiled subroutine PRNT is called to print the H, G, and NRE arrays. Array NRE shows the sign (<, =, >) of the linear programming row.

q. RHDATA

Subroutine RHDATA is called by LPDATA to punch the RHS section of the MPS/360 linear programming problem.

r. RODATA

Subroutine RODATA punches the ROWS section of the MPS/360 linear programming problem. The ROWS section associates names with the tableau rows and specifies the relation of each row to its right-hand side, i.e., \leq , $=$, or \geq .

s. SEARCH

This subroutine sets a parameter to 1 if there are nonzero elements in the given row of the passed two-dimensional array. Otherwise a zero is returned.

t. VERFY

If a VERIFY indicator record is encountered and variable INP is not zero, subroutine VERFY is called to print all of the PERFORM problem specification data.

u. VERFY2

If variable INT is nonzero, subroutine VERFY2 is called to print out the intermediate resulting arrays. These include A, B, D, R, AEI.

B. MPS/360

A listing and discussion of the MPS/360 control program is in this section. The material about MPS and its relation to PERFORM in part B of the Section III of this report is useful background information to this appendix.

Consider the listing of the MPS/360 control program. The first two statements, PROGRAM and TITLE, identify the program name and the title to be printed on each page of the solution report.

The first instruction is the macro INITIALZ. Macro instructions direct the compiler to include at the point of appearance a predefined set of source instructions identified by the macro name; macros eliminate the need for tedious programmer coding of repeatedly used sets of instructions. The INITIALZ macros initializes values of certain tolerances, standard frequencies, etc, and specifies actions to be taken should errors occur during execution.

MPS/360 Control Program Listing

//UVAAE001 JOB 605R0,WANG ,MSGLEVEL*1

/*FORMAT PU,DDNAME*SYSPUNCH,DEST*LOCAL

/*MAIN TIME*10,LINES*10

// EXEC LP

//LP.SYSIN DD *

PROGRAM (IPM)

TITLE (UVA EXAMPLES)

INITIALZ

MOVE (XDATA,EXMP1)

MOVE (XPBNAME,ILTMDYN)

CONVERT (ICHECK,ISUMMARY)

BCDOUT (IDNE)

SETUP (IMINI,IROUND,IRDS)

PICTURE

MOVE (XOBJ,OBJF)

MOVE (XRHS,RHS)

PRIMAL

SOLUTION

MOVE (XDATA,ANSWER)

PUNCH (ILIST,IVALUE)

EXIT

PEND

/*

//GO.SYSPRINT DD SYSOUT=A

//GO.SYSIN DD *

(Place MPS/360 Linear Programming Problem Data Deck here)

/*

The next two move instructions set data cells XDATA and XPBNAME. Identifiers beginning with X are predefined special variables for passing information to the procedures. The contents of XDATA, which is set to EXMP1, identifies the name of the data to be used by the following procedures. If the input stream has several named decks one can be picked for use by setting XDATA to the name on the deck NAME card. XPBNAME is the name to be given to the problem file — an internal MPS file, omitted from the system flowchart and designated PROBFIL.

Procedure CONVERT writes on PROBFIL in converted format the data deck named by XDATA. The contents of PBNAME identifies the converted data. Parameters 'CHECK' and 'SUMMARY' specify special checks to be performed and a summary of the data to be printed.

The next procedure, BCDOUT, prints the problem on the PROB file identified by XPBNAME. Parameter 'ONE' specifies one value per printed line.

Certain computations that must be done before the solution is found are done by SETUP; XPBNAME identifies the problem to be set up. Parameter 'MIN' specifies object function minimization; 'BOUND' and 'BDS' identifies BDSI as the vector name of the bounds specifications.

PICTURE causes a picture of the matrix to be printed.

The next two move statements identify vector OBJF to be used as the objective function coefficients and RHS1 the right-hand side vector.

PRIMAL is the optimization procedure. The next procedure SOLUTION produces a printout of the solution obtained by procedure PRIMAL.

The linear programming problem solution card file is produced by procedure PUNCH. Parameter 'LIST' produces a printed listing of the output and 'VALUE' is necessary for values to be punched.

Procedure EXIT is the final statement and returns control to the system from the program. It is equivalent to the FORTRAN CALL EXIT or STOP statements.

PEND, like FORTRAN END, specifies to the compiler the end of the program.

C. PSTPROC

A discussion of the program PSTPROC is given in this section. Appendix IV B contains a listing of program PSTPROC. There are three subroutines in PSTPROC in addition to the main section. Each of these is described below.

1. Main Section

The main section is described in the Section III of this report. Arrays have the same identifiers in both this program and PREPROC.

2. Subroutines

a. SEARCH

Subroutine SEARCH sets a parameter to 1 if a nonzero element is found in a given row of the passed array. If all row elements are zero, a 0 is returned.

b. TRAJ

Subroutine TRAJ plots the tabulation function against time; a tabulated listing is printed in addition to the line printer plot.

The logic of the program is straightforward; the position of the star is determined and computed GO TO statements transfer control to a WRITE-FORMAT pair which prints the star.

c. TRADE

The logic of this subroutine is much like that of TRAJ. It plots the tradeoff between the objective function values and the values of varying bounds.

APPENDIX IV

LISTINGS OF PROGRAMS

A. Program PREPROC

```

PROGRAM PREPROC(INPUT, OUTPUT, TAPE5=INPUT, TAPE6=OUTPUT, PUNCH)
DIMENSION IXX(8)
COMMON /PLT/ ITR(8), ITO, KSWT
COMMON /RHIO/ ISP, MSP(8,2)
COMMON /INIT/ SII(20)
COMMON /XAP/ AII(20,20), P(20,20)
COMMON /ABD/ A(20,20), B(20,4), D(20,4)
COMMON /ORJ/ PX1(5,26), PX2(5,4), PX3(5,4)
COMMON /EKC/ EH(10,10), CC(10,10), FF(10,4), CAY(10,10), UU(10,4)
COMMON /IIST/ ISET(10)
COMMON /CONST/ Y1(5,20), Y2(5,4), Y3(5,4)
COMMON /TAB/ Q1( 3,20), Q2( 3,3), Q3( 3,3)
COMMON /UPLQ/ YU(20,5), YL(20,5), Y(20)
COMMON /FOFUN/ F(1,20,4)
COMMON /TI/ ITIL(12)
COMMON /ALL/ INTR, KS(8)
COMMON /RHS/ NOBF, NOC, NOB, NOT
COMMON /I/  IM
COMMON /INPT/ II, N, M, NF, NU, KI, KJ, NDF, MODE, IZ
COMMON /MT/ NOE
COMMON /FORC/ NSETS
COMMON /VER/ IVE1, IVE2, IVE3, IVE4, IVE5, IVE6, IVE7, IVE8, IVE9, IVE10
COMMON /VER1/ IVE11, IVE12, IVE13, IVE14, IVE15, IVE16, IVE17, IVE19
COMMON /VER2/ IVE20, IVE21, IVE23, IVE24
INM1 = (+6HA MATR) 1 24
INM2 = (+6HB MATR) 1 25
INM3 = (+6HD MATR) 1 26
INM4 = (+6HH MATR) 1 27
INM5 = (+6HC MATR) 1 28
INM6 = (+6HK MATR) 1 29
INM7 = (+6HF MATR) 1 30
INM8 = (+6HU MATR) 1 31
INM9 = (+6HINITIA) 1 32
INM10 = (+6HFORCIN) 1 33
INM11 = (+6HPX1 MA) 1 34
INM12 = (+6HPX2 MA) 1 35
INM13 = (+6HPX3 MA) 1 36
INM14 = (+6HY1 MAT) 1 37
INM15 = (+6HY2 MAT) 1 38
INM16 = (+6HY3 MAT) 1 39
INM17 = (+6HBOUNDS) 1 40
INM18 = (+6HMODIFY) 1 41
INM19 = (+6HQ1 MAT) 1 42
INM20 = (+6HQ2 MAT) 1 43
INM21 = (+6HQ3 MAT) 1 44
INM22 = (+6HTRADE) 1 45
INM23 = (+6HFINISH) 1 46
INM24 = (+6HSTOP) 1 47
INM25 = (+6H*) 1 48
INM26 = (+6HRESTAR) 1 49
INM27 = (+6HVERIFY) 1 50
INM28 = (+6HTRAJEC) 1 51
5 READ (5,10) (NPB, (ITIL(I), I = 1,12))
10 FORMAT (1X,15,4X,12A5)
000071 READ (5,20) NOE, MODE, NDF, NU, NF, NSETS, II, IM, NOB, NOC, ISP, NOT
000125 20 FORMAT (5X,11,4X,11,4X,5I5, F10.6,2I5,4X,11,15)
000125 WRITE (6,22) (NPB, (ITIL(I), I = 1,12))

```

```

000141 22 FORMAT (1H1,4X,16HPROBLEM NUMBER =,15,5X,12A5)
000141 23 IF (NOE-1)23,23,28
000144 M=N
000146 GO TO 26
000147 28 N=NDF*2
000147 M=N
000151 26 DO 2112 I=1,N
000152 S(I,I) = 0.0
000154 Y(I) = 0.0
000156 DO 2111 J=1,N
000157 A(I,J) = 0.0
000160 ACI(I,J)=0.0
000163 P(I,J)=0.0
000166 2111 CONTINUE
000171 DO 2119 J=1,4
000173 R(I,J) = 0.0
000175 D(I,J) = 0.0
000200 2119 CONTINUE
000203 DO 2112 J=1,5
000205 YU(I,J)=0.0
000206 YL(I,J)=0.0
000211 2112 CONTINUE
000214 DO 2116 I=1,NOC
000220 ISET(I) = 0
000222 2116 CONTINUE
000223 DO 2117 I=1,8
000225 IXX(I) = 0
000227 IIR(I) = 0
000230 MSP(I,1) = 0
000231 MSP(I,2) = 0
000232 2117 CONTINUE
000233 DO 2113 I=1,NDF
000235 DO 2113 J=1,NDF
000236 EM(I,J) = 0.0
000237 CC(I,J) = 0.0
000242 CAY(I,J) = 0.0
000245 FF(I,J) = 0.0
000247 UU(I,J) = 0.0
000252 2113 CONTINUE
000254 DO 2114 I=1,3
000260 DO 2114 J=1,4
000262 Q3(I,J) = 0.0
000263 Q2(I,J) = 0.0
000266 Y3(I,J) = 0.0
000270 Y2(I,J) = 0.0
000272 PX3(I,J) = 0.0
000274 PX2(I,J) = 0.0
000276 2114 CONTINUE
000303 DO 2115 I=1,3
000305 DO 2115 J=1,20
000306 Y1(I,J) = 0.0
000311 PX1(I,J) = 0.0
000313 F(I,J,I)=0.0
000315 2115 CONTINUE
000320 INTR=0
000324 IWEI = 0
000325

```

000326	IVE2 = 0	
000327	IVE3 = 0	
000330	IVE4 = 0	
000331	IVE5 = 0	
000332	IVE6 = 0	
000333	IVE7 = 0	
000334	IVE8 = 0	
000335	IVE9 = 0	
000336	IVE10 = 0	
000337	IVE11 = 0	
000340	IVE12 = 0	
000341	IVE13 = 0	
000342	IVE14 = 0	
000343	IVE15 = 0	
000344	IVE16 = 0	
000345	IVE17 = 0	
000346	IVE19 = 0	
000347	IVE20 = 0	
000350	IVE21 = 0	
000351	IVE22 = 0	
000352	IVE23 = 0	
000353	IVE24 = 0	
000354	NH = 0	
000355	I2 = 0	
000356	I10 = 0	
000357	IVE24 = 1	
000360	READ (5,24) (ISET(I), I = 1,NOT)	
000372	24 FORMAT (6I10)	
000372	25 READ (5,30) NAME	
000400	30 FORMAT (A6)	
000400	IF (NAME.EQ. INM1) GO TO 445	1124
000402	IF (NAME.EQ. INM2) GO TO 450	1125
000404	IF (NAME.EQ. INM3) GO TO 455	1126
000406	IF (NAME.EQ. INM4) GO TO 460	1127
000410	IF (NAME.EQ. INM5) GO TO 465	1128
000412	IF (NAME.EQ. INM6) GO TO 470	1129
000414	IF (NAME.EQ. INM7) GO TO 475	1130
000416	IF (NAME.EQ. INM8) GO TO 480	1131
000420	IF (NAME.EQ. INM9) GO TO 45	1132
000422	IF (NAME.EQ. INM10) GO TO 60	1133
000424	IF (NAME.EQ. INM11) GO TO 125	1134
000426	IF (NAME.EQ. INM12) GO TO 135	1135
000430	IF (NAME.EQ. INM13) GO TO 140	1136
000432	IF (NAME.EQ. INM14) GO TO 150	1137
000434	IF (NAME.EQ. INM15) GO TO 160	1138
000436	IF (NAME.EQ. INM16) GO TO 170	1139
000440	IF (NAME.EQ. INM17) GO TO 200	1140
000442	IF (NAME.EQ. INM18) GO TO 490	1141
000444	IF (NAME.EQ. INM19) GO TO 500	1142
000446	IF (NAME.EQ. INM20) GO TO 505	1143
000450	IF (NAME.EQ. INM21) GO TO 510	1144
000452	IF (NAME.EQ. INM22) GO TO 515	1145
000454	IF (NAME.EQ. INM23) GO TO 860	1146
000456	IF (NAME.EQ. INM24) GO TO 999	1147
000460	IF (NAME.EQ. INM25) GO TO 25	1148
000462	IF (NAME.EQ. INM26) GO TO 5	1149
000464	IF (NAME.EQ. INM27) GO TO 550	1150
000466	IF (NAME.EQ. INM28) GO TO 580	1151

```

000470 40 WRITE (6,32) NAME
000476 32 FORMAT (25H0 DO NOT RECOGNIZE NAME #,A6,1H#)
000476 GO TO 999
C INITIAL CONDITIONS
000477 45 READ (5,50) (KEY,I,S(1,I))
000512 50 FORMAT (11,15,5X,F12.6)
000512 IVE9 = 1
000513 IF (KEY) 25,45,25
C FORCING FUNCTIONS
000515 60 READ (5,65) KEY2,I
000525 65 FORMAT (11,15)
000525 IVE10 = 1
000526 70 READ (5,75) KEY1,J,KIND
000540 75 FORMAT (11,15,4X,11)
000540 IF (KIND.EQ.1) GO TO 83
000542 80 READ (5,50)(KEY,K,F(I,K,J))
000557 IF (KEY) 105,80,105
000561 83 WRITE (6,85)
000565 85 FORMAT (22H READ FUNCTION OF TIME)
000565 105 IF (KEY1.EQ.0) GO TO 70
000566 IF (KEY2) 25,60,25
C OBJECTIVE FUNCTION
000570 125 READ (5,130) KEY,I,J,PX1(I,J)
000606 130 FORMAT (11,215,F12.6)
000606 IVE11 = 1
000607 IF (KEY) 25,125,25
000611 135 READ (5,130) KEY,I,J,PX2(I,J)
000627 IVE12 = 1
000630 IF (KEY) 25,135,25
000632 140 READ (5,130) KEY,I,J,PX3(I,J)
000650 IVE13 = 1
000651 IF (KEY) 25,140,25
C CONSTRAINT
000653 150 READ (5,130) KEY,I,J,Y1(I,J)
000671 IVE14 = 1
000672 IF (KEY) 25,150,25
000674 160 READ (5,130) KEY,I,J,Y2(I,J)
000712 IVE15 = 1
000713 IF (KEY) 25,160,25
000715 170 READ (5,130) KEY,I,J,Y3(I,J)
000733 IVE16 = 1
000734 IF (KEY) 25,170,25
C BOUNDS OF CONSTRAINTS
000736 185 FORMAT (F12.6,15,F12.6)
000736 200 READ (5,205) KEY1,I,MSP(I,1),MSP(I,2)
000752 205 FORMAT (11,15,4X,11,4X,11)
000752 IVE17 = 1
000753 IF (MSP(I,1)-1) 210,290,350
000756 210 IF (MSP(I,2) -1)215,235,250
000761 215 READ (5,218) NCN
000767 218 FORMAT (1X,11)
000767 IF (NCN-1) 220,224,224
000772 220 READ (5,185) SVAL,NIC1,VIC1
001004 DO 222 K = 1,11
001006 222 YU(K,I) = SVAL
001015 223 IF (NIC1) 225,225,223
001016 223 IXX(I) = 1
001020 IZ = NIC1

```



```

001022 SZ1 = SVA1
001023 VZ1 = VIC1
001025 GO TO 225
001025 224 READ( 5,50) KEY,K,YU(K,I)
001041 IF (KEY.EQ. 0) GO TO 224
001042 225 READ (5,218) NCN
001050 IF (NCN-1) 226,230,230
001053 226 READ (5,185) SVA2,NIC2,VIC2
001065 227 YL(K,I) = 1,I
001067 227 YL(K,I) = SVA2
001076 IF (NIC2) 440,440,229
001077 229 IXX(I) = IXX(I)+2
001102 SZ2 = SVA2
001103 VZ2 = VIC2
001104 IZ = NIC2
001106 GO TO 440
001106 230 READ (5,50) KEY,K,YL(K,I)
001122 IF ( KEY) 440,230,440
001124 235 READ(5,218) NCN
001132 IF (NCN-1) 240,245,245
001135 240 READ(5,185) SVA1,NIC1,VIC1
001147 242 YU(K,I) = 1,I
001151 242 YU(K,I) = SVA1
001160 IF (NIC1) 440,440,243
001161 243 IXX(I) = 1
001163 IZ = NIC1
001165 SZ1 = SVA1
001166 VZ1 = VIC1
001170 GO TO 440
001170 245 READ(5,50) KEY,K,YU(K,I)
001204 IF (KEY) 440,245,440
001206 250 IF (HSP(I,2) -2) 225,225,235
001212 290 IF (HSP(I,2)-1)292,305,315
001215 292 READ(5,218) NCN
001223 IF (NCN-1) 295,300,300
001226 295 READ (5,293) SVA1,NIC1,VIC1,KS(I)
001242 293 FORMAT (F12.6,I5)
001242 K = KS(I)
001244 YU(K,I) = SVA1
001250 IF (NIC1) 301,301,299
001251 299 IXX(I) = 1
001253 IZ = NIC1
001255 SZ1 = SVA1
001256 VZ1 = VIC1
001260 GO TO 301
001260 300 READ (5,50) KEY,K,YU(K,I)
001274 KS (I) = K
001276 IF (KEY.EQ. 0) GO TO 300
001277 301 READ (5,218) NCN
001305 IF (NCN-1) 302,304,304
001310 302 READ(5,293) SVA2,NIC2,VIC2,KS(I)
001324 K = KS(I)
001326 YL(K,I) = SVA2
001332 IF (NIC2) 440,440,303
001333 303 IXX(I) = IXX(I)+2
001336 SZ2 = SVA2
001337 VZ2 = VIC2
001340 IZ = NIC2

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```

001342 GO TO 440
001342 304 READ (5,50) KEY,K,YL(K,I)
001356 KS(I) = K
001360 IF (KEY) 440,304,440
001362 305 READ (5,218) NCN
001370 IF (NCN-1) 307,310,310
001373 307 READ (5,293) SVA1,NIC1,VIC1,KS(I)
001407 K = KS(I)
001411 YU(K,I) = SVA1
001415 IF (NIC1) 440,440,308
001416 308 IXX(I) = 1
001420 IZ = NIC1
001422 SZ1 = SVA1
001423 VZ1 = VIC1
001425 GO TO 440
001425 310 READ (5,50) KEY,K,YU(K,I)
001441 KS(I) = K
001443 IF (KEY) 440,310,440
001445 315 IF (HSP(I,2)-2) 301,301,305
001451 350 IF (NSP(I,2)-2) 360,370,380
001454 360 CONTINUE
001454 370 CONTINUE
001454 380 CONTINUE
001454 READ (5,390) KI,KJ
001464 390 FORMAT (2I5)
001464 440 IF (KEY1) 25,200,25
001464 C A MATRIX
001466 445 READ(5,130) KEY,I,J,A(I,J)
001504 IVE1 = 1
001505 IF (KEY) 25,445,25
001505 C B MATRIX
001507 450 READ (5,130) KEY,I,J,B(I,J)
001525 IVE2 = 1
001526 IF (KEY) 25,450,25
001526 C D MATRIX
001530 455 READ (5,130) KEY,I,J,D(I,J)
001546 IVE3 = 1
001547 IF (KEY) 25,455,25
001547 C M MATRIX
001551 460 READ (5,130) KEY,I,J,EH(I,J)
001567 IVE4 = 1
001570 IF (KEY) 25,460,25
001570 C C MATRIX
001572 465 READ (5,130) KEY,I,J,CO(I,J)
001610 IVE5 = 1
001611 IF (KEY) 25,465,25
001611 C K MATRIX
001613 470 READ (5,130) KEY,I,J,CAY(I,J)
001631 IVE6 = 1
001632 IF (KEY) 25,470,25
001632 C F MATRIX
001634 475 READ (5,130) KEY,I,J,FF(I,J)
001652 IVE7 = 1
001653 IF (KEY) 25,475,25
001653 C U MATRIX
001655 480 READ (5,130) KEY,I,J,UU(I,J)
001673 IVE8 = 1
001674 IF (KEY) 25,480,25

```

C	MODIFY PROBLEM
001676	C 490 NM = NM+1
001700	WRITE (6,495) NM,(ITITL(I),I = 1,12)
001713	495 FORMAT (1M1,10X,16HMODIFICATION NO.,15,10X,12A5)
001713	INT = 0
001714	INP = 0
001715	IVE23 = 0
001716	GO TO 25
C	TABULATING
001716	500 READ (5,130) KEY,I,J,Q1(I,J)
001734	IVE19 = 1
001735	IF (KEY) 25,500,25
001737	505 READ (5,130) KEY,I,J,Q2(I,J)
001755	IVE20 = 1
001756	IF (KEY) 25,505,25
001760	510 READ (5,130) KEY,I,J,Q3(I,J)
001776	IVE21 = 1
001777	IF (KEY) 25,510,25
C	TRADE OFF DIAGRAM
002001	515 READ (5,555) ITD,KSWT
002011	GO TO 25
002012	550 READ (5,555) INP,INT
002022	555 FORMAT (2I5)
002022	IF (INP.EQ.0) GO TO 560
002023	CALL VERFY
002024	560 IF (INT.EQ.0) GO TO 25
002025	IF (IVE23.EQ.0) GO TO 25
002026	CALL VERFY2
002027	GO TO 25
002030	580 READ (5,75) KEY,I,ITR(I)
002042	IF (KEY) 25,580,25
002044	860 IF (NOE.EQ.-1) GO TO 865
002046	CALL COVERT
002047	865 IVE 23=1
002050	CALL HEXAP
002051	CALL BRIDGE
002052	CALL ELEMTP
002053	CALL ELEMTQ
002054	CALL RHDATA
002055	CALL POST
C	CALL LPDATA
002056	CALL PRNT
002057	IF (INT.EQ.0) GO TO 870
002060	CALL VERFY2
002061	870 IF (IZ.EQ.0) GO TO 25
002062	880 I = 1
002063	IZZ = IZ+1
002065	890 IF (IXX(I)) 910,1140,910
002067	910 IR = 1
002071	IF (IXX(I)-2) 920,940,960
002073	920 DO 922 L = 1,IZZ
002075	922 Y(L) = SZ1+(L-1)*VZ1
002105	IF (HSP(I,1).EQ.0) GO TO 930
002107	ID = 2
002110	GO TO 1110
002110	930 ID = 1
002111	GO TO 980
002112	940 DO 942 L = 1,IZZ

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002114 942 Y(L) = S22*(L-1)*VZ2
002124 IF (MSP(I,1) .EQ. 0) GO TO 950
002126 ID = 4
002127 GO TO 1110
002127 950 ID = 3
002130 GO TO 980
002131 960 DO 962 L = 1,1Z
002133 962 Y(L) = S24*(L-1)*VZ1
002143 IF (MSP(I,1) .EQ. 0) GO TO 970
002145 ID = 6
002146 GO TO 1110
002146 970 ID = 5
002147 980 DO 1100 L = 1,1Z
002151 111=11
002153 IF (ID -3) 982,986,990
002155 982 DO 984 K = 1,111
002157 YU(K,IR) = S21*L*VZ1
002166 984 CONTINUE
002170 GO TO 994
002171 986 DO 988 K = 1,111
002173 YL(K,IR) = S22*L*VZ2
002202 988 CONTINUE
002204 GO TO 994
002205 990 DO 992 K = 1,111
002207 YU(K,IR) = S21*L*VZ1
002215 YL(K,IR) = S22*L*VZ2
002222 992 CONTINUE
002224 994 CALL ELEMTP
002225 CALL ELEMTP
002226 PUNCH 789
002232 789 FORMAT(3HRHS)
002232 CALL RHOATA
002233 CALL PRNT
002234 IF (IMP .EQ. 0) GO TO 1100
002235 CALL VERFY
002236 1100 CONTINUE
002241 GO TO 1140
002241 1110 DO 1130 L = 1,1Z
002243 IR2 = KS(IR)
002245 IF (ID -4) 1112,1114,1116
002250 1112 YU(IR2,IR) = S21*L*VZ1
002257 GO TO 1120
002257 1114 YL(IR2,IR) = S22*L*VZ2
002266 GO TO 1120
002266 1116 YU(IR2,IR) = S21*L*VZ1
002275 YL(IR2,IR) = S22*L*VZ2
002302 1120 CALL ELEMTP
002303 CALL ELEMTP
002304 PUNCH 789
002310 CALL RHOATA
002311 CALL PRNT
002312 IF (IMP .EQ. 0) GO TO 1130
002313 CALL VERFY
002314 1130 CONTINUE
002317 GO TO 25
002317 1140 IF (I-NOC) 1150,25,25
002322 1150 I = I+1
002324 GO TO 890

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SUBROUTINE VERFY
COMMON/INIT/ ISP , MSP(8,2)
COMMON/INIT/ S(1,20)
COMMON/EKC/EN(10,10),CC(10,10),FF(10,4),CAY(10,10),UUI(10,4)
COMMON/UPL0/YU(20,5),YL(20,5),Y(20)
COMMON/FOFUN/F(1,20,3)
COMMON/ABD/A(20,20),B(20,4),D(20,4)
COMMON/OBJ/PX1(5,20),PX2(5,4),PX3(5,4)
COMMON/CONST/Y1(5,20),Y2(5,4),Y3(5,4)
COMMON/IIIST/ISEI(10)
COMMON/TAB/Q1( 3,20),Q2( 3,3),Q3( 3,3)
COMMON/RMS/ NOBF, NOC, NOB, NOT
COMMON /INPT/II,NZ,M,NF,NU,KI,KJ,NDF,MODE
COMMON/FORC/ NSETS
COMMON/VER/IVE1,IVE2,IVE3,IVE4,IVE5,IVE6,IVE7,IVE8,IVE9,IVE10
COMMON/VER1/IVE11,IVE12,IVE13,IVE14,IVE15,IVE16,IVE17,IVE19
COMMON/VER2/IVE20,IVE21,IVE23,IVE24
N = NDF
WRITE (6,5)
000004 5 FORMAT (27H VERIFICATION OF INPUT DATA)
000007 IF (IVE1.EQ. 0) GO TO 40
000010 WRITE (6,10)
000014 10 FORMAT (9H0A MATRIX)
000014 DO 20 I = 1,M
000016 20 WRITE (6,30) (A(I,J),J = 1,M)
000035 30 FORMAT (1X,10E12.5,(/6X,9E12.5))
000035 25 FORMAT(5X,2I5)
000035 35 FOMAT (1X,2HK=,14,10E12.5,(/ 6X,9E12.5))
000035 40 IF (IVE2.EQ. 0) GO TO 70
000036 WRITE (6,50)
000042 50 FORMAT (9H0B MATRIX)
000042 DO 60 I = 1,M
000044 60 WRITE (6,30) (B(I,J),J = 1,NU)
000063 70 IF (IVE3.EQ. 0) GO TO 90
000064 WRITE (6,75)
000070 75 FORMAT (9H0D MATRIX)
000070 DO 80 I = 1,M
000072 80 WRITE (6,30) (D(I,J),J = 1,NF)
000111 90 IF (IVE4.EQ. 0) GO TO 110
000112 WRITE (6,95)
000116 95 FORMAT (9H0C MATRIX)
000116 DO 100 I = 1,N
000120 100 WRITE (6,30) (EM(I,J),J = 1,N)
000136 110 IF (IVE5.EQ. 0) GO TO 130
000137 WRITE (6,115)
000143 115 FORMAT (9H0C MATRIX)
000143 DO 120 I = 1,N
000145 120 WRITE (6,30) (CG(I,J),J = 1,N)
000163 130 IF (IVE6.EQ. 0) GO TO 150
000164 WRITE (6,135)
000170 135 FORMAT (9H0C MATRIX)
000170 DO 140 I = 1,N
000172 140 WRITE (6,30) (CAY(I,J),J = 1,N)
000210 150 IF (IVE7.EQ. 0) GO TO 170
000211 WRITE (6,155)
000215 155 FORMAT (9H0F MATRIX)
000215 DO 160 I = 1,N

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000217 160 WRITE (6,30) (FF(I,J),J = 1,NF)
000235 170 IF (IVE8.EQ. 0) GO TO 190
000236 WRITE (6,175)
000242 175 FORMAT (9H0U MATRIX)
000242 DO 180 I = 1,N
000244 180 WRITE (6,30) (UU(I,J),J = 1,NU)
000262 190 IF (IVE9.EQ. 0) GO TO 200
000263 WRITE (6,195)
000267 195 FORMAT (19H0INITIAL CONDITIONS)
000267 WRITE (6,30) (S(I,I),I = 1,M)
000302 200 IF (IVE10.EQ. 0) GO TO 225
000303 WRITE (6,205)
000307 205 FORMAT (17H0FORCING FUNCTION)
000307 DO 220 IS = 1,NSETS
000311 WRITE (6,210)
000314 210 FORMAT (1H0)
000314 III = II-1
000316 DO 220 K = 1,III
000320 220 WRITE (6,30) (F(IS,K,J),J = 1,NF)
000341 225 IF (IVE11.EQ. 0) GO TO 240
000342 WRITE (6,230)
000346 230 FORMAT (11H0PX1 MATRIX)
000346 DO 235 I = 1,N08
000350 235 WRITE (6,30) (PX1(I,J),J = 1,M)
000366 240 IF (IVE12.EQ. 0) GO TO 260
000367 WRITE (6,245)
000373 245 FORMAT (11H0PX2 MATRIX)
000373 DO 250 I = 1,N08
000375 250 WRITE (6,30) (PX2(I,J),J = 1,NU)
000413 260 IF (IVE13.EQ. 0) GO TO 280
000414 WRITE (6,265)
000420 265 FORMAT (11H0PX3 MATRIX)
000420 DO 270 I = 1,N08
000422 270 WRITE (6,30) (PX3(I,J),J = 1,NF)
000440 280 IF (IVE14.EQ. 0) GO TO 300
000441 WRITE (6,285)
000445 285 FORMAT (10H0Y1 MATRIX)
000445 DO 290 I = 1,N0C
000447 290 WRITE (6,30) (Y1(I,J),J = 1,M)
000465 300 IF (IVE15.EQ. 0) GO TO 320
000466 WRITE (6,305)
000472 305 FORMAT (10H0Y2 MATRIX)
000472 DO 310 I = 1,N0C
000474 310 WRITE (6,30) (Y2(I,J),J = 1,NU)
000512 320 IF (IVE16.EQ. 0) GO TO 340
000513 WRITE (6,325)
000517 325 FORMAT (10H0Y3 MATRIX)
000517 DO 330 I = 1,N0C
000521 330 WRITE (6,30) (Y3(I,J),J = 1,NF)
000537 340 IF (IVE17.EQ. 0) GO TO 360
000540 WRITE (6,345)
000544 345 FORMAT (13H0UPPER BOUNDS)
000544 DO 350 K = 1,II
000546 350 WRITE (6,35) K,(YU(K,I),I = 1,N0C)
000567 WRITE (6,355)
000572 355 FORMAT (13H0LOWER BOUNDS)
000572 DO 360 K = 1,II
000574 360 WRITE (6,35) K,(YL(K,I),I = 1,N0C)

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000615 WRITE (6,365)
000620 365 FORMAT(21H0SPECIFICATION MATRIX)
000620 DO 370 I = 1,NOC
000622 370 WRITE( 6,25) (MSP(I,J),J = 1,2)
000637 380 IF (IVE19.EQ. 0) GO TO 400
000640 WRITE (6,385)
000644 385 FORMAT (10H001 MATRIX)
000644 DO 390 I = 1,NOT
000646 390 WRITE (6,30) (Q1(I,J),J = 1,M)
000664 400 IF (IVE20.EQ. 0) GO TO 420
000665 WRITE (6,405)
000671 405 FORMAT (10H002 MATRIX)
000671 DO 410 I = 1,NOT
000673 410 WRITE (6,30) (Q2(I,J),J = 1,NU)
000711 420 IF (IVE21.EQ. 0) GO TO 460
000712 WRITE (6,425)
000716 425 FORMAT (10H003 MATRIX)
000716 DO 430 I = 1,NOT
000720 430 WRITE (6,30) (Q3(I,J),J = 1,NF)
000736 460 IF (IVE24.EQ.0) GO TO 470
000737 WRITE (6,465)
000743 465 FORMAT (12H01SET VECTOR)
000743 WRITE (6,25) (ISET (I),I = 1,NOT)
000756 470 RETURN
000757 END

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SURROUTINE VERFY2
COMMON /INPT/ II,N,M,NF,NU,KI,KJ,NDF,MODE,IZ
COMMON /RMS/ NOBF,NOC,NOB,NOT
COMMON /FORC/ NSETS
COMMON /MT/NOE
COMMON /PRG/R(20,20,4),T(20,20,4)
COMMON /CSS/C1(20,20),C2(1,20,20),C(1,20,20)
COMMON /ABD/A(20,20),B(20,4),D(20,4)
COMMON /MXAP/ AEI(20,20),P(20,20)
WRITE (6,20)
000002 20 FORMAT (31H1DATA CALCULATED WITHIN PROGRAM)
000006 30 FORMAT (1X,10E12.5,(/11X,9E12.5))
000006 IF (NOE.EQ.1) GO TO 35
000010 WRITE (6,200)
000014 200 FORMAT (9H0A MATRIX)
000014 DO 210 I = 1,M
000016 210 WRITE (6,30) (A(I,J),J = 1,M)
000035 WRITE (6,220)
000040 220 FORMAT (9H0B MATRIX)
000040 DO 230 I = 1,M
000042 230 WRITE (6,30) (B(I,J),J = 1,NU)
000061 WRITE (6,240)
000064 240 FORMAT (9H0D MATRIX)
000064 DO 250 I = 1,M
000066 250 WRITE (6,30) (D(I,J),J = 1,NF)
000105 35 WRITE (6,40)
000111 40 FORMAT (9H0MATRIX R)
000111 III = II-1
000113 DO 60 K = 1,III
000115 WRITE (6,50)
000120 50 FORMAT (1H0)
000120 DO 60 I = 1,M
000122 60 WRITE (6,30) (R(K,I,J),J = 1,NU)
000145 WRITE (6,70)
000151 70 FORMAT (9H0MATRIX I)
000151 DO 80 K = 1,III
000153 WRITE (6,50)
000156 DO 80 I = 1,M
000160 80 WRITE (6,30) (I(K,I,J),J = 1,NF)
000203 WRITE (6,90)
000207 90 FORMAT (9H0MATRIX C)
000207 DO 100 IS = 1,NSETS
000211 WRITE (6,50)
000214 DO 100 K = 2,II
000216 100 WRITE (6,30) (C(IS,K,I),I = 1,M)
000237 WRITE (6,110)
000243 110 FORMAT (9H0MATRIX P)
000243 DO 120 I = 1,M
000245 120 WRITE (6,30) (P(I,J),J = 1,M)
000264 WRITE (6,130)
000267 130 FORMAT (11H0MATRIX AEI)
000267 DO 140 I = 1,M
000271 140 WRITE (6,30) (AEI(I,J), J = 1,M)
000310 RETURN
000310 END

```

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SUBROUTINE COVERT
COMMON/EKG/EM(10,10),CC(10,10),FF(10,4),CAY(10,10),UU(10,4)
000002 DIMENSION EM(10,10)
000002 DIMENSION CH(10,10),CYM(10,10),UM(10,10),FM(10,10)
000002 COMMON/ABD/A(20,20),B(20,4),D(20,4)
000002 COMMON /INPT/II,NZ,H,NF,NU,KI,KJ,NDF,MODE
000002 IF(NDF-1) 90,80,90
000004 80 EM(I,1) = 1./EM(I,1)
000006 N=NDF
000010 GO TO 100
000010 90 CALL MIV(EM,NDF,EM,10)
000013 N=NDF
000015 100 CALL M2X2 (N,N,N,EM,CC,CM)
000021 CALL M2X2 (N,N,N,EM,CAY,CYM)
000025 CALL M2X2(N,N,N,NU,EM,UU,UH)
000031 CALL M2X2(N,N,NF,EM,FF,FM)
000035 DO 125 I = 1,N
000037 A(I+N,I) = 1.0
000044 DO 125 J = 1,N
000045 A(I,J) = CH(I,J)*(-1.0)
000053 A(I,J+N) = CYM(I,J)*(-1.0)
000061 IF (J.GT. NF) GO TO 120
000064 O(I,J ) = FM(I,J)
000071 120 IF (J.GT. NU) GO TO 125
000075 B(I,J ) = UM(I,J)*(-1.0)
000103 125 CONTINUE
000110 RETURN
000110 END

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SURROUTINE BRIDGE

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000002 COMMON/INIT/ S(1,20)
000002 DIMENSION CT(1,20,20)
000002 COMMON/ERG/R(20,20,4),T(20,20,4)
000002 COMMON/CSS/C1(20,20),C2(1,20,20),C(1,20,20)
000002 COMMON/FOFUN/F(1,20,3)
000002 COMMON/ABD/A(20,20),B(20,4),O(20,4)
000002 COMMON /MXAP/ AEI(20,20),P(20,20)
000002 COMMON/FORC/ NSETS
000002 COMMON /INPT/ II,N,M,NF,NU,KI,KJ,NDF,MODE
000002 DO 220 I=1,N
000004 C1(I,I)=S(1,I)
000010 DO 210 J=1,NU
000012 R(I,I,J)=0.0
000017 DO 210 L=1,N
000020 R(L,I,J)=R(L,I,J)+AEI(I,L)*B(L,J)
000034 210 CONTINUE
000041 DO 220 J=1,NF
000042 T(1,I,J)=0.0
000047 DO 220 L=1,N
000050 T(L,I,J)=T(L,I,J)+AEI(I,L)*D(L,J)
000064 220 CONTINUE
000073 DO 500 K=2,II
000075 K4=K-1
000077 DO 330 I=1,N
000100 DO 310 J=1,NU
000101 R(K,I,J)=0.0
000106 DO 310 L=1,N
000110 R(K,I,J)=R(K,I,J)+P(I,L)*R(K4,L,J)
000127 310 CONTINUE
000134 DO 320 J=1,NF
000135 T(K,I,J)=0.0
000142 DO 320 L=1,N
000144 T(K,I,J)=T(K,I,J)+P(I,L)*T(K4,L,J)
000163 320 CONTINUE
000170 C1(K,I)=0.0
000173 DO 330 J=1,N
000175 C1(K,I)=C1(K,I)+P(I,J)*C1(K4,J)
000210 330 CONTINUE
000214 DO 430 IS=1,NSETS
000216 DO 390 L=1,N
000217 C2(IS,K,L)=0.0
000224 390 CONTINUE
000226 DO 400 I=1,K4
000230 KMI=K-I
000232 DO 410 IP=1,N
000233 CT(IS,K,IP)=0.0
000237 DO 410 J=1,NF
000241 CT(IS,K,IP)=CT(IS,K,IP)+T(KMI,IP,J)*F( IS,I,J)
000260 410 CONTINUE
000265 DO 420 L=1,N
000266 C2(IS,K,L)=C2(IS,K,L)+CT(IS,K,L)
000277 420 CONTINUE
000301 400 CONTINUE
000303 DO 430 I=1,N
000305 C(1S,K,I)=C1(K,I)+C2(IS,K,I)
000317 430 CONTINUE

```

000326 RETURN
000327 END

```

SUBROUTINE PRNT
COMMON /INPT/ II,N,M,NF,NU,KI,KJ,NOF,MODE
COMMON /PVAL/ H(120,80)
COMMON /RHV/ G(120),NRE(120)
COMMON /ALL/ INTR,KS(8)
251 JL = (II-1)*NU+1
000006 WRITE (6,225)
000011 225 FORMAT (9H0MATRIX H/1X,4HR0MS)
000011 DO 200 I = 1,INTR
000013 200 WRITE (6,250) (I,(H(I,J),J = 1,JL))
000034 250 FORMAT (1X,I4,5X, 7E14.7,(/15X,7E14.7))
000034 WRITE (6,350)
000037 350 FORMAT (26H1RHS VALUES AND EQUALITIES/1X,4HR0MS)
000037 DO 400 I = 1,INTR
000041 400 WRITE(6,450) I,NRE(I),G(I)
000055 450 FORMAT (1X,I4,3X,A1,3X,E12.5)
000055 DO 500 I = 1,INTR
000056 G(I) = 0.0
000057 NRE(I) = 0
000060 DO 500 J = 1,JL
000062 H(I,J) = 0.0
000066 500 CONTINUE
000073 INTR = 0
000073 RETURN
000074 END

```

```
000002 SUBROUTINE LPDATA
000004 MPSNM = SHEXRPI
000011 PUNCH 610,MPSNM
000011 610 FORMAT (4HNAME,10X,A6)
000011 PUNCH 612
000015 612 FORMAT (4HROWS)
000015 CALL RODATA
000016 PUNCH 620
000022 620 FORMAT (7HCOLUMNS)
000022 CALL CODATA
000023 PUNCH 625
000027 625 FORMAT (3HRHS)
000027 CALL RHDATA
000030 PUNCH 630
000034 630 FORMAT(6HBOUNDS)
000034 CALL BODATA
000035 PUNCH 660
000041 660 FORMAT(6HENDATA)
000041 RETURN
000042 END
```

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SUBROUTINE ROATA
COMMON/RHV/G(120),NRE(120)
COMMON/ALL/ INTR,KS(8)
ILAST = INTR
CHK = 3.
IFRST = 9
ISEC = 99
IF (ILAST - 9) 10,10,20
10 IFRST = ILAST
CHK = 1.
GO TO 40
20 IF(ILAST - 99) 30,30,40
30 ISEC = ILAST
CHK = 2.
40 IFRS1 = IFRST+1
ISEC2 = ISEC+1
PUNCH 42
42 FORMAT (1X,1HN,2X,4H0BJF)
DO 50 I = 1,IFRST
45 PUNCH 55,NRE(I),I
50 CONTINUE
55 FORMAT (1X,A1,2X,3HROW,11)
IF(CHK-1.) 100,100,60
60 DO 65 I = IFRS1,ISEC
63 PUNCH 70,NRE(I),I
65 CONTINUE
70 FORMAT(1X,A1,2X,3HROW,12)
IF(CHK -2.) 100,100,80
80 DO 85 I = ISEC2,ILAST
83 PUNCH 90,NRE(I),I
85 CONTINUE
90 FORMAT(1X,A1,2X,3HROW,13)
100 RETURN
000107 ENO

```


Address	Code	Comments
000002	SUBROUTINE C00DATA	
000002	COMMON/PVAL/H(120,88)	
000002	COMMON/ALL/ INIR,KS(8)	
000002	COMMON /INPT/ II,N,M,NF,NU,KI,KJ,NDF,MODE	
000002	253 FORMAT(4X,3HCOL,13,4X,3HROW,13,4X,E12.5)	
000002	85 FORMAT(4X,4HCOL1,6X,4H08JF,6X,E12.5)	
000002	95 FORMAT(4X,3HCOL,11,6X,3HROW,11,6X,E12.5)	
000002	115 FORMAT(4X,3HCOL,11,6X,3HROW,12,5X,E12.5)	
000002	133 FORMAT(4X,3HCOL,11,6X,3HROW,13,4X,E12.5)	
000002	163 FORMAT(4X,3HCOL,12,5X,3HROW,11,6X,E12.5)	
000002	182 FORMAT(4X,3HCOL,12,5X,3HROW,12,5X,E12.5)	
000002	223 FORMAT(4X,3HCOL,13,4X,3HROW,11,6X,E12.5)	
000002	202 FORMAT(4X,3HCOL,12,5X,3HROW,13,4X,E12.5)	
000002	238 FORMAT(4X,3HCOL,13,4X,3HROW,12,5X,E12.5)	
000002	ILAST = INIR	
000004	JLAST = (11-11)*NU+1	
000010	CHJ = 3.	
000011	CHK = 3.	
000012	IFRST = 9	
000013	ISEC = 99	
000014	IF (ILAST -9) 10,10,20	
000016	10 IFRST = ILAST	
000020	CHK = 1.	
000021	GO TO 40	
000022	20 IF(ILAST -99) 30,30,40	
000025	30 ISEC = ILAST	
000027	CHK = 2.	
000030	40 JFRST = 9	
000031	JSEC = 99	
000032	IF(JLAST-9) 50,50,60	
000035	50 JFRST = JLAST	
000037	CHJ = 1.	
000040	GO TO 80	
000041	60 IF(JLAST-99) 70,70,80	
000044	70 JSEC = JLAST	
000046	CHJ = 2.	
000047	80 IFRS1 = IFRST+1	
000051	ISEC2 = ISEC+1	
000053	JFRS1 = JFRST+1	
000054	JSEC2 = JSEC+1	
000056	X0BJ = 1.0	
000057	PUNCH 85,X0BJ	
000055	DO 130 J = 1,JFRST	
000057	DO 93 I = 1,IFRST	
000070	IF(H(I,J))90,93,90	
000074	90 PUNCH 95,J,I, H(I,J)	
000110	93 CONTINUE	
000113	IF(CHK-1.) 130,130,100	
000115	DO 113 I = IFRS1,ISEC	
000117	IF(H(I,J))110,113,110	
000123	110 PUNCH 115,J,I, H(I,J)	
000137	113 CONTINUE	
000142	IF(CHK-2.) 130,130,120	
000144	DO 128 I = ISEC2,ILAST	
000146	IF(H(I,J))125,128,125	
000152	125 PUNCH 135,J,I, H(I,J)	
000166	128 CONTINUE	

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000171 130 CONTINUE
000174 140 IF(CHJ-1.) 260,260,150
000177 150 DO 200 J = JFRS1,I,SEC
000201 DO 160 I = 1,IFRS1
000202 IF( H(I,J))158,160,158
000206 158 PUNCH 163,J,I, H(I,J)
000222 160 CONTINUE
000225 IF(CHK -1.) 200,200,170
000227 170 DO 180 I = IFRS1,I,SEC
000231 IF( H(I,J))175,180,175
000235 175 PUNCH 182,J,I, H(I,J)
000251 180 CONTINUE
000254 IF(CHK-2.) 200,200,190
000256 190 DO 198 I = ISEC2,I,IASI
000260 IF( H(I,J))195,198,195
000264 195 PUNCH 202,J,I, H(I,J)
000300 198 CONTINUE
000303 200 CONTINUE
000306 205 IF(CHJ-2.) 260,260,210
000311 210 DO 250 J = JSEC2,J,IASI
000313 DO 220 I = 1,IFRS1
000314 IF( H(I,J))218,220,218
000320 218 PUNCH 223,J,I, H(I,J)
000334 220 CONTINUE
000337 IF(CHK-1.) 250,250,225
000341 225 DO 235 I = IFRS1,I,SEC
000343 IF( H(I,J))230,235,230
000347 230 PUNCH 238,J,I, H(I,J)
000363 235 CONTINUE
000366 IF(CHK-2.) 250,250,240
000370 240 DO 248 I = ISEC2,I,IASI
000372 IF( H(I,J))245,248,245
000376 245 PUNCH 253,J,I, H(I,J)
000412 248 CONTINUE
000415 250 CONTINUE
000420 260 RETURN
000421 END

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SUBROUTINE RHDATA
000002 COMMON/RHV/G(120),NRE(120)
000002 COMMON/ALL/ INTR,KS(8)
000002 85 FORMAT(4X,4HRHS1,6X,3HROW,12,5X,E12.5)
000002 55 FORMAT(4X,4HRHS1,6X,3HROW,11,6X,E12.5)
000002 115 FORMAT (4X,4HRHS1,6X,3HROW,13,4X,E12.5)
000002 ILAST = INTR
000003 CHK = 3.
000005 IFRST = 9
000006 ISEC = 99
000007 IF(ILAST - 9) 10,10,20
000012 10 IFRST = ILAST
000013 CHK = 1.
000015 GO TO 40
000016 20 IF(ILAST-99) 30,30,40
000021 30 ISEC = ILAST
000022 CHK = 2.
000024 40 IFRST = IFRST+1
000026 ISEC2 = ISEC+1
000030 00 60 I = 1,IFRST
000031 IF(G(I)) 50,60,90
000033 50 PUNCH 55,I,G(I)
000043 60 CONTINUE
000046 IF(CHK-1.) 130,130,70
000050 70 00 90 I = IFRST,ISEC
000052 IF(G(I)) 80,90,80
000054 80 PUNCH 85,I,G(I)
000064 90 CONTINUE
000067 IF(CHK-2.) 130,130,100
000071 100 00 120 I = ISEC2,ILAST
000073 IF(G(I)) 110,120,110
000075 110 PUNCH 115,I,G(I)
000105 120 CONTINUE
000110 130 RETURN
000111 END

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SUBROUTINE BODATA
COMMON /INPT/ II,N,M,NF,NU,KI,KJ,NDF,MODE
JLAST=(II-1)*NU+1
CHJ=3.
JFRST = 9
JSEC=99
IF (JLAST-9) 10,10,20
10 JFRST=JLAST
CHJ=1.
GO TO 40
20 IF (JLAST-99) 30,30,40
30 JSEC=JLAST
CHJ=2.
40 JFRST=JFRST+1
JSEC=JSEC+1
DO 90 J=2,JFRST
PUNCH 50,J
50 FORMAT(1X,2HFR,1X,4HBDS1,6X,3HCOL,I1)
90 CONTINUE
IF (CHJ - 1.) 160,160,100
100 DO 120 J=JFRST,JSEC
PUNCH 60,J
60 FORMAT(1X,2HFR,1X,4HBDS1,6X,3HCOL,I2)
120 CONTINUE
IF (CHJ-2.) 160,160,130
130 DO 150 J=JSEC,JLAST
PUNCH 70,J
70 FORMAT(1X,2HFR,1X,4HBDS1,6X,3HCOL,I3)
150 CONTINUE
160 RETURN
END
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SUBROUTINE ELEMTIP
COMMON/BRG/R(20,20,4),T(20,20,4)
COMMON/CSS/C1(20,20),C2(1,20,20),C(1,20,20)
COMMON/FOF/F(1,20,3)
COMMON/OBJ/PX1(5,20),PX2(5,4),PX3(5,4)
COMMON/ELS/C4(20,20)
COMMON/PVAL/H(120,80)
COMMON/RHV/G(120),NRE(120)
COMMON/RMID/ISP,MSPI(8,2)
COMMON/INPT/II,N,M,NF,NU,KI,KJ,NDF,MODE
COMMON/ALL/INITR,KS(8)
COMMON/FORC/NSETS
COMMON/RWS/NOBF,NOG,NOB,NOT
DO 1 I=1,120
  G(I)=0.0
  NRE(I)=0
DO 1 J=1,80
  H(I,J)=0.0
1 CONTINUE
DO 850 I=1,NOB
  CALL SEARCH(I,N,PX1,ISH,5,20)
  IF (ISH.EQ.0) GO TO 600
  CALL SEARCH(I,NU,PX2,ISH,5,4)
  IF (ISH.EQ.0) GO TO 500
400 JL=NU+1
  IL=II-2
  IX=2*IL
  IIX=II-1
  DO 415 K=2,IIX
  CALL M12X3(K,I,N,NU,PX1,R,C4)
  IP=INITR+(K-1)
  IQ=IP+IL
  HIP,1)=-1.0
  H(IQ,1)=1.0
  DO 405 J=2,JL
  H(IP,J)=C4(I,J-1)
  H(IQ,J)=H(IP,J)
  H(IP,J+NU)=PX2(I,J-1)
  H(IQ,J+NU)=H(IP,J+NU)
405 CONTINUE
  IF (K.EQ.2) GO TO 415
  JF=K*NU+1
  JL1=JL+1
  DO 410 J=JL1,JF
  H(IP,J)=H(IP-1,J-NU)
  H(IQ,J)=H(IP,J)
410 CONTINUE
415 CONTINUE
DO 450 IS=1,NSETS
  DO 450 K=2,IIX
  JK=K*NU+1
  IP=INITR+(IS-1)*IX+K-1
  IQ=IP+IL
  G(IP)=0.0
  DO 420 J=1,NF
  G(IP)=G(IP)-PX3(I,J)*F(IS,K,J)
420 CONTINUE

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000201      DO 423 J = 1,N
000203      G(IIP) = G(IIP)-PX1(I,J)*C(IS,K,J)
000215      423 CONTINUE
000217      G(IQ) = G(IIP)
000222      IF (ISP.EQ.0) GO TO 425
000223      NRE(IP) = 1HG
000225      NRE(IQ) = 1HL
000227      GO TO 430
000227      425 NRE(IP) = 1HL
000231      NRE(IQ) = 1HG
000233      430 IF (IS.EQ.1) GO TO 450
000235      DO 440 J = 1,JK
000237      H(IP,J) = H(IP-IX,J)
000245      H(IQ,J) = H(IQ-IX,J)
000251      440 CONTINUE
000254      450 CONTINUE
000261      GO TO 800
000262      500 JL = NU+1
000264      IL = II-1
000266      IX = 2*IL
000267      DO 515 K = 2,II
000270      CALL H12X3 (K,I,N,NU,PX1,R,C4)
000276      IP = INITR+(K-1)
000301      IQ = IP+IL
000303      H(IP,1) = -1.0
000304      H(IQ,1) = 1.
000306      DO 505 J = 2,JL
000310      H(IP,J) = C4(I,J-1)
000316      H(IQ,J) = H(IP,J)
000324      505 CONTINUE
000326      IF (K.EQ.2) GO TO 515
000330      JF = (K-1)*NU+1
000334      JUL = JL+1
000335      DO 510 J = JL1,JF
000336      H(IP,J) = H(IP-1,J-NU)
000345      H(IQ,J) = H(IP,J)
000352      510 CONTINUE
000354      515 CONTINUE
000357      DO 560 IS = 1,NSETS
000360      DO 560 K = 2,II
000361      JK = (K-1)*NU+1
000365      IP = INITR+(IS-1)*IX+K-1
000372      IQ = IP+IL
000374      G(IP) = 0.0
000375      DO 520 J = 1,NF
000376      G(IP) = G(IP) -PX3(I,J)*F(IS,K-1,J)
000410      520 CONTINUE
000412      DO 523 J = 1,N
000414      G(IP) = G(IP)-PX1(I,J)*C(IS,K,J)
000426      523 CONTINUE
000430      G(IQ) = G(IP)
000433      IF (ISP.EQ.0) GO TO 530
000434      NRE(IP) = 1HG
000436      NRE(IQ) = 1HL
000440      GO TO 540
000440      530 NRE(IP) = 1HL
000442      NRE(IQ) = 1HG
000444      540 IF (IS.EQ.1) GO TO 560

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000450 H(IQ,J) = H(IQ-IX,J)
000456 550 CONTINUE
000462 H(IQ,J) = H(IQ-IX,J)
000465 560 CONTINUE
000472 GO TO 800
000473 600 CALL SEARCH (I,NF,PX3,ISH,5,6)
000477 IF (ISH.EQ.0) GO TO 700
000500 IL = II-1
000502 DO 630 IS = 1,NSETS
000504 DO 630 K = 1,IL
000505 IP = (IS-1)*(II-1)+2+(K-1)*+INIR
000515 IQ = IP+IL
000517 H(IP,I) = -1.0
000521 H(IQ,I) = 1.0
000523 IF (ISP.EQ.0) GO TO 605
000524 NRE(IP) = 1HG
000525 NRE(IQ) = 1HL
000527 GO TO 610
000527 605 NRE(IP) = 1HL
000531 NRE(IQ) = 1HG
000533 610 G(IP) = 0.0
000535 DO 620 L = 1,NF
000536 G(IP) = G(IP)-PX3(I,L)*F(IS,K,L)
000550 620 CONTINUE
000552 J1 = 1+(K-1)*NU
000556 DO 635 J = 1,NU
000560 JP = J1+J
000562 H(IP,JP) = PX2(I,J)
000570 H(IQ,JP) = PX2(I,J)
000575 635 CONTINUE
000577 630 CONTINUE
000604 GO TO 800
000605 700 IL = II-1
000607 DO 720 K = 1,IL
000611 J1 = 1+(K-1)*NU
000615 I1 = INIR + (K-1)
000617 IP = I1+1
000620 IQ = IL+IP
000621 H(IP,I) = -1.0
000623 H(IQ,I) = 1.0
000625 IF (ISP.EQ.0) GO TO 705
000626 NRE(IP) = 1HG
000627 NRE(IQ) = 1HL
000631 GO TO 710
000631 705 NRE(IP) = 1HL
000633 NRE(IQ) = 1HG
000635 710 DO 715 J = 1,NU
000637 JP = J1+J
000641 H(IP,JP) = PX2(I,J)
000647 H(IQ,JP) = PX2(I,J)
000654 715 CONTINUE
000656 720 CONTINUE
000661 800 INIR = IQ
000663 850 CONTINUE
000665 RETURN
000666 END

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000002	SUBROUTINE ELEMTO
000002	COMMON /RWD/ ISP ,MSP(0,2)
000002	COMMON /RMS/ NOBF, NOG, NOB, NOI
000002	DO 399 I = 1, NOC
000004	200 IF (MSP(I,2) -1) 250,251,205
000007	205 IF (MSP(I,2) -2) 252,252,253
000013	250 CALL ELEMTR (I)
000015	CALL ELEMTR (I)
000017	GO TO 399
000020	251 CALL ELEMTR (I)
000022	GO TO 399
000023	252 CALL ELEMTR (I)
000025	GO TO 399
000026	253 CALL ELEMTR (I)
000030	399 CONTINUE
000033	RETURN
000033	END


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000003 COMMON/PVAL/HI(20,80)
000003 COMMON/RHV/G(120),NRE(120)
000003 COMMON/ERG/R(20,20,4),T(20,20,4)
000003 COMMON/CSS/C1(20,20),C2(1,20,20),C(1,20,20)
000003 COMMON/FOFUN/F(1,20,3)
000003 COMMON/UPLD/YU(20,5),YL(20,5),Y(20)
000003 COMMON/CONST/Y1(5,20),Y2(5,4),Y3(5,4)
000003 COMMON/ELS/C4(20,20)
000003 COMMON/RNID/ISP,HSP(8,2)
000003 COMMON/INPT/II,N,M,NF,NU,KI,KJ,NDF,MODE
000003 COMMON/ALL/INTR,KS(8)
000003 COMMON/FORC/ NSETS
000003 COMMON/RHS/ NOBF, NOC, NOB, NOT
000003 CALL SEARCH (I,N,Y1,ISH,5,20)
000007 IF (ISH.EQ. 0) GO TO 400
000011 CALL SEARCH (I,NU,Y2,ISH,5,4)
000015 IF (ISH.EQ. 0) GO TO 300
000017 200 IF (HSP(I,1).NE. 0) GO TO 205
000021 KINIT = 2
000022 KLAST = II-1
000024 GO TO 208
000024 205 KINIT = KS(I)
000026 KLAST = KS(I)
000030 IP=INTR+1
000032 DO 213 L=2, KINIT
000033 LL=KINIT -L+2
000036 CALL M12X3(LL,I,N,NU,Y1,R,C4)
030045 J1=1+(L-2)*NU
000052 J11=J1+1
000053 J2=J1+NU
000056 DO 214 J=J11,J2
000056 214 H(IP,J)=C4(I,J-J1)
000071 213 CONTINUE
000074 J3=J2+1
000076 J4=J2+NU
000100 DO 216 J=J3,J4
000102 216 H(IP,J)=Y2(I,J-J2)
000115 GO TO 227
000116 208 JL = NU+1
000120 IL = II-2
000122 DO 220 K = KINIT ,KLAST
000124 CALL M12X3 (K,I,N,NU,Y1,R,C4)
000133 IF (HSP(I,1).NE. 0) GO TO 209
000136 IP = INTR +(K-1)
000141 GO TO 211
000141 209 IP = INTR +1
000143 211 DO 210 J = 2,JL
000145 H(IP,J) =C4(I,J-1)
000153 H(IP,J+NU) = Y2(I,J-1)
000161 210 CONTINUE
000164 IF (HSP(I,1).NE. 0) GO TO 220
000166 IF (K.LE. 2) GO TO 220
000170 JF = K*NU+1
000174 JL1 = JL+1
000175 DO 215 J = JL1,JF
000176 H(IP,J) = H(IP-1,J-NU)

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000206 215 CONTINUE
000210 220 CONTINUE
000213 227 DO 240 IS = 1,NSETS
000215 DO 240 K = KINIT, KLAST
000217 JK = K*NU+1
000223 IF (MSP(I,1) .NE. 0) GO TO 221
000225 IP = INITR+(IS-1)*IL+K-1
000232 GO TO 222
000233 221 IP = INITR+(IS-1)+1
000236 K = KS(I)
000240 IL = 1
000241 222 G(IP) = 0.0
000243 DO 230 J = 1,NF
000244 G(IP) = G(IP) - Y3(I,J)*F(IS,K,J)
000255 230 CONTINUE
000257 DO 233 J = 1,N
000261 G(IP) = G(IP) - Y1(I,J)*C(IS,K,J)
000272 233 CONTINUE
000274 G(IP) = G(IP)+YU(K,I)
000302 NRE(IP) = IHL
000303 IF (IS .EQ. 1) GO TO 240
000305 DO 235 J = 1,K
000307 H(IP,J) = H(IP-IL,J)
000317 235 CONTINUE
000321 240 CONTINUE
000326 GO TO 550
000327 300 IF (MSP(I,1) .NE. 0) GO TO 305
000331 KINIT = 2
000332 KLAST = II
000333 GO TO 308
000334 305 KINIT = KS(I)
000336 KLAST = KS(I)
000340 IP=INITR+1
000342 DO 313 L=2, KINIT
000343 LL=KINIT -L+2
000346 CALL M12X3(LL,I,N,NU,Y1,R,C4)
000355 J1=1+(L-2)*NU
000362 J1=J1+1
000363 J2=J1+NU
000364 DO 314 J=J1,J2
000366 314 H(IP,J)=C4(I,J-J1)
000401 313 CONTINUE
000404 GO TO 332
000404 308 JL = NU+1
000406 IL = II-1
000410 DO 320 K = KINIT, KLAST
000412 KJ=K-1
000414 DO 401 J=1,NU
000415 C4(I,J)=0.0
000420 DO 401 L=1,N
000422 C4(I,J)=C4(I,J)+Y1(I,L)*R(KJ,L,J)
000436 401 CONTINUE
000443 IF (MSP(I,1) .NE. 0) GO TO 309
000445 IP = INITR +K-1
000447 GO TO 311
000450 309 IP = INITR +1
000452 K = KS(I)
000454 311 DO 310 J = 2,JL

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000456 H(IP,J) = C4(I,J-1)
000465 310 CONTINUE
000467 IF (MSP(I,1) .NE. 0) GO TO 320
000471 IF (K .LE. 2) GO TO 320
000473 JF = (K-1)*NU+1
000477 JL1 = JL+1
000500 00 315 J = JF
000501 H(IP,J) = H(IP-1,J-NU)
000511 315 CONTINUE
000513 320 CONTINUE
000516 322 DO 335 IS = 1,NSEIS
000520 00 335 K = KINIT, KLAST
000522 JK = (K-1)*NU+1
000526 IF (MSP(I,1) .NE. 0) GO TO 321
000530 IP = INITR+(IS-1)*IL+K-1
000535 GO TO 322
000536 321 IP = INITR+(IS-1)+1
000541 K = KS(I)
000543 IL = 1
000544 322 G(IP) = 0.0
000546 00 325 J = 1,NF
000547 G(IP) = G(IP) - Y3(I,J)*F(IS,K,J)
000560 325 CONTINUE
000562 00 328 J = 1,N
000564 G(IP) = G(IP) - V1(I,J)*C(IS,K,J)
000575 328 CONTINUE
000577 G(IP) = G(IP)+YU(K,I)
000605 NRE(IP) = 1HL
000606 IF (IS .EQ. 1) GO TO 335
000610 00 330 J = 1,JK
000612 H(IP,J) = H(IP-IL,J)
000622 330 CONTINUE
000624 335 CONTINUE
000631 00 330 GO TO 550
000632 400 CALL SEARCH (I,NF,Y3,ISM,5,4)
000636 IF (ISM .EQ. 0) GO TO 500
000640 IF (MSP(I,1) .NE. 0) GO TO 405
000642 KINIT = 1
000643 KLAST = II-1
000645 00 405 GO TO 408
000645 405 KINIT = KS(I)
000647 KLAST = KS(I)
000651 408 IL = II-1
000653 00 420 IS = 1,NSEIS
000655 00 420 K = KINIT, KLAST
000657 IF (MSP(I,1) .NE. 0) GO TO 409
000661 IP = (IS-1)*(II-1)+(K-1)+1+INITR
000670 GO TO 411
000671 409 IP = INITR+(IS-1)+1
000674 K = KS(I)
000676 411 NRE(IP) = 1HL
000700 G(IP) = 0.0
000701 00 410 L = 1,NF
000703 410 G(IP) = G(IP)-Y3(I,L)*F(IS,K,L)
000716 G(IP) = G(IP)+YU(K,I)
000724 J1 = 1+(K-1)*NU
000727 00 415 J = 1,NU
000731 JP = J1+J

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000733 H(IP,JP) = Y2(I,J)
000741 415 CONTINUE
000743 420 CONTINUE
000750 GO TO 550
000750 500 IF (MSP(I,1) .NE. 0) GO TO 505
000752 KINIT = 1
000753 KLAST = II-1
000755 GO TO 508
000755 505 KINIT = KS(I)
000757 KLAST = KS(I)
000761 508 IL = II-1
000763 DO 515 K = KINIT, KLAST
000765 J1 = 1+(K-1)*NU
000771 IF (MSP(I,1) .NE. 0) GO TO 506
000773 I1 = INITR+(K-1)
000776 IP = I1+1
000777 GO TO 507
000777 506 IP = INITR +1
001001 K = KS(I)
001003 507 NRE(IP) = 1HL
001005 G(IP) = YU(K,I)
001012 DO 510 J = 1,NU
001013 JP = J1+J
001015 H(IP,JP) = Y2(I,J)
001023 510 CONTINUE
001025 515 CONTINUE
001027 550 INTR = IP
001031 RETURN
001031 END

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000003	SUBROUTINE ELEMTS (I)
000003	COMMON/PVAL/H(120,80)
000003	COMMON/RHV/G(120),NRE(120)
000003	COMMON/ELS/C4(20,20)
000003	COMMON/BRG/R(20,20,4),T(20,20,4)
000003	COMMON/CSS/C1(20,20),C2(1,20,20),C(1,20,20)
000003	COMMON/FOFUN/F(1,20,3)
000003	COMMON/UPLO/YU(20,5),YL(20,5),Y(20)
000003	COMMON/CONST/YI(5,20),Y2(5,4),Y3(5,4)
000003	COMMON /RMID/ ISP ,MSP(6,2)
000003	COMMON /INPT/ II,N,M,NF,NU,KI,KJ,NDF,MODE
000003	COMMON/ALL/ INITR,KS(8)
000003	COMMON/FORC/ NSETS
000003	COMMON /RWS/ NOBF,NGC,NOB,NOT
000003	CALL SEARCH (I,N,Y1,ISH,5,20)
000007	IF (ISH .EQ. 0) GO TO 400
000011	CALL SEARCH (I,NU,Y2,ISH,5,4)
000015	IF (ISH .EQ. 0) GO TO 300
000017	200 IF (MSP (I,1) .NE. 0) GO TO 205
000021	KINIT = 2
000022	KLAST = II-1
000024	GO TO 208
000024	205 KINIT = KS(I)
000026	KLAST = KS(I)
000030	IP=INITR+1
000032	DO 213 I=2, KINIT
000033	LL=KINIT -L+2
000036	CALL M12X3(LL,I,N,NU,Y1,R,C4)
000045	J1=1+(L-2)*NU
000052	J11=J1+1
000053	J2=J1+NU
000054	DO 214 J=J11,J2
000056	214 H(IP,J)=C4(I,J-J1)
000071	213 CONTINUE
000074	J3=J2+1
000076	J4=J2+NU
000100	DO 216 J=J3,J4
000102	216 H(IP,J)=Y2(I,J-J2)
000115	GO TO 227
000116	208 JL = NU+1
000120	IL = II-2
000122	DO 220 K = KINIT ,KLAST
000124	CALL M12X3 (K,I,N,NU,Y1,R,C4)
000133	IF (MSP(I,1) .NE. 0) GO TO 209
000136	IP = INITR +(K-1)
000141	GO TO 211
000141	209 IP = INITR +1
000143	211 DO 210 J = 2,JL
000145	H(IP,J) =C4(I,J-1)
000153	H(IP,J +NU) = Y2(I,J-1)
000161	210 CONTINUE
000164	IF (MSP(I,1) .NE. 0) GO TO 220
000166	IF (K .LE. 2) GO TO 220
000170	JF = K*NU+1
000174	JL1 = JL+1
000175	DO 215 J = JL1,JF
000176	H(IP,J) = H(IP-1,J-NU)

```

000206 215 CONTINUE
000210 220 CONTINUE
000213 227 DO 240 IS = 1,NSETS
000215 DO 240 K = KINIT,KLAST
000217 JK = K*NU+1
000223 IF (MSP(I,1) .NE. 0) GO TO 221
000225 IP = INTR+(IS-1)*IL+K-1
000232 GO TO 222
000233 221 IP = INTR+(IS-1)+1
000236 K = KS(I)
000240 IL = 1
000241 222 G(IP) = 0.0
000243 DO 230 J = 1,NF
000244 G(IP) = G(IP) - Y3(I,J)*F(IS,K,J)
000255 230 CONTINUE
000257 DO 233 J = 1,N
000261 G(IP) = G(IP) - Y1(I,J)*G(IS,K,J)
000272 233 CONTINUE
000274 G(IP) = G(IP)+YL(K,I)
000302 NRE(IP) = 1HG
000303 IF (IS .EQ. 1) GO TO 240
000305 DO 235 J = 1,JK
000307 H(IP,J) = H(IP-IL,J)
000317 235 CONTINUE
000321 240 CONTINUE
000326 GO TO 550
000327 300 IF (MSP(I,1) .NE. 0) GO TO 305
000331 KINIT = 2
000332 KLAST = II
000333 GO TO 308
000334 305 KINIT = KS(I)
000336 KLAST = KS(I)
000340 IP=INTR+1
000342 DO 313 L=2, KINIT
000343 LL=KINIT -L+2
000346 CALL M12X3(LL,I,N,NU,Y1,R,C4)
000355 J1=1+(L-2)*NU
000362 J11=J1+1
000363 J2=J1+NU
000364 DO 314 J=J11,J2
000366 314 H(IP,J)=C4(I,J-J1)
000401 313 CONTINUE
000404 GO TO 332
000406 308 JL = NU+1
000406 IL = II-1
000410 DO 320 K = KINIT,KLAST
000412 CALL M12X3 (K,I,N,NU,Y1,R,C4)
000421 IF (MSP(I,1) .NE. 0) GO TO 309
000424 IP = INTR +K-1
000426 GO TO 311
000427 309 IP = INTR +1
000431 K = KS(I)
000433 311 DO 310 J = 2,JL
000435 H(IP,J) = C4(I,J-1)
000444 310 CONTINUE
000446 IF (MSP(I,1) .NE. 0) GO TO 320
000450 IF (K .LE. 2) GO TO 320
000452 JF = (K-1)*NU+1

```

```

000456 J1 = J1+1
000457 DO 315 J = J1, JF
000460 H(IP, J) = H(IP-1, J-NU)
000470 315 CONTINUE
000472 320 CONTINUE
000475 332 DO 335 IS = 1, NSEIS
000477 DO 335 K = KINIT, KLAST
000501 JK = (K-1)*NU+1
000505 IF (MSP(I, 1) .NE. 0) GO TO 321
000507 IP = INTR+(IS-1)*IL+K-1
000514 GO TO 322
000515 321 IP = INTR+(IS-1)+1
000520 K = KS(I)
000522 IL = 1
000523 322 G(IP) = 0.0
000525 DO 325 J = 1, NF
000526 G(IP) = G(IP) - V3(I, J)*F(IS, K, J)
000537 325 CONTINUE
000541 DO 328 J = 1, N
000543 G(IP) = G(IP) - Y1(I, J)*C(IS, K, J)
000554 328 CONTINUE
000556 G(IP) = G(IP)+YL(K, I)
000564 NRE(IP) = 1HG
000565 IF (IS .EQ. 1) GO TO 335
000567 DO 330 J = 1, JK
000571 H(IP, J) = H(IP-IL, J)
000601 330 CONTINUE
000603 335 CONTINUE
000610 GO TO 550
000611 400 CALL SEARCH (I, NF, Y3, ISH, 5, 4)
000615 IF (ISH .EQ. 0) GO TO 500
000617 IF (MSP(I, 1) .NE. 0) GO TO 405
000621 KINIT = 1
000622 KLAST = II-1
000624 GO TO 408
000624 405 KINIT = KS(I)
000626 KLAST = KS(I)
000630 408 IL = II-1
000632 DO 420 IS = 1, NSEIS
000634 DO 420 K = KINIT, KLAST
000636 IF (MSP(I, 1) .NE. 0) GO TO 409
000640 IP = (IS-1)*(II-1)+(K-1)+1, INTR
000647 GO TO 411
000650 409 IP = INTR+(IS-1)+1
000653 K = KS(I)
000655 411 NRE(IP) = 1HG
000657 G(IP) = 0.0
000660 DO 410 L = 1, NF
000662 G(IP) = G(IP)-Y3(I, L)*F(IS, K, L)
000675 G(IP) = G(IP)+YL(K, I)
000703 J1 = 1+(K-1)*NU
000706 DO 415 J = 1, NU
000710 JP = J1+J
000712 H(IP, JP) = Y2(I, J)
000720 415 CONTINUE
000722 420 CONTINUE
000727 GO TO 550
000727 500 IF (MSP(I, 1) .NE. 0) GO TO 505

```

```

000731 KINIT = 1
000732 KLAST = II-1
000733 GO TO 508
000734 505 KINIT = KS(I)
000735 KLAST = KS(I)
000736
000740 508 IL = II-1
000742 DO 515 K = KINIT,KLAST
000744 J1 = 1+(K-1)*NU
000750 IF (HSP(I,1) .NE. 0) GO TO 506
000752 I1 = INITR+(K-1)
000755 IP = I1+1
000756 GO TO 507
000758 506 IP = INITR +1
000760 K = KS(I)
000762 507 NRE(IP) = IMG
000764 G(IP) = YL(K,I)
000771 DO 510 J = 1,NU
000772 JP = J1+J
000774 H(IP,JP) = Y2(I,J)
001002 510 CONTINUE
001004 515 CONTINUE
001006 550 INTR = IP
001010 RETURN
001010 END

```


000003	COMMON/RHV/G(120),NRE(120)
000003	COMMON/PVAL/H(120,80)
000003	COMMON/ELS/C4(20,20)
000003	COMMON/ERG/R(20,20,4),I(20,20,4)
000003	COMMON/CSS/C1(20,20),C2(1,20,20),C(1,20,20)
000003	COMMON/FOFUN/F(1,20,3)
000003	COMMON/UPLD/YU(20,5),YL(20,5),Y(20)
000003	COMMON/CONST/Y1(5,20),Y2(5,4),Y3(5,4)
000003	COMMON/RMID/ISP,MSP(8,2)
000003	COMMON/INPT/II,N,M,NF,NU,KI,KJ,NDF,MODE
000003	COMMON/ALL/INITR,KS(8)
000003	COMMON/FORC/NSET5
000003	COMMON/RWS/NOBF,NOC,NOB,NOT
000003	CALL SEARCH(I,N,Y1,ISH,5,20)
000007	IF(ISH.EQ.0) GO TO 400
000011	CALL SEARCH(I,NU,Y2,ISH,5,4)
000015	IF(ISH.EQ.0) GO TO 300
000017	200 IF(MSP(I,1).NE.0) GO TO 205
000021	KINIT = 2
000022	KLAST = II-1
000024	GO TO 208
000024	205 KINIT = KS(1)
000026	KLAST = KS(1)
000030	IP=INITR+1
000032	DO 213 L=2, KINIT
000033	LL=KINIT-L+2
000036	CALL M12X3(LL,I,N,NU,Y1,R,C4)
000045	J1=1+(L-2)*NU
000052	J11=J1+1
000053	J2=J1+NU
000054	DO 214 J=J11,J2
000056	214 H(IP,J)=C4(I,J-J1)
000071	213 CONTINUE
000074	J3=J2+1
000076	J4=J2+NU
000100	DO 216 J=J3,J4
000102	216 H(IP,J)=Y2(I,J-J2)
000115	GO TO 227
000116	208 JL = NU+1
000120	IL = II-2
000122	DO 220 K = KINIT,KLAST
000124	CALL M12X3(K,I,N,NU,Y1,R,C4)
000133	IF(MSP(I,1).NE.0) GO TO 209
000136	IP = INITR + (K-1)
000141	GO TO 211
000141	209 IP = INITR + 1
000143	211 DO 210 J = 2,JL
000145	H(IP,J)=C4(I,J-1)
000153	H(IP,J+NU)=Y2(I,J-1)
000161	210 CONTINUE
000164	IF(MSP(I,1).NE.0) GO TO 220
000166	IF(K.LE.2) GO TO 220
000170	JF = K*NU+1
000174	JL1 = JL+1
000175	DO 215 J = JL1,JF
000176	H(IP,J) = H(IP-1,J-NU)

```

000206 215 CONTINUE
000210 220 CONTINUE
000213 227 DO 240 IS = 1, NSEIS
000215 DO 240 K = KINIT, KLAST
000217 JK = K*NU+1
000223 IF (MSP(I,1) .NE. 0) GO TO 221
000225 IP = INTR+(IS-1)*IL+K-1
000232 GO TO 222
000233 221 IP = INTR+(IS-1)+1
000236 K = KS(I)
000240 IL = 1
000241 222 G(IP) = 0.0
000243 DO 230 J = 1, NF
000244 G(IP) = G(IP) - Y3(I,J)*F(IS,K,J)
000255 230 CONTINUE
000257 DO 233 J = 1, N
000261 G(IP) = G(IP) - Y1(I,J)*C(IS,K,J)
000272 233 CONTINUE
000274 G(IP) = G(IP)+YU(K,I)
000302 IF (IS .EQ. 1) GO TO 240
000304 NRE(IP) = 1HE
000305 DO 235 J = 1, JK
000307 H(IP,J) = H(IP-IL,J)
000317 235 CONTINUE
000321 240 CONTINUE
000326 GO TO 550
000327 300 IF (MSP(I,1) .NE. 0) GO TO 305
000331 KINIT = 2
000332 KLAST = II
000333 GO TO 308
000334 305 KINIT = KS(I)
000336 KLAST = KS(I)
000340 IP=INTR+1
000342 DO 313 L=2, KINIT
000343 LL=KINIT-L+2
000346 CALL M12X3(LL,I,N,NU,Y1,R,C4)
000355 J1=1+(L-2)*NU
000362 J11=J1+1
000363 J2=J1+NU
000364 DO 314 J=J11,J2
000366 H(IP,J)=C4(I,J-J1)
000401 313 CONTINUE
000404 GO TO 332
000434 308 JL = NU+1
000406 IL = II-1
000410 DO 320 K = KINIT, KLAST
000412 CALL M12X3 (K,I,N,NU,Y1,R,C4)
000421 IF (MSP(I,1) .NE. 0) GO TO 309
000424 IP = INTR +K-1
000426 GO TO 311
000427 309 IP = INTR +1
000431 K = KS(I)
000433 DO 310 J = 2,JL
000435 H(IP,J) = C4(I,J-1)
000444 310 CONTINUE
000446 IF (MSP(I,1) .NE. 0) GO TO 320
000450 IF (K .LE. 2) GO TO 320
000452 JF = (K-1)*NU+1

```

```

000470 H(1P,J) = H(1P-1,J-NU)
000471 315 CONTINUE
000472 320 CONTINUE
000473 332 DO 335 IS = 1,NSETS
000474 DO 335 K = KINIT ,KLAST
000475 JK = (K-1)*NU+1
000501 IF (HSP(I,1) .NE. 0) GO TO 321
000505 IP = INITR*(IS-1)*IL+K-1
000507 GO TO 322
000514 321 IP = INITR*(IS-1)+1
000515 322 K = KS(I)
000520 IL = 1
000522 322 G(IP) = 0.0
000523 DO 325 J = 1,NF
000525 G(IP) = G(IP) - Y3(I,J)*F(IS,K,J)
000526 325 CONTINUE
000537 DO 328 J = 1,N
000541 G(IP) = G(IP) - Y1(I,J)*G(IS,K,J)
000543 328 CONTINUE
000554 G(IP) = G(IP)+YU(K,I)
000556 NRE(IP) = 1HE
000564 IF (IS .EQ. 1) GO TO 335
000565 DO 330 J = 1,JK
000567 H(IP,J) = H(IP-IL,J)
000571 330 CONTINUE
000601 335 CONTINUE
000603 GO TO 550
000610 400 CALL SEARCH (I,NF,Y3,ISH,5,4)
000611 IF (ISH .EQ. 0) GO TO 500
000615 IF (HSP(I,1) .NE. 0) GO TO 405
000617 KINIT = 1
000621 KLAST = II-1
000622 GO TO 408
000624 405 KINIT = KS(I)
000626 KLAST = KS(I)
000630 408 IL = II-1
000632 DO 420 IS = 1,NSETS
000634 DO 420 K = KINIT,KLAST
000636 IF (HSP(I,1) .NE. 0) GO TO 409
000640 IP = (IS-1)*(II-1)+(K-1)+1+INITR
000647 GO TO 411
000650 409 IP = INITR*(IS-1)+1
000653 K = KS(I)
000655 411 NRE(IP) = 1HE
000657 G(IP) = 0.0
000660 DO 410 L = 1,NF
000662 410 G(IP) = G(IP)-Y3(I,L)*F(IS,K,L)
000675 G(IP) = G(IP)+YU(K,I)
000703 J1 = 1+(K-1)*NU
000706 DO 415 J = 1,NU
000710 JP = J1+J
000712 H(IP,JP) = Y2(I,J)
000720 415 CONTINUE
000722 420 CONTINUE
000727 GO TO 550
000727 500 IF (HSP(I,1) .NE. 0) GO TO 505

```

```

000731 KINIT = 1
000732 KLAST = II-1
000733 GO TO 508
000734 505 KINIT = KS(I)
000735 KLAST = KS(I)
000736
000740 508 IL = II-1
000742 00 515 K = KINIT,KLAST
000744 J1 = 1+(K-1)*NU
000750 IF (HSP(I,1).NE. 0) GO TO 506
000752 I1 = INITR+(K-1)
000755 IP = I1+1
000756 GO TO 507
000756 506 IP = INITR +1
000760 K = KS(I)
000762 507 NRE(IP) = 1HE
000764 G(IP) = YU(K,I)
000771 00 510 J = 1,NU
000772 JP = J1+J
000774 H(IP,JP) = Y2(I,J)
001002 510 CONTINUE
001004 515 CONTINUE
001006 550 INITR = IP
001010 RETURN
001010 END

```

```
000011 DIMENSION A(NI,NJ)
000011 DO 500 J = 1,NX
000012 IF (A(IX,J)) 510,500,510
000016 500 CONTINUE
000021 ISH = 0
000021 RETURN
000022 510 ISH = 1
000023 RETURN
000024 END
```

```

SUBROUTINE M12X3 ( KI,IX,K,M,A,B,C)
DIMENSION A(5,20),B(20,20,4),C(20,20)
KJ = KI-1
DO 400 J = 1,M
C(IX,J) = 0.0
DO 400 L = 1,K
C(IX,J) = C(IX,J)+A(IX,L)*B(KJ,L,J)
400 CONTINUE
RETURN
END

```

```

000004 DIMENSION M(100,100),S(100,100),C(100,100)
000011 DO 200 I = 1,N
000012 DO 200 J = 1,M
000013 C(I,J) = 0.0
000016 DO 200 L = 1,K
000020 200 C(I,J) = C(I,J) + A(I,L) * B(L,J)
000043 RETURN
000043 END

```

```

SUBROUTINE MEXAP
COMMON/XXAP/AEI(20,20),P(20,20)
COMMON/ABD/A(20,20),B(20,4),D(20,4)
COMMON/INPT/II,N,MQ,NF,NU,KI,KJ,NOF,MODE,IZ
COMMON/T/IM
DIMENSION X(20,20),XT(20,20),Y(20,20),YT(20,20)
CC0002 DIMENSION U(6),V(4),M(4)
CC0002 T=IM
CC0004 Q=0.28999933
CC0005 U(1)=0.2499986842
CC0007 U(2)=0.0312575832
CC0010 U(3)=0.0025913712
CC0012 U(4)=0.0001715620
CC0013 U(5)=0.000054302
CC0015 U(6)=0.000006906
CC0016 V(1)=-2.21781431
CC0020 V(2)=3.33131912
CC0021 V(3)=-1.62781495
CC0023 V(4)=0.51431014
CC0024 W(1)=0.28905386
CC0026 W(2)=-0.33240494
CC0027 W(3)=0.45548498
CC0031 W(4)=0.58785666
CC0032 DO 1 I=1,N
CC0034 DO 1 J=1,N
CC0035 X(I,J)=0.0
CC0041 1 CONTINUE
CC0045 DO 20 I=1,N
CC0047 DO 10 J=1,N
CC0050 P(I,J)=0.0
CC0053 Y(I,J)=0.0
CC0056 X(I,J)=T*A(I,J)
CC0064 10 CONTINUE
CC0066 P(I,I)=1.0
CC0072 Y(I,I)=1.0
CC0075 20 CONTINUE
CC0077 DO 60 M=1,6
CC0100 DO 40 I=1,N
CC0101 DO 40 J=1,N
CC0102 XT(I,J)=0.0
CC0105 DO 30 L=1,N
CC0107 XT(I,J)=XT(I,J)+X(I,L)*Y(L,J)
CC0121 30 CONTINUE
CC0123 P(I,J)= P(I,J)+XT(I,J)*U(M)
CC0131 40 CONTINUE
CC0136 DO 50 I=1,N
CC0137 DO 50 J=1,N
CC0140 Y(I,J)=YT(I,J)
CC0147 50 CONTINUE
CC0153 60 CONTINUE
CC0155 DO 70 I=1,N
CC0157 DO 70 J=1,N
CC0160 XT(I,J)=0.0
CC0163 DO 70 L=1,N
CC0165 XT(I,J)=XT(I,J)+ P(I,L)*P(L,J)
CC0177 70 CONTINUE
CC0205 DO 80 I=1,N

```



```

000213 00 80 L=1,N
000215 Y(I,J)=Y(I,J)+X(I,L)*XT(L,J)
000227 80 CONTINUE
000235 CALL MIV(Y,N,P,20)
000240 DO 110 I=1,N
000242 DO 90 J=1,N
000243 XT(I,J)=Q*X(I,J)
000253 90 CONTINUE
000255 XT(I,I)=1.0+XT(I,I)
000261 110 CONTINUE
000263 CALL MIV(XT,N,X,20)
000266 DO 130 I=1,N
000270 DO 120 J=1,N
000271 YT(I,J)=0.0
000274 Y(I,J)=0.0
000277 AEI(I,J)=0.0
000302 120 CONTINUE
000304 AEI(I,I)=1.0
000310 Y(I,I)=1.0
000313 130 CONTINUE
000315 DO 170 M=1,4
000316 DO 150 I=1,N
000317 DO 150 J=1,N
000320 XT(I,J)=0.0
000323 DO 140 L=1,N
000325 XT(I,J)=XT(I,J)+X(I,L)*Y(L,J)
000337 140 CONTINUE
000341 AEI(I,J)=AEI(I,J)+XT(I,J)*V(M)
000347 YT(I,J)=YT(I,J)+XT(I,J)*H(M)
000355 150 CONTINUE
000362 DO 160 I=1,N
000363 DO 160 J=1,N
000364 Y(I,J)=XT(I,J)
000373 160 CONTINUE
000377 170 CONTINUE
000401 CALL MIV(AEI,N,XT,20)
000404 DO 190 I=1,N
000406 DO 190 J=1,N
000407 AEI(I,J)=0.0
000412 DO 180 L=1,N
000414 AEI(I,J)=AEI(I,J)+XT(I,L)*YT(L,J)
000426 180 CONTINUE
000430 AEI(I,J)=T*AEI(I,J)
000434 190 CONTINUE
000440 RETURN
000440 END

```

```

SUBROUTINE MIV(EM,N,EMI,N1)
  DIMENSION EM(N1,N1),EMI(N1,N1)
  DO 10 I = 1,N
    DO 10 J = 1,N
      10 EMI(I,J) = EM(I,J)
      DO 1 I = 1,N
        X = EMI(I,I)
        EMI(I,I) = 1.0
        DO 2 J = 1,N
          2 EMI(I,J) = EMI(I,J)/X
          DO 1 K = 1,N
            IF (K.EQ.I) GO TO 1
            X = EMI(K,I)
            EMI(K,I) = 0.0
            DO 4 J = 1,N
              4 EMI(K,J) = EMI(K,J) - X * EMI(I,J)
            1 CONTINUE
          RETURN
        END
      END
    END
  END

```

B. Program PSTPROC

COMMON /YSS/ Y(20)
COMMON /ALL/ INTR
COMMON /INPT/ II,N,NF,NU,NDF,NSETS,NOT
COMMON /CSS/ C1(50,20),C2(50,20),C3(50,20)
COMMON /BRG/ R(50,20,4)
COMMON /FOFON/ F(1,50,4)
COMMON /TAB/ Q1(20,20),Q2(20,4),Q3(20,4),ISET(20)
DIMENSION U(50,8)
DIMENSION Z(8),TB(50),PHI(21),ITR(8)
402 FORMAT(6X,5HWHERE/)
401 FORMAT(3X,21H,IB= 01*S+ 02*U+ 03*F/)
403 FORMAT(8X,3HQ1=,20F6.2)
404 FORMAT(8X,3HQ2=,20F6.2)
405 FORMAT(8X,3HQ3=,20F6.2)
406 FORMAT(/,40X,13HTIME INTERVAL,12X,2HTB/)
400 FORMAT(37X,F7.3,4H TO ,F7.3, 6X,F12.6)
1000 FORMAT(44X,F18.8)
25 FORMAT (F12.6)
30 FORMAT(6E12.6)
31 FORMAT(14I5)
32 FORMAT(10I5,F10.6)
IPB=0
READ(5,304) NPB
304 FORMAT (I2)
303 READ (5,32) II,N,NF,NU,NDF,NSETS,NOT,I2,IID,KSMI,IM
IPB=IPB+1
IU=II-1
I1=II-1
INM1=(+3HSOL)
INM2=(+3HEND)
DO 20 I = 1,NOT
20 READ (5,30) (Q1(I,J),J = 1,N)
DO 40 I = 1,NOT
40 READ(5,30) (Q2(I,J) ,J=1,NU)
DO 50 I = 1,NOT
50 READ (5,30) (Q3(I,J),J= 1,NF)
READ (5,30) (Y(I),I = 1,I2)
DO 80 K = 1,I1
DO 80 I = 1,N
80 READ (5,30) (R(K,I,J),J = 1,NU)
DO 90 IS = 1,NSETS
DO 90 K = 1,I1
90 READ (5,30) (F(IS,K,I) ,I = 1,NF)
DO 100 IS = 1,NSETS
DO 100 K = 2,I1
100 READ (5,30) (C(IS,K,I),I = 1,N)
READ (5,31) (ISET(I),I = 1,NOT)
READ (5,31) (ITR(I),I = 1,NOT)
XX=2.0
I3=0
IDF=100
IOL=0
1001 READ(5,191)NAME
191 FORMAT(A3)
IF(NAME.EQ.INM1)GO TO 111

```

000003 COMMON TM
001003 COMMON/YSS/ Y(20)
002003 COMMON/ALL/ INTR
003003 COMMON /INPT/ II,N,NF,NU,NDF,NSETS,NOT
004003 COMMON /CSS/ C1(50,20),C2(50,20),C3(50,20)
005003 COMMON /BRG/ R(50,20,4)
006003 COMMON /FOFON/ F(1,50,4)
007003 COMMON /TAB/ Q1(20,20),Q2(20,4),Q3(20,4),ISET(20)
008003 DIMENSION U(50,8)
009003 DIMENSION Z(8),TB(50),PHI(21),ITR(8)
010003 402 FORMAT(6X,5HWHERE/)
011003 401 FORMAT(3X,21H,IB= 01*S+ 02*U+ 03*F/)
012003 403 FORMAT(8X,3HQ1=,20F6.2)
013003 404 FORMAT(8X,3HQ2=,20F6.2)
014003 405 FORMAT(8X,3HQ3=,20F6.2)
015003 406 FORMAT(/,40X,13HTIME INTERVAL,12X,2HTB/)
016003 400 FORMAT(37X,F7.3,4H TO ,F7.3, 6X,F12.6)
017003 1000 FORMAT(44X,F18.8)
018003 25 FORMAT (F12.6)
019003 30 FORMAT(6E12.6)
020003 31 FORMAT(14I5)
021003 32 FORMAT(10I5,F10.6)
022003 IPB=0
023003 READ(5,304) NPB
024003 304 FORMAT (I2)
025003 303 READ (5,32) II,N,NF,NU,NDF,NSETS,NOT,I2,IID,KSMI,IM
026003 IPB=IPB+1
027003 IU=II-1
028003 I1=II-1
029003 INM1=(+3HSOL)
030003 INM2=(+3HEND)
031003 DO 20 I = 1,NOT
032003 20 READ (5,30) (Q1(I,J),J = 1,N)
033003 DO 40 I = 1,NOT
034003 40 READ(5,30) (Q2(I,J) ,J=1,NU)
035003 DO 50 I = 1,NOT
036003 50 READ (5,30) (Q3(I,J),J= 1,NF)
037003 READ (5,30) (Y(I),I = 1,I2)
038003 DO 80 K = 1,I1
039003 DO 80 I = 1,N
040003 80 READ (5,30) (R(K,I,J),J = 1,NU)
041003 DO 90 IS = 1,NSETS
042003 DO 90 K = 1,I1
043003 90 READ (5,30) (F(IS,K,I) ,I = 1,NF)
044003 DO 100 IS = 1,NSETS
045003 DO 100 K = 2,I1
046003 100 READ (5,30) (C(IS,K,I),I = 1,N)
047003 READ (5,31) (ISET(I),I = 1,NOT)
048003 READ (5,31) (ITR(I),I = 1,NOT)
049003 XX=2.0
050003 I3=0
051003 IDF=100
052003 IOL=0
053003 1001 READ(5,191)NAME
054003 191 FORMAT(A3)
055003 IF(NAME.EQ.INM1)GO TO 111

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```

000311 IF (NAME.EQ.INH2)GO TO 450
000313 111 DO 110 K=1,II1
000315 DO 110 J=1,NU
000316 110 U(K,J)=0.0
000317 WRITE (6,123)
000322 123 FORMAT (2X,11WHERE IS 110)
000332 READ(5,1000)T
000340 PHI(I3)=T
000342 DO 4000 I=1,IU
000344 DO 4000 J=1,NU
000345 READ(5,1000)T
000352 U(I,J)=T
000357 4000 CONTINUE
000363 WRITE (6,321)
000367 321 FORMAT (2X,12WHERE IS 1100)
000367 1100 DO 420 I=1,NOT
000371 WRITE (6,120)
000374 120 FORMAT (1H1)
000374 X1 = 0
000375 X2 = 0
000376 X3 = 0
000377 X4 = 0
000400 IS = ISET(I)
000402 CALL SEARCH (I,N,Q1,IQ1)
000405 CALL SEARCH (I,NU,Q2,IQ2)
000410 IF (IQ1 .EQ. 0) GO TO 275
000411 200 IF (IQ2 .EQ.0) GO TO 250
000412 KINIT = 2
000413 KLAST = II-1
000415 GO TO 300
000416 250 KINIT = 2
000417 KLAST = II
000421 GO TO 300
000421 275 KINIT = 1
000422 KLAST = II-1
000424 300 WRITE(6,401)
000430 WRITE(6,402)
000434 WRITE(6,403)(Q1(I,J),J=1,N)
000451 WRITE(6,404)(Q2(I,J),J=1,NU)
000466 WRITE(6,405)(Q3(I,J),J=1,NF)
000503 WRITE(6,406)
000507 DO 410 K = KINIT,KLAST
000511 IF (IQ1 .EQ. 0) GO TO 325
000512 X1 = 0
000513 DO 310 J = 1,N
000514 X1 = Q1(I,J) *C(IS,K,J) *X1
000525 310 CONTINUE
000527 K1 = K-1
000531 DO 320 J = 1,N
000533 Z(J) = 0.0
000534 DO 320 L = 1,K1
000536 DO 320 LL = 1,NU
000537 Z(J) = Z(J) +R(K-L,J,LL)*U(L,LL)
000554 320 CONTINUE
000563 X2 = 0
000564 DO 330 J = 1,N
000565 X2 = Q1(I,J)*Z(J)+X2
000573 330 CONTINUE

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000576 X3 = 0
000577 DO 340 J = 1,NU
000581 X3 = X3 + Q2(I,J) * U(K,J)
000583 340 CONTINUE
000585 X4 = 0
000586 DO 360 J = 1,NF
000590 X4 = X4 + Q3(I,J) * F(IS,K,J)
000592 360 CONTINUE
000594 TB(K) = X1 * X2 + X3 * X4
000596 FK = K
000598 TK1 = (FK - 1.0) * TM
000600 TK2 = TK1 + TM
000602 WRITE (6,400) TK1,TK2,IB(K)
000604 400 CONTINUE
000606 IF (ITR(I) .EQ. 0) GO TO 420
000608 CALL TRAJ (KINIT,KLAST,TB)
000610 420 CONTINUE
000612 C
000614 GO TO 1001
000616 450 IF (ITD .EQ. 0) GO TO 999
000618 WRITE (6,453)
000620 453 FORMAT (1H1)
000622 DO 455 I = 1,IZ
000624 455 WRITE (6,460) PHI(I),Y(I)
000626 460 FORMAT(1X,20HOBJECTIVE FUNCTION =,F12.6,5X,7HBOUND =,F12.6)
000628 CALL TRADE(PHI,Y,IZ,KSWT)
000630 999 IF (IPB .LI. NPB) GO TO 303
000632 STOP
000634 END
000636

```

SUBROUTINE TRADE (X,Y,NOC,KSHT)
 DIMENSION A(50),B(50),X(50),Y(50),SCL(50)

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000007 WRITE (6,10)
000012 10 FORMAT (1H1,14HTRADE OFF PLOT/11X,18HOBJECTIVE FUNCTION)
000012 DO 20 J = 1,NOC
000016 B(J) = X(J)
000020 20 A(J) = Y(J)
000024 DO 68 J = 1,NOC
000026 K = NOC-J
000027 DO 68 I = 1,K
000031 IF (A(I) - A(I+1)) 40,40,30
000034 30 TEMP = A(I)
000036 A(I) = A(I+1)
000040 A(I+1) = TEMP
000042 40 IF (B(I) - B(I+1)) 60,60,50
000046 50 TEMP = B(I)
000050 B(I) = B(I+1)
000052 B(I+1) = TEMP
000054 60 IF (X(I) - X(I+1)) 65,60,68
000060 65 TEMP = X(I)
000062 X(I) = X(I+1)
000065 X(I+1) = TEMP
000066 TEMP = Y(I)
000070 Y(I) = Y(I+1)
000072 Y(I+1) = TEMP
000074 68 CONTINUE
000101 XMAXO = B(NOC)
000102 XMAXC = A(NOC)
000103 IF (KSHT.EQ. 0) GO TO 80
000105 XMINO = B(1)
000106 XMINC = A(1)
000107 XMINO = INT(XMINO)
000111 XMINC = INT(XMINC)
000113 GO TO 82
000114 80 XMINO = 0.
000115 XMINC = 0.
000116 82 RNGO = XMAXO-XMINO
000120 RNGC = XMAXC-XMINC
000122 IF (RNGO.LT. 7.) GO TO 84
000125 XINTO = INT(RNGO/8.+9)
000133 XMAXO = XINTO*8.+ XMINO+1.0
000134 GO TO 86
000135 84 XINTO = RNGO/8.
000137 XMAXO = XINTO*8.+XMINO
000142 86 IF (RNGC.LT. 7.) GO TO 88
000145 XINTC = INT (RNGC/8.+9)
000150 XMAXC = XINTC*8.+ XMINC
000153 GO TO 90
000154 88 XINTC = RNGC/8.
000156 XMAXC = XINTC*8.+XMINC
000161 90 XINT6 = XINTO/6.
000163 100 K3 = 0
000164 J = 1
000165 SC = 0.
000166 DO 698 K = 1,48
000170 AK = K
000171 XMAXU = XMAXO-(XINT6*(AK-1.))

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000175 XMAXL = XMAXO-(XINT6*AK)
000200 IF (J.GT. NOD) GO TO 140
000203 IF (X(J).LE. XMAXU .AND. X(J).GT. XMAXL) GO TO 110
000215 GO TO 140
000215 110 DO 460 L = 1,9
000217 AL = L
000220 XMIN1 = XMINC +(XINTC*(AL-1.))
000224 XMIN2 = XMINC +(XINTC*AL)
000227 IF (Y(J).GE. XMIN1 .AND. Y(J).LT. XMIN2) GO TO 120
000241 GO TO 460
000241 120 XINT10 = XINIC/10.
000243 130 DO 450 LI = 1,10
000245 AL1 = LI
000246 XMIN4 = XMIN1 +(XINT10*(AL1-1.))
000252 XMIN5 = XMIN1+(XINT10*AL1)
000255 IF (Y(J).GE. XMIN4 .AND. Y(J).LT. XMIN5) GO TO 190
000267 GO TO 450
000267 140 K3 = K3+1
000271 IF (K3-6) 160,160,150
000273 150 K3 = 1
000274 160 IF (K3-1) 180,170,180
000276 170 SC = SC+1.
000300 XMAX2 = XMAXO-(XINTO*(SC-1.))
000304 WRITE (6,175) XMAX2
000311 175 FORMAT (10X,F10.3,1H*)
000311 GO TO 698
000314 180 WRITE (6,185)
000320 185 FORMAT (20X,1H*)
000320 GO TO 698
000323 190 K3 = K3+1
000325 IF (K3-6) 195,195,193
000327 193 K3 = 1
000330 195 IF (K3-1) 200,210,200
000332 200 GO TO (401,402,403,404,405,406,407,408,580),L
000347 210 SC = SC+1
000351 XMAX2 = XMAXO-(XINTO*(SC-1.))
000355 GO TO ( 421,422,423,424,425,426,427,428,680),L
000372 401 GO TO (503,501,502,503,504,505,506,507,508,509),L1
000410 402 GO TO (513,511,512,513,514,515,516,517,518,519),L1
000426 403 GO TO (520,521,522,523,524,525,526,527,528,529),L1
000444 404 GO TO (530,531,532,533,534,535,536,537,538,539),L1
000462 405 GO TO (540,541,542,543,544,545,546,547,548,549),L1
000500 406 GO TO (550,551,552,553,554,555,556,557,558,559),L1
000516 407 GO TO (560,561,562,563,564,565,566,567,568,569),L1
000534 408 GO TO (570,571,572,573,574,575,576,577,578,579),L1
000552 421 GO TO (600,601,602,603,604,605,606,607,608,609),L1
000570 422 GO TO (610,611,612,613,614,615,616,617,618,619),L1
000606 423 GO TO (620,621,622,623,624,625,626,627,628,629),L1
000624 424 GO TO (630,631,632,633,634,635,636,637,638,639),L1
000642 425 GO TO (640,641,642,643,644,645,646,647,648,649),L1
000660 426 GO TO (650,651,652,653,654,655,656,657,658,659),L1
000676 427 GO TO (660,661,662,663,664,665,666,667,668,669),L1
000714 428 GO TO (670,671,672,673,674,675,676,677,678,679),L1
000732 450 CONTINUE
000734 460 CONTINUE
000736 500 WRITE (6,700)
000742 700 FORMAT (20X,1H*)
000742 GO TO 692

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000745	501 WRITE (6,701)
000751	701 FORMAT (20X,1H\$, 1H\$)
000751	GO TO 692
000754	502 WRITE (6,702)
000760	702 FORMAT (20X,1H\$, 1X,1H\$)
000760	GO TO 692
000763	503 WRITE (6,703)
000767	703 FORMAT (20X,1H\$, 2X,1H\$)
000767	GO TO 692
000772	504 WRITE (6,704)
000776	704 FORMAT (20X,1H\$, 3X,1H\$)
000776	GO TO 692
001001	505 WRITE (6,705)
001005	705 FORMAT (20X,1H\$, 4X,1H\$)
001005	GO TO 692
001010	506 WRITE (6,706)
001014	706 FORMAT (20X,1H\$, 5X,1H\$)
001014	GO TO 692
001017	507 WRITE (6,707)
001023	707 FORMAT (20X,1H\$, 6X,1H\$)
001023	GO TO 692
001026	508 WRITE (6,708)
001032	708 FORMAT (20X,1H\$, 7X,1H\$)
001032	GO TO 692
001035	509 WRITE (6,709)
001041	709 FORMAT (20X,1H\$, 8X,1H\$)
001041	GO TO 692
001044	510 WRITE (6,710)
001050	710 FORMAT (20X,1H\$, 9X,1H\$)
001050	GO TO 692
001053	511 WRITE (6,711)
001057	711 FORMAT (20X,1H\$, 10X,1H\$)
001057	GO TO 692
001062	512 WRITE (6,712)
001066	712 FORMAT (20X,1H\$, 11X,1H\$)
001066	GO TO 692
001071	513 WRITE (6,713)
001075	713 FORMAT (20X,1H\$, 12X,1H\$)
001075	GO TO 692
001100	514 WRITE (6,714)
001104	714 FORMAT (20X,1H\$, 13X,1H\$)
001104	GO TO 692
001107	515 WRITE (6,715)
001113	715 FORMAT (20X,1H\$, 14X,1H\$)
001113	GO TO 692
001116	516 WRITE (6,716)
001122	716 FORMAT (20X,1H\$, 15X,1H\$)
001122	GO TO 692
001125	517 WRITE (6,717)
001131	717 FORMAT (20X,1H\$, 16X,1H\$)
001131	GO TO 692
001134	518 WRITE (6,718)
001140	718 FORMAT (20X,1H\$, 17X,1H\$)
001140	GO TO 692
001143	519 WRITE (6,719)
001147	719 FORMAT (20X,1H\$, 18X,1H\$)
001147	GO TO 692
001152	520 WRITE (6,720)

001156	GO TO 692	521 WRITE (6,721)
001161	721 FORMAT (20X,1MS,20X,1MS)	
001165	GO TO 692	522 WRITE (6,722)
001170	722 FORMAT (20X,1MS,21X,1MS)	
001174	GO TO 692	523 WRITE (6,723)
001177	723 FORMAT (20X,1MS,22X,1MS)	
001203	GO TO 692	524 WRITE (6,724)
001206	724 FORMAT (20X,1MS,23X,1MS)	
001212	GO TO 692	525 WRITE (6,725)
001215	725 FORMAT (20X,1MS,24X,1MS)	
001221	GO TO 692	526 WRITE (6,726)
001224	726 FORMAT (20X,1MS,25X,1MS)	
001230	GO TO 692	527 WRITE (6,727)
001233	727 FORMAT (20X,1MS,26X,1MS)	
001237	GO TO 692	528 WRITE (6,728)
001242	728 FORMAT (20X,1MS,27X,1MS)	
001246	GO TO 692	529 WRITE (6,729)
001251	729 FORMAT (20X,1MS,28X,1MS)	
001255	GO TO 692	530 WRITE (6,730)
001260	730 FORMAT (20X,1MS,29X,1MS)	
001264	GO TO 692	531 WRITE (6,731)
001267	731 FORMAT (20X,1MS,30X,1MS)	
001273	GO TO 692	532 WRITE (6,732)
001276	732 FORMAT (20X,1MS,31X,1MS)	
001302	GO TO 692	533 WRITE (6,733)
001305	733 FORMAT (20X,1MS,32X,1MS)	
001311	GO TO 692	534 WRITE (6,734)
001314	734 FORMAT (20X,1MS,33X,1MS)	
001320	GO TO 692	535 WRITE (6,735)
001323	735 FORMAT (20X,1MS,34X,1MS)	
001327	GO TO 692	536 WRITE (6,736)
001332	736 FORMAT (20X,1MS,35X,1MS)	
001336	GO TO 692	537 WRITE (6,737)
001341	737 FORMAT (20X,1MS,36X,1MS)	
001345	GO TO 692	538 WRITE (6,738)
001350	738 FORMAT (20X,1MS,37X,1MS)	
001354	GO TO 692	539 WRITE (6,739)
001357	739 FORMAT (20X,1MS,38X,1MS)	
001363		

001363	GO TO 692
001366	540 WRITE (6,740)
001372	740 FORMAT (20X,1HS,39X,1H*)
001372	GO TO 692
001375	541 WRITE (6,741)
001401	741 FORMAT (20X,1HS,40X,1H*)
001401	GO TO 692
001404	542 WRITE (6,742)
001410	742 FORMAT (20X,1HS,41X,1H*)
001410	GO TO 692
001413	543 WRITE (6,743)
001417	743 FORMAT (20X,1HS,42X,1H*)
001417	GO TO 692
001422	544 WRITE (6,744)
001426	744 FORMAT (20X,1HS,43X,1H*)
001426	GO TO 692
001431	545 WRITE (6,745)
001435	745 FORMAT (20X,1HS,44X,1H*)
001435	GO TO 692
001440	546 WRITE (6,746)
001444	746 FORMAT (20X,1HS,45X,1H*)
001444	GO TO 692
001447	547 WRITE (6,747)
001453	747 FORMAT (20X,1HS,46X,1H*)
001453	GO TO 692
001456	548 WRITE (6,748)
001462	748 FORMAT (20X,1HS,47X,1H*)
001462	GO TO 692
001465	549 WRITE (6,749)
001471	749 FORMAT (20X,1HS,48X,1H*)
001471	GO TO 692
001474	550 WRITE (6,750)
001500	750 FORMAT (20X,1HS,49X,1H*)
001500	GO TO 692
001503	551 WRITE (6,751)
001507	751 FORMAT (20X,1HS,50X,1H*)
001507	GO TO 692
001512	552 WRITE (6,752)
001516	752 FORMAT (20X,1HS,51X,1H*)
001516	GO TO 692
001521	553 WRITE (6,753)
001525	753 FORMAT (20X,1HS,52X,1H*)
001525	GO TO 692
001530	554 WRITE (6,754)
001534	754 FORMAT (20X,1HS,53X,1H*)
001534	GO TO 692
001537	555 WRITE (6,755)
001543	755 FORMAT (20X,1HS,54X,1H*)
001543	GO TO 692
001546	556 WRITE (6,756)
001552	756 FORMAT (20X,1HS,55X,1H*)
001552	GO TO 692
001555	557 WRITE (6,757)
001561	757 FORMAT (20X,1HS,56X,1H*)
001561	GO TO 692
001564	558 WRITE (6,758)
001570	758 FORMAT (20X,1HS,57X,1H*)
001570	GO TO 692

001577	759	FORMAT (20X,1HS,58X,1H*)
001578		GO TO 692
001602	560	WRITE (6,760)
001606	760	FORMAT (20X,1HS,59X,1H*)
001611		GO TO 692
001615	561	WRITE (6,761)
001620	761	FORMAT (20X,1HS,60X,1H*)
001624		GO TO 692
001627	562	WRITE (6,762)
001633	762	FORMAT (20X,1HS,61X,1H*)
001636		GO TO 692
001642	564	WRITE (6,764)
001645	764	FORMAT (20X,1HS,63X,1H*)
001651		GO TO 692
001654	565	WRITE (6,765)
001660	765	FORMAT (20X,1HS,64X,1H*)
001663		GO TO 692
001667	566	WRITE (6,766)
001672	766	FORMAT (20X,1HS,65X,1H*)
001676		GO TO 692
001701	569	WRITE (6,769)
001705	769	FORMAT (20X,1HS,68X,1H*)
001710		GO TO 692
001714	570	WRITE (6,770)
001717	770	FORMAT (20X,1HS,69X,1H*)
001723		GO TO 692
001726	571	WRITE (6,771)
001732	771	FORMAT (20X,1HS,70X,1H*)
001735		GO TO 692
001741	572	WRITE (6,772)
001744	772	FORMAT (20X,1HS,71X,1H*)
001750		GO TO 692
001753	573	WRITE (6,773)
001757	773	FORMAT (20X,1HS,72X,1H*)
001762		GO TO 692
001766	574	WRITE (6,774)
001771	774	FORMAT (20X,1HS,73X,1H*)
001775		GO TO 692
002000	575	WRITE (6,775)
	775	FORMAT (20X,1HS,74X,1H*)
		GO TO 692
	576	WRITE (6,776)
	776	FORMAT (20X,1HS,75X,1H*)
		GO TO 692
	577	WRITE (6,777)
	777	FORMAT (20X,1HS,76X,1H*)
		GO TO 692
	578	WRITE (6,778)

002004	770	FORMAT (20X,1MS,77X,1H*)
002004	GO TO 692	
002007	579	WRITE (6,779)
002013	779	FORMAT (20X,1MS,78X,1H*)
002013	GO TO 692	
002016	580	WRITE (6,780)
002022	780	FORMAT (20X,1MS,79X,1H*)
002022	GO TO 692	
002025	600	WRITE (6,800) XMAX2
002033	800	FORMAT (10X,F10.3,1H*)
002033	GO TO 692	
002036	601	WRITE (6,801) XMAX2
002044	801	FORMAT (10X,F10.3,1H*, 1H*)
002044	GO TO 692	
002047	602	WRITE (6,802) XMAX2
002055	802	FORMAT (10X,F10.3,1H*, 1X,1H*)
002055	GO TO 692	
002060	603	WRITE (6,803) XMAX2
002066	803	FORMAT (10X,F10.3,1H*, 2X,1H*)
002066	GO TO 692	
002071	604	WRITE (6,804) XMAX2
002077	804	FORMAT (10X,F10.3,1H*, 3X,1H*)
002077	GO TO 692	
002102	605	WRITE (6,805) XMAX2
002110	805	FORMAT (10X,F10.3,1H*, 4X,1H*)
002110	GO TO 692	
002113	606	WRITE (6,806) XMAX2
002121	806	FORMAT (10X,F10.3,1H*, 5X,1H*)
002121	GO TO 692	
002124	607	WRITE (6,807) XMAX2
002132	807	FORMAT (10X,F10.3,1H*, 6X,1H*)
002132	GO TO 692	
002135	608	WRITE (6,808) XMAX2
002143	808	FORMAT (10X,F10.3,1H*, 7X,1H*)
002143	GO TO 692	
002146	609	WRITE (6,809) XMAX2
002154	809	FORMAT (10X,F10.3,1H*, 8X,1H*)
002154	GO TO 692	
002157	610	WRITE (6,810) XMAX2
002165	810	FORMAT (10X,F10.3,1H*, 9X,1H*)
002165	GO TO 692	
002170	611	WRITE (6,811) XMAX2
002176	811	FORMAT (10X,F10.3,1H*,10X,1H*)
002176	GO TO 692	
002201	612	WRITE (6,812) XMAX2
002207	812	FORMAT (10X,F10.3,1H*,11X,1H*)
002207	GO TO 692	
002212	613	WRITE (6,813) XMAX2
002220	813	FORMAT (10X,F10.3,1H*,12X,1H*)
002220	GO TO 692	
002223	614	WRITE (6,814) XMAX2
002231	814	FORMAT (10X,F10.3,1H*,13X,1H*)
002231	GO TO 692	
002234	615	WRITE (6,815) XMAX2
002242	815	FORMAT (10X,F10.3,1H*,14X,1H*)
002242	GO TO 692	
002245	616	WRITE (6,816) XMAX2
002253	816	FORMAT (10X,F10.3,1H*,15X,1H*)
002253	GO TO 692	

002264	817	FORMAT (10X,F10.3,1H,16X,1H*)
002264		GO TO 692
002267	618	WRITE (6,818) XMAX2
002275	818	FORMAT (10X,F10.3,1H,17X,1H*)
002275		GO TO 692
002300	619	WRITE (6,819) XMAX2
002306	819	FORMAT (10X,F10.3,1H,18X,1H*)
002306		GO TO 692
002311	620	WRITE (6,820) XMAX2
002317	820	FORMAT (10X,F10.3,1H,19X,1H*)
002317		GO TO 692
002322	621	WRITE (6,821) XMAX2
002330	821	FORMAT (10X,F10.3,1H,20X,1H*)
002330		GO TO 692
002333	622	WRITE (6,822) XMAX2
002341	822	FORMAT (10X,F10.3,1H,21X,1H*)
002341		GO TO 692
002344	623	WRITE (6,823) XMAX2
002352	823	FORMAT (10X,F10.3,1H,22X,1H*)
002352		GO TO 692
002355	624	WRITE (6,824) XMAX2
002363	824	FORMAT (10X,F10.3,1H,23X,1H*)
002363		GO TO 692
002366	625	WRITE (6,825) XMAX2
002374	825	FORMAT (10X,F10.3,1H,24X,1H*)
002374		GO TO 692
002377	626	WRITE (6,826) XMAX2
002405	826	FORMAT (10X,F10.3,1H,25X,1H*)
002405		GO TO 692
002410	627	WRITE (6,827) XMAX2
002416	827	FORMAT (10X,F10.3,1H,26X,1H*)
002416		GO TO 692
002421	628	WRITE (6,828) XMAX2
002427	828	FORMAT (10X,F10.3,1H,27X,1H*)
002427		GO TO 692
002432	629	WRITE (6,829) XMAX2
002440	829	FORMAT (10X,F10.3,1H,28X,1H*)
002440		GO TO 692
002443	630	WRITE (6,830) XMAX2
002451	830	FORMAT (10X,F10.3,1H,29X,1H*)
002451		GO TO 692
002454	631	WRITE (6,831) XMAX2
002462	831	FORMAT (10X,F10.3,1H,30X,1H*)
002462		GO TO 692
002465	632	WRITE (6,832) XMAX2
002473	832	FORMAT (10X,F10.3,1H,31X,1H*)
002473		GO TO 692
002476	633	WRITE (6,833) XMAX2
002504	833	FORMAT (10X,F10.3,1H,32X,1H*)
002504		GO TO 692
002507	634	WRITE (6,834) XMAX2
002515	834	FORMAT (10X,F10.3,1H,33X,1H*)
002515		GO TO 692
002520	635	WRITE (6,835) XMAX2
002526	835	FORMAT (10X,F10.3,1H,34X,1H*)
002526		GO TO 692

002531	636 WRITE (6,836) XMAX2
002537	836 FORMAT (10X,F10.3,1H+,35X,1H*)
002537	GO TO 692
002542	637 WRITE (6,837) XMAX2
002550	837 FORMAT (10X,F10.3,1H+,36X,1H*)
002550	GO TO 692
002553	638 WRITE (6,838) XMAX2
002561	838 FORMAT (10X,F10.3,1H+,37X,1H*)
002561	GO TO 692
002564	639 WRITE (6,839) XMAX2
002572	839 FORMAT (10X,F10.3,1H+,38X,1H*)
002572	GO TO 692
002575	640 WRITE (6,840) XMAX2
002603	840 FORMAT (10X,F10.3,1H+,39X,1H*)
002603	GO TO 692
002606	641 WRITE (6,841) XMAX2
002614	841 FORMAT (10X,F10.3,1H+,40X,1H*)
002614	GO TO 692
002617	642 WRITE (6,842) XMAX2
002625	842 FORMAT (10X,F10.3,1H+,41X,1H*)
002625	GO TO 692
002630	643 WRITE (6,843) XMAX2
002636	843 FORMAT (10X,F10.3,1H+,42X,1H*)
002636	GO TO 692
002641	644 WRITE (6,844) XMAX2
002647	844 FORMAT (10X,F10.3,1H+,43X,1H*)
002647	GO TO 692
002652	645 WRITE (6,845) XMAX2
002660	845 FORMAT (10X,F10.3,1H+,44X,1H*)
002660	GO TO 692
002663	646 WRITE (6,846) XMAX2
002671	846 FORMAT (10X,F10.3,1H+,45X,1H*)
002671	GO TO 692
002674	647 WRITE (6,847) XMAX2
002702	847 FORMAT (10X,F10.3,1H+,46X,1H*)
002702	GO TO 692
002705	648 WRITE (6,848) XMAX2
002713	848 FORMAT (10X,F10.3,1H+,47X,1H*)
002713	GO TO 692
002716	649 WRITE (6,849) XMAX2
002724	849 FORMAT (10X,F10.3,1H+,48X,1H*)
002724	GO TO 692
002727	650 WRITE (6,850) XMAX2
002735	850 FORMAT (10X,F10.3,1H+,49X,1H*)
002735	GO TO 692
002740	651 WRITE (6,851) XMAX2
002746	851 FORMAT (10X,F10.3,1H+,50X,1H*)
002746	GO TO 692
002751	652 WRITE (6,852) XMAX2
002757	852 FORMAT (10X,F10.3,1H+,51X,1H*)
002757	GO TO 692
002762	653 WRITE (6,853) XMAX2
002770	853 FORMAT (10X,F10.3,1H+,52X,1H*)
002770	GO TO 692
002773	654 WRITE (6,854) XMAX2
003001	854 FORMAT (10X,F10.3,1H+,53X,1H*)
003001	GO TO 692
003004	655 WRITE (6,855) XMAX2

003112	GO TO 692
003115	656 WRITE (6,856) XMAX2
003123	856 FORMAT (10X,F10.3,1H+,55X,1H+)
003023	GO TO 692
003026	657 WRITE (6,857) XMAX2
003034	857 FORMAT (10X,F10.3,1H+,56X,1H+)
003034	GO TO 692
003037	658 WRITE (6,858) XMAX2
003045	858 FORMAT (10X,F10.3,1H+,57X,1H+)
003045	GO TO 692
003050	659 WRITE (6,859) XMAX2
003056	859 FORMAT (10X,F10.3,1H+,58X,1H+)
003056	GO TO 692
003061	660 WRITE (6,860) XMAX2
003067	860 FORMAT (10X,F10.3,1H+,59X,1H+)
003067	GO TO 692
003072	661 WRITE (6,861) XMAX2
003100	861 FORMAT (10X,F10.3,1H+,60X,1H+)
003100	GO TO 692
003103	662 WRITE (6,862) XMAX2
003111	862 FORMAT (10X,F10.3,1H+,61X,1H+)
003111	GO TO 692
003114	663 WRITE (6,863) XMAX2
003122	863 FORMAT (10X,F10.3,1H+,62X,1H+)
003122	GO TO 692
003125	664 WRITE (6,864) XMAX2
003133	864 FORMAT (10X,F10.3,1H+,63X,1H+)
003133	GO TO 692
003136	665 WRITE (6,865) XMAX2
003144	865 FORMAT (10X,F10.3,1H+,64X,1H+)
003144	GO TO 692
003147	666 WRITE (6,866) XMAX2
003155	866 FORMAT (10X,F10.3,1H+,65X,1H+)
003155	GO TO 692
003160	667 WRITE (6,867) XMAX2
003166	867 FORMAT (10X,F10.3,1H+,66X,1H+)
003166	GO TO 692
003171	668 WRITE (6,868) XMAX2
003177	868 FORMAT (10X,F10.3,1H+,67X,1H+)
003177	GO TO 692
003202	669 WRITE (6,869) XMAX2
003210	869 FORMAT (10X,F10.3,1H+,68X,1H+)
003210	GO TO 692
003213	670 WRITE (6,870) XMAX2
003221	870 FORMAT (10X,F10.3,1H+,69X,1H+)
003221	GO TO 692
003224	671 WRITE (6,871) XMAX2
003232	871 FORMAT (10X,F10.3,1H+,70X,1H+)
003232	GO TO 692
003235	672 WRITE (6,872) XMAX2
003243	872 FORMAT (10X,F10.3,1H+,71X,1H+)
003243	GO TO 692
003246	673 WRITE (6,873) XMAX2
003254	873 FORMAT (10X,F10.3,1H+,72X,1H+)
003254	GO TO 692
003257	674 WRITE (6,874) XMAX2
003265	874 FORMAT (10X,F10.3,1H+,73X,1H+)

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003265 GO TO 692
003270 675 WRITE (6,875) XMAX2
003276 875 FORMAT (10X,F10.3,1H*,74X,1H*)
003276 GO TO 692
003301 676 WRITE (6,876) XMAX2
003307 876 FORMAT (10X,F10.3,1H*,75X,1H*)
003307 GO TO 692
003312 677 WRITE (6,877) XMAX2
003320 877 FORMAT (10X,F10.3,1H*,76X,1H*)
003320 GO TO 692
003323 678 WRITE (6,878) XMAX2
003331 878 FORMAT (10X,F10.3,1H*,77X,1H*)
003331 GO TO 692
003334 679 WRITE (6,879) XMAX2
003342 879 FORMAT (10X,F10.3,1H*,78X,1H*)
003342 GO TO 692
003345 680 WRITE (6,880) XMAX2
003353 880 FORMAT (10X,F10.3,1H*,79X,1H*)
003353 692 J = J+1
003355 698 CONTINUE
C PRINT X AXIS
003362 XMAX2 = XMAX0 -(XINT0*8.)
003365 905 WRITE (6,910) XMAX2
003373 910 FORMAT (10X,F10.3,1H*,8(10H-----+15X,10HCONSTRAINT)
C FIND SCALE FOR X AXIS AND PRINT
003373 DO 920 I = 1,9
003377 AI = 1
003400 SCL(I) = XMINC +(XINTC * (AI-1.))
003404 920 CONTINUE
003406 WRITE (6,930) SCL(1),SCL(2),SCL(3),SCL(4),SCL(5),SCL(6),SCL(7),
1 SCL(8),SCL(9)
003434 930 FORMAT (16X,F8.3,8(2X,F8.3))
003434 999 RETURN
003435 END

```


000007 DIMENSION A(20,NX)
000007 00 500 J = 1,NX
000010 IF (A(IX,J)) 510,500,510
000014 500 CONTINUE
000017 ISH = 0
000017 RETURN
000020 510 ISH = 1
000021 RETURN
000022 END

```

SUBROUTINE TRAJ (KINIT,KLAST,Y)
COMMON TM
DIMENSION SC(50),Y(50),X(50),B(50)
NOC = KLAST
DO 25 K = KINIT,KLAST
CK = K
X(K) = CK*TM
25 CONTINUE
DO 50 K = KINIT,KLAST
50 B(K) = Y(K)
K = NOC - J
DO 60 I = KINIT,K
58 IF (B(I) - B(I+1)) 60,60,59
59 TEMP = B(I)
B(I) = B(I+1)
B(I+1) = TEMP
60 CONTINUE
FK = KLAST + 1
XMAX = FK*TM
XMIN = C.0
YMAX = B(NOC)
YMIN = B(KINIT)
IF (YMAX - YMIN) 67,68,67
68 YRNG = ABS(YMIN)*2.
GO TO 69
67 YRNG = ABS(YMAX - YMIN)
69 YINT = YRNG/6.
XINT = XRNG/8.
XINT6 = XINT/6.
WRITE (6,70)
70 FORMAT(1H1,15HTRAJECTORY PLOT)
DO 73 I = 1,7
AI = I
73 SC(I) = YMIN + YINT * (AI-1.)
WRITE (6,75) SC(1),SC(2),SC(3),SC(4),SC(5),SC(6),SC(7)
75 FORMAT (1H0, 22X,7F10.3)
WRITE (6,80)
80 FORMAT (29X,1H+,6(10H-----+))
J = KINIT
YINT10 = YINT/10.
K3 = 0
DO 755 K=1,48
K3 = K3+1
XMAXU = XMIN + (XINT6*(AK-1.))
AK = K
XMAXL = XMIN + (XINT6*AK)
IF (J.GT.NOC) GO TO 85
IF (X(J) .GE. XMAXU .AND. X(J) .LE. XMAXL) GO TO 150
85 IF (K3-6) 740,90,740
90 K3 = 0
GO TO 750
150 DO 710 I=1,7
AI = I
YMIN1 = YMIN + YINT * (AI-1.)
YMIN2 = YMIN + YINT*AI

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000214 IF(Y(J) .GE. YMIN1.AND.Y(J).LT. YMIN2) GO TO 160
000226 GO TO 710
000226 160 00 700 I1=1,10
000230 A11=11
000231 YMIN1=YMIN1+(VINT10*(A11-1))
000235 YMIN2=YMIN1+(VINT10*A11)
000240 IF(Y(J) .GE. YMIN1.AND. Y(J) .LT. YMIN2) GO TO 160
000252 GO TO 700
000252 160 IF (K3-6) 290,190,290
000254 190 K3 = 0
000255 GO TO 295
000256 290 GO TO (301,302,303,304,305,306,560),I
000271 295 GO TO (311,312,313,314,315,316,860),I
000304 301 GO TO (500,501,502,503,504,505,506,507,508,509),I1
000322 302 GO TO (510,511,512,513,514,515,516,517,518,519),I1
000340 303 GO TO (520,521,522,523,524,525,526,527,528,529),I1
000356 304 GO TO (530,531,532,533,534,535,536,537,538,539),I1
000374 305 GO TO (540,541,542,543,544,545,546,547,548,549),I1
000412 306 GO TO (550,551,552,553,554,555,556,557,558,559),I1
000430 311 GO TO (800,801,802,803,804,805,806,807,808,809),I1
000446 312 GO TO (810,811,812,813,814,815,816,817,818,819),I1
000464 313 GO TO (820,821,822,823,824,825,826,827,828,829),I1
000502 314 GO TO (830,831,832,833,834,835,836,837,838,839),I1
000520 315 GO TO (840,841,842,843,844,845,846,847,848,849),I1
000536 316 GO TO (850,851,852,853,854,855,856,857,858,859),I1
000554 500 WRITE (6,600)
000560 600 FORMAT (29X,1H*,29X,1H*)
000550 GO TO 720
000563 501 WRITE (6,601)
000567 601 FORMAT (30X,1H*,28X,1H*)
000567 GO TO 720
000572 502 WRITE (6,602)
000576 602 FORMAT (31X,1H*,27X,1H*)
000576 GO TO 720
000601 503 WRITE (6,603)
000605 603 FORMAT (32X,1H*,26X,1H*)
000605 GO TO 720
000610 504 WRITE (6,604)
000614 604 FORMAT (33X,1H*,25X,1H*)
000614 GO TO 720
000617 505 WRITE (6,605)
000623 605 FORMAT (34X,1H*,24X,1H*)
000623 GO TO 720
000625 506 WRITE (6,606)
000632 606 FORMAT (35X,1H*,23X,1H*)
000632 GO TO 720
000635 507 WRITE (6,607)
000641 607 FORMAT (36X,1H*,22X,1H*)
000641 GO TO 720
000644 508 WRITE (6,608)
000650 608 FORMAT (37X,1H*,21X,1H*)
000650 GO TO 720
000653 509 WRITE (6,609)
000657 609 FORMAT (38X,1H*,20X,1H*)
000657 GO TO 720
000662 510 WRITE (6,610)
000666 610 FORMAT (39X,1H*,19X,1H*)
000666 GO TO 720

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000671	511	WRITE (6,611)
000675	611	FORMAT (40X,1H*,10X,1HS)
000675		GO TO 720
000730	512	WRITE (6,612)
000704	612	FORMAT (41X,1H*,17X,1HS)
000704		GO TO 720
000707	513	WRITE (6,613)
000713	613	FORMAT (42X,1H*,16X,1HS)
000713		GO TO 720
000716	514	WRITE (6,614)
000722	614	FORMAT (43X,1H*,15X,1HS)
000722		GO TO 720
000725	515	WRITE (6,615)
000731	615	FORMAT (44X,1H*,14X,1HS)
000731		GO TO 720
000734	516	WRITE (6,616)
000740	616	FORMAT (45X,1H*,13X,1HS)
000740		GO TO 720
000743	517	WRITE (6,617)
000747	617	FORMAT (46X,1H*,12X,1HS)
000747		GO TO 720
000752	518	WRITE (6,618)
000756	618	FORMAT (47X,1H*,11X,1HS)
000756		GO TO 720
000761	519	WRITE (6,619)
000765	619	FORMAT (48X,1H*,10X,1HS)
000765		GO TO 720
000770	520	WRITE (6,620)
000774	620	FORMAT (49X,1H*, 9X,1HS)
000774		GO TO 720
000777	521	WRITE (6,621)
001003	621	FORMAT (50X,1H*, 8X,1HS)
001003		GO TO 720
001006	522	WRITE (6,622)
001012	622	FORMAT (51X,1H*, 7X,1HS)
001012		GO TO 720
001015	523	WRITE (6,623)
001021	623	FORMAT (52X,1H*, 6X,1HS)
001021		GO TO 720
001024	524	WRITE (6,624)
001030	624	FORMAT (53X,1H*, 5X,1HS)
001030		GO TO 720
001033	525	WRITE (6,625)
001037	625	FORMAT (54X,1H*, 4X,1HS)
001037		GO TO 720
001042	526	WRITE (6,626)
001046	626	FORMAT (55X,1H*, 3X,1HS)
001046		GO TO 720
001051	527	WRITE (6,627)
001055	627	FORMAT (56X,1H*, 2X,1HS)
001055		GO TO 720
001060	528	WRITE (6,628)
001064	628	FORMAT (57X,1H*, 1X,1HS)
001064		GO TO 720
001067	529	WRITE (6,629)
001073	629	FORMAT (58X,1H*, 1HS)
001073		GO TO 720
001076	530	WRITE (6,630)

001102	GO TO 720
001105	531 WRITE (6,631)
001111	631 FORMAT (59X,1HS, 1H*)
001111	GO TO 720
001114	532 WRITE (6,632)
001120	632 FORMAT (59X,1HS, 1X,1H*)
001120	GO TO 720
001123	533 WRITE (6,633)
001127	633 FORMAT (59X,1HS, 2X,1H*)
001127	GO TO 720
001132	534 WRITE (6,634)
001136	634 FORMAT (59X,1HS, 3X,1H*)
001136	GO TO 720
001141	535 WRITE (6,635)
001145	635 FORMAT (59X,1HS, 4X,1H*)
001145	GO TO 720
001150	536 WRITE (6,636)
001154	636 FORMAT (59X,1HS, 5X,1H*)
001154	GO TO 720
001157	537 WRITE (6,637)
001163	637 FORMAT (59X,1HS, 6X,1H*)
001163	GO TO 720
001166	538 WRITE (6,638)
001172	638 FORMAT (59X,1HS, 7X,1H*)
001172	GO TO 720
001175	539 WRITE (6,639)
001201	639 FORMAT (59X,1HS, 8X,1H*)
001201	GO TO 720
001204	540 WRITE (6,640)
001210	640 FORMAT (59X,1HS, 9X,1H*)
001210	GO TO 720
001213	541 WRITE (6,641)
001217	641 FORMAT (59X,1HS,10X,1H*)
001217	GO TO 720
001222	542 WRITE (6,642)
001226	642 FORMAT (59X,1HS,11X,1H*)
001226	GO TO 720
001231	543 WRITE (6,643)
001235	643 FORMAT (59X,1HS,12X,1H*)
001235	GO TO 720
001240	544 WRITE (6,644)
001244	644 FORMAT (59X,1HS,13X,1H*)
001244	GO TO 720
001247	545 WRITE (6,645)
001253	645 FORMAT (59X,1HS,14X,1H*)
001253	GO TO 720
001256	546 WRITE (6,646)
001262	646 FORMAT (59X,1HS,15X,1H*)
001262	GO TO 720
001265	547 WRITE (6,647)
001271	647 FORMAT (59X,1HS,16X,1H*)
001271	GO TO 720
001274	548 WRITE (6,648)
001300	648 FORMAT (59X,1HS,17X,1H*)
001300	GO TO 720
001303	549 WRITE (6,649)
001307	649 FORMAT (59X,1HS,18X,1H*)

001307	GO TO 720
001312	550 WRITE (6,650)
001316	650 FORMAT (59X,1HS,19X,1H*)
001316	GO TO 720
001321	551 WRITE (6,651)
001325	651 FORMAT (59X,1HS,20X,1H*)
001325	GO TO 720
001330	552 WRITE (6,652)
001334	652 FORMAT (59X,1HS,21X,1H*)
001334	GO TO 720
001337	553 WRITE (6,653)
001343	653 FORMAT (59X,1HS,22X,1H*)
001343	GO TO 720
001346	554 WRITE (6,654)
001352	654 FORMAT (59X,1HS,23X,1H*)
001352	GO TO 720
001355	555 WRITE (6,655)
001361	655 FORMAT (59X,1HS,24X,1H*)
001361	GO TO 720
001364	556 WRITE (6,656)
001370	656 FORMAT (59X,1HS,25X,1H*)
001370	GO TO 720
001373	557 WRITE (6,657)
001377	657 FORMAT (59X,1HS,26X,1H*)
001377	GO TO 720
001402	558 WRITE (6,658)
001406	658 FORMAT (59X,1HS,27X,1H*)
001406	GO TO 720
001411	559 WRITE (6,659)
001415	659 FORMAT (59X,1HS,28X,1H*)
001415	GO TO 720
001420	560 WRITE (6,660)
001424	660 FORMAT (59X,1HS,29X,1H*)
001424	GO TO 720
001427	800 WRITE (6,900) XMAXL
001435	900 FORMAT (16X,F10.3, 3X,1H*,29X,1H*)
001435	GO TO 720
001440	801 WRITE (6,901) XMAXL
001446	901 FORMAT (16X,F10.3, 4X,1H*,28X,1H*)
001446	GO TO 723
001451	802 WRITE (6,902) XMAXL
001457	902 FORMAT (16X,F10.3, 5X,1H*,27X,1H*)
001457	GO TO 720
001462	803 WRITE (6,903) XMAXL
001470	903 FORMAT (16X,F10.3, 6X,1H*,26X,1H*)
001470	GO TO 720
001473	804 WRITE (6,904) XMAXL
001501	904 FORMAT (16X,F10.3, 7X,1H*,25X,1H*)
001501	GO TO 723
001504	805 WRITE (6,905) XMAXL
001512	905 FORMAT (16X,F10.3, 8X,1H*,24X,1H*)
001512	GO TO 720
001515	806 WRITE (6,906) XMAXL
001523	906 FORMAT (16X,F10.3, 9X,1H*,23X,1H*)
001523	GO TO 720
001526	807 WRITE (6,907) XMAXL
001534	907 FORMAT (16X,F10.3,10X,1H*,22X,1H*)
001534	GO TO 720

001545	GO TO 720
001550	809 WRITE (6,909) XMAXL
001556	909 FORMAT (16X,F10.3,12X,1H*,20X,1H*)
001556	GO TO 720
001561	810 WRITE (6,910) XMAXL
001567	910 FORMAT (16X,F10.3,13X,1H*,19X,1H*)
001567	GO TO 720
001572	811 WRITE (6,911) XMAXL
001600	911 FORMAT (16X,F10.3,14X,1H*,18X,1H*)
001600	GO TO 720
001603	812 WRITE (6,912) XMAXL
001611	912 FORMAT (16X,F10.3,15X,1H*,17X,1H*)
001611	GO TO 720
001614	813 WRITE (6,913) XMAXL
001622	913 FORMAT (16X,F10.3,16X,1H*,16X,1H*)
001622	GO TO 720
001625	814 WRITE (6,914) XMAXL
001633	914 FORMAT (16X,F10.3,17X,1H*,15X,1H*)
001633	GO TO 720
001636	815 WRITE (6,915) XMAXL
001644	915 FORMAT (16X,F10.3,18X,1H*,14X,1H*)
001644	GO TO 720
001647	816 WRITE (6,916) XMAXL
001655	916 FORMAT (16X,F10.3,19X,1H*,13X,1H*)
001655	GO TO 720
001660	817 WRITE (6,917) XMAXL
001666	917 FORMAT (16X,F10.3,20X,1H*,12X,1H*)
001666	GO TO 720
001671	818 WRITE (6,918) XMAXL
001677	918 FORMAT (16X,F10.3,21X,1H*,11X,1H*)
001677	GO TO 720
001702	819 WRITE (6,919) XMAXL
001710	919 FORMAT (16X,F10.3,22X,1H*,10X,1H*)
001710	GO TO 720
001713	820 WRITE (6,920) XMAXL
001721	920 FORMAT (16X,F10.3,23X,1H*,9X,1H*)
001721	GO TO 720
001724	821 WRITE (6,921) XMAXL
001732	921 FORMAT (16X,F10.3,24X,1H*,8X,1H*)
001732	GO TO 720
001735	822 WRITE (6,922) XMAXL
001743	922 FORMAT (16X,F10.3,25X,1H*,7X,1H*)
001743	GO TO 720
001746	823 WRITE (6,923) XMAXL
001754	923 FORMAT (16X,F10.3,26X,1H*,6X,1H*)
001754	GO TO 720
001757	824 WRITE (6,924) XMAXL
001765	924 FORMAT (16X,F10.3,27X,1H*,5X,1H*)
001765	GO TO 720
001770	825 WRITE (6,925) XMAXL
001776	925 FORMAT (16X,F10.3,28X,1H*,4X,1H*)
001776	GO TO 720
002001	826 WRITE (6,926) XMAXL
002007	926 FORMAT (16X,F10.3,29X,1H*,3X,1H*)
002007	GO TO 720
002012	827 WRITE (6,927) XMAXL

002020	927	FORMAT (16X,F10.3,30X,1H*, 2X,1H*)
002020	GO TO 720	
002023	828	WRITE (6,928) XMAXL
002031	928	FORMAT (16X,F10.3,31X,1H*, 1X,1H*)
002031	GO TO 720	
002034	829	WRITE (6,929) XMAXL
002042	929	FORMAT (16X,F10.3,32X,1H*, 1H*)
002042	GO TO 720	
002045	830	WRITE (6,930) XMAXL
002053	930	FORMAT (16X,F10.3,33X,1H*)
002053	GO TO 720	
002056	831	WRITE (6,931) XMAXL
002064	931	FORMAT (16X,F10.3,33X,1H*, 1H*)
002064	GO TO 720	
002067	832	WRITE (6,932) XMAXL
002075	932	FORMAT (16X,F10.3,33X,1H*, 1X,1H*)
002075	GO TO 720	
002100	833	WRITE (6,933) XMAXL
002106	933	FORMAT (16X,F10.3,33X,1H*, 2X,1H*)
002106	GO TO 720	
002111	834	WRITE (6,934) XMAXL
002117	934	FORMAT (16X,F10.3,33X,1H*, 3X,1H*)
002117	GO TO 720	
002122	835	WRITE (6,935) XMAXL
002130	935	FORMAT (16X,F10.3,33X,1H*, 4X,1H*)
002130	GO TO 720	
002133	836	WRITE (6,936) XMAXL
002141	936	FORMAT (16X,F10.3,33X,1H*, 5X,1H*)
002141	GO TO 720	
002144	837	WRITE (6,937) XMAXL
002152	937	FORMAT (16X,F10.3,33X,1H*, 6X,1H*)
002152	GO TO 720	
002155	838	WRITE (6,938) XMAXL
002163	938	FORMAT (16X,F10.3,33X,1H*, 7X,1H*)
002163	GO TO 720	
002166	839	WRITE (6,939) XMAXL
002174	939	FORMAT (16X,F10.3,33X,1H*, 8X,1H*)
002174	GO TO 720	
002177	840	WRITE (6,940) XMAXL
002205	940	FORMAT (16X,F10.3,33X,1H*, 9X,1H*)
002205	GO TO 720	
002210	841	WRITE (6,941) XMAXL
002216	941	FORMAT (16X,F10.3,33X,1H*, 10X,1H*)
002216	GO TO 720	
002221	842	WRITE (6,942) XMAXL
002227	942	FORMAT (16X,F10.3,33X,1H*, 11X,1H*)
002227	GO TO 720	
002232	843	WRITE (6,943) XMAXL
002240	943	FORMAT (16X,F10.3,33X,1H*, 12X,1H*)
002240	GO TO 720	
002243	844	WRITE (6,944) XMAXL
002251	944	FORMAT (16X,F10.3,33X,1H*, 13X,1H*)
002251	GO TO 720	
002254	845	WRITE (6,945) XMAXL
002262	945	FORMAT (16X,F10.3,33X,1H*, 14X,1H*)
002262	GO TO 720	
002265	846	WRITE (6,946) XMAXL
002273	946	FORMAT (16X,F10.3,33X,1H*, 15X,1H*)

002276	847 WRITE (6,947) XMAXL
002304	947 FORMAT (16X,F10.3,33X,1H+,16X,1H*)
002304	GO TO 720
002307	848 WRITE (6,948) XMAXL
002315	948 FORMAT (16X,F10.3,33X,1H+,17X,1H*)
002315	GO TO 720
002320	849 WRITE (6,949) XMAXL
002326	949 FORMAT (16X,F10.3,33X,1H+,18X,1H*)
002326	GO TO 720
002331	850 WRITE (6,950) XMAXL
002337	950 FORMAT (16X,F10.3,33X,1H+,19X,1H*)
002337	GO TO 720
002342	851 WRITE (6,951) XMAXL
002350	951 FORMAT (16X,F10.3,33X,1H+,20X,1H*)
002350	GO TO 720
002353	852 WRITE (6,952) XMAXL
002361	952 FORMAT (16X,F10.3,33X,1H+,21X,1H*)
002361	GO TO 720
002364	853 WRITE (6,953) XMAXL
002372	953 FORMAT (16X,F10.3,33X,1H+,22X,1H*)
002372	GO TO 720
002375	854 WRITE (6,954) XMAXL
002403	954 FORMAT (16X,F10.3,33X,1H+,23X,1H*)
002403	GO TO 720
002406	855 WRITE (6,955) XMAXL
002414	955 FORMAT (16X,F10.3,33X,1H+,24X,1H*)
002414	GO TO 720
002417	856 WRITE (6,956) XMAXL
002425	956 FORMAT (16X,F10.3,33X,1H+,25X,1H*)
002425	GO TO 720
002430	857 WRITE (6,957) XMAXL
002436	957 FORMAT (16X,F10.3,33X,1H+,26X,1H*)
002436	GO TO 720
002441	858 WRITE (6,958) XMAXL
002447	958 FORMAT (16X,F10.3,33X,1H+,27X,1H*)
002447	GO TO 720
002452	859 WRITE (6,959) XMAXL
002460	959 FORMAT (16X,F10.3,33X,1H+,28X,1H*)
002460	860 WRITE (6,960) XMAXL
002466	960 FORMAT (16X,F10.3,33X,1H+,29X,1H*)
002466	GO TO 720
002471	700 CONTINUE
002473	710 CONTINUE
002475	720 J= J+1
002477	GO TO 755
002477	740 WRITE (6,742)
002503	742 FORMAT (59X,1H5)
002503	GO TO 755
002506	750 WRITE (6,752) XMAXL
002514	752 FORMAT (16X,F10.3,33X,1H+)
002514	755 CONTINUE
002520	WRITE (6,760)
002524	760 FORMAT (58X,4HTIME)
002524	999 RETURN
002525	END

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